Geotechnical Report

Trunk Highway 7 / Louisiana Avenue Interchange

St. Louis Park, Minnesota

S.P. No. 2706-226 S.P. No. 163-101-038 SEH No. STLOU 116227

March 19, 2012



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March 16, 2012

I hereby certify that this report was prepared by me or under my direct supervision, and that I am a duly Licensed Professional Engineer under the laws of the State of Minnesota.

Brent A. Theroux, PE Date: March 16, 2012 Lic. No.: 44276 Reviewed by: Wagne & Wantold March 16, 2012

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Geotechnical Report

Trunk Highway 7 / Louisiana Avenue Interchange

Prepared for City of St. Louis Park

1.0 Introduction

A new controlled-access freeway interchange is proposed at the intersection of Trunk Highway 7 (TH 7) and Louisiana Avenue in the city of St. Louis Park, Minnesota. Currently the intersection consists of an at-grade crossing with a traffic signal. The new interchange will consist of a double-span bridge with new 15-foot high approach embankments to carry TH 7 over Louisiana Avenue and three new roundabouts along Louisiana Avenue. Other project elements include a retaining wall along both approach embankments, new embankment fill in ramp areas, a subcut along Louisiana Avenue as it crosses beneath the new bridge, a temporary bypass to maintain traffic during construction, two new stormwater ponds, storm sewer, sanitary sewer, and water main utilities. The project extends along TH 7 from 1500 feet west to 1700 feet east of Louisiana Avenue, and along Louisiana Avenue from 900 feet north to 850 feet south of TH 7. It also includes portions of Walker Street, Lake Street, and the frontage roads located both north and south of TH 7.

Organic soils consisting of peat and organic silt and clay, as well as areas of creosote and other environmental contaminants, are known to exist across the site. While observations of "foreign odors" were noted by the driller on the soil boring logs, this report discusses only the geotechnical aspects of the proposed project features. Information pertaining to environmental analysis and impacts to the project can be found in the "Phase II Investigation Report for the Trunk Highway 7 and Louisiana Avenue Interchange" prepared by SEH and dated January, 2012.

The bridge abutments, central bridge pier, and retaining walls will be supported on driven H-pile foundations bearing on bedrock. Due to environmental contamination, the west approach embankment will also be supported on driven H-piles bearing on bedrock; embankment loads will be transferred to the piles via a Load Transfer Platform (LTP) that consists of geosynthetic reinforcement layers and select fill. Areas of embankment fill for the entrance/exit ramps located outside of the pile-supported LTP will be surcharged. Soil correction beneath the east approach embankment is proposed to consist of 15 to 30 feet of muck excavation and replacement. Construction is proposed to occur in multiple phases, which includes the creation of a temporary paved bypass in order to maintain traffic during the project.

This report presents the results of the project subsurface investigation (completed in 2011); summaries of selected previous subsurface investigations; and geotechnical evaluations for the bridge, retaining walls, approach and ramp embankments, pavement subgrades, buried utilities, and ponds. Geotechnical recommendations for final design of the TH 7 and Louisiana Avenue Interchange are provided herein.

2.0 Background Information

SEH was provided the following documents for reference:

- Braun Intertec, Boring Logs ST-64 and ST-65 (1980)
- Hennepin County Soil Atlas (1989)
- STS Consultants, Boring Logs B-1, B-2, B-4, and B-5 (1989)
- Braun Intertec, Boring Logs ST-1 to ST-5 (2004)
- Braun Intertec, Soil Boring Report (2009)
- Summit Environmental, Water Level Data in Drift Zone, Observation Well W425 (2009-11)
- SEH, Phase II Environmental Investigation Geoprobe Logs GP-1 to GP-33 (2011)

2.1 Scope of Services

This report was prepared in accordance with the April 4, 2011 proposal by SEH to the City of St. Louis Park.

The scope of work for preparing this report included drilling soil borings and performing laboratory testing; these services were provided by Braun Intertec, Inc. of Minneapolis, Minnesota. Details of the drilling and laboratory testing program are discussed in the "Field and Laboratory Investigation" section of this report.

Geotechnical evaluation included providing recommendations for pile capacity, muck excavation, surcharge design, roadway subgrade; as well as assessments of slope stability at retaining wall and embankment slope locations, settlement due to surcharges at ramp locations, and potential impacts from dewatering and staged muck excavation. The scope did not include any environmental assessment or exploration for the presence of hazardous or toxic materials in the soil, surface water, ground water, or air on, below or adjacent to the site.

3.0 Drilling and Laboratory Testing Program

All borings and laboratory testing were completed by Braun Intertec, Inc. of Bloomington, Minnesota between May 9 and June 13, 2011. All soils were classified in accordance with the MnDOT triangular textural soil classification system. The final boring logs were prepared utilizing the MnDOT gINT® templates. The county coordinates and elevation for each boring are provided on the logs. The final boring logs, as completed by Braun, and considered for the bridge foundation analysis are enclosed with this memorandum, as well as a boring location diagram prepared by SEH.

3.1 Drilling

The subsurface investigation consisted of both soil borings and cone soundings (C-1 to C-12). Soil borings consisted of standard penetration test-type (SPT) borings (B-1 to B-14, E-1 to E-5, P-1, and R-1 to R-9) and flight auger-type (FA) borings (S-1 to S-21).

Borings E-1 to E-5 and R-1 to R-9 and soundings C-1 to C-12 were designated as foundation borings. Foundation borings were performed in general conformance with the document "MnDOT Specifications for Subsurface Investigation and Geotechnical Analysis and Design Recommendations", which specifies drilling and testing procedures for borings used in foundation design of structures. These borings were conducted at locations for the bridge abutments, central bridge pier, retaining walls, and fill embankments over suspected organic soils. The CPT soundings were implemented as substitutes for SPT foundation borings originally located within the TH 7 traffic lanes or along the TH 7 shoulder where time and

Geotechnical Report City of St. Louis Park traffic control restrictions were imposed on drilling operations by the MnDOT permitting office. Borings E-1 to E-5 were drilled through organic soils to a depth of 41 feet. Borings R-1 to R-9 were drilled to top of bedrock and then rock cored approximately 10 feet. Soundings C-1 to C-12 were advanced until cone refusal, generally at a depth shallower than the apparent top of bedrock.

Borings B-1 to B-14 and S-1 to S-21 were designated as roadway borings and performed for the purposes of subgrade evaluation and existing pavement section measurements. Roadway borings were drilled through existing pavement sections along TH 7 and Louisiana Avenue and along proposed new ramp embankment alignments. Borings B-1 to B-14 were drilled to a depth of 21 feet. Boring S-1 to S-15 were drilled through existing TH 7 pavement to a depth of 10 feet. Borings S-17 to S-21 were drilled through existing Louisiana Avenue pavement to a depth of 6 feet. Boring S-16 was not drilled due to environmental concerns at its proposed location and was deleted from the investigation program.

Boring P-1 was drilled in the approximate area for a proposed stormwater pond for the purpose of assessing soil stratigraphy and hydrologic qualities.

3.2 Laboratory Testing

Lab testing was performed on foundation borings in general conformance with MnDOT criteria, which requires moisture content tests for all recovered split-spoon samples and dry unit weight and unconfined compression tests for all recovered thin wall samples. In addition, Atterberg limits, gradations, organic content, consolidation, and undrained-unconsolidated triaxial tests were performed on selected samples from all borings.

4.0 General Site Conditions

4.1 Overview of previous work performed at the site

The following paragraphs provide an overview of earthwork performed as part of two previous major construction projects at the site.

4.1.1 TH 7 Fill Embankment and Bridge (circa 1934)

MnDOT historical records indicate a majority of the original Trunk Highway 7 was constructed in 1934. Construction involved several areas of both cuts and fills. In the vicinity of the current project, earthwork primarily entailed building a fill embankment for the highway over peat soils. The extent to which the peat was to be removed or displaced during construction was not noted. The maximum height of the embankment above surrounding finished grade was indicated to be approximately 20 feet, although the original plans note that the final embankment grade was subject to change pending final plan approval. In conjunction with the embankment construction, a bridge was also built to carry the highway over an existing railroad alignment (in the vicinity of borings E-5 and C-11). The plans show a complete excavation of the peat soils in the area for the bridge foundation, which consisted of timber piles. Other than noting the area of peat soils and an apparent "firm bottom," no other soil or earthwork information pertaining to this area of the project was available.

4.1.2 TH 7 & Louisiana Avenue Intersection (circa 1980)

In 1982, the TH 7 embankment was cut down in order to implement an at-grade intersection with the newly extended Louisiana Avenue. The embankment height was decreased approximately 15 to 20 feet. The project included the removal of the TH 7 Bridge over the railroad, a 4-foot subcut along TH 7, and muck excavation and a 9-foot embankment surcharge along Louisiana Avenue. According to MnDOT records, the surcharge along

Louisiana Avenue extended from approximately 200 feet north to 300 feet south of TH 7. The material specifications for the surcharge and backfill material were not contained in the MnDOT records made available. MnDOT records also did not indicate whether the railroad was abandoned in conjunction with the bridge removal or at a later date. The railroad is no longer present at the site.

4.2 **Existing Site Conditions**

The following paragraphs provide a summary of the existing soil and rock conditions encountered during the subsurface investigation performed as part of the current project. Available subsurface data from previous investigations are also presented. Although odors were detected during drilling and testing that may be representative of possible contamination, any environmental impacts were not assessed. Any discussion of environmental considerations pertaining to potential contamination is beyond the scope of this report. Soil samples that exhibited a "foreign odor," as observed by Braun Intertec, are noted on the boring logs.

4.2.1 **Site Conditions**

The project area is located at the existing intersection of TH 7 and Louisiana Avenue in St. Louis Park, Minnesota. TH 7 is a four-lane divided highway with double left-turn lanes at the traffic signal. Louisiana Avenue is a four-lane street with double left-turn lanes at the traffic signal and concrete curbs. Payement along TH 7, Louisiana Avenue, and all side streets within the project area are bituminous-surfaced. Low-lying areas exist below roadway grades northeast and southeast of the intersection. A multi-story apartment building is situated northwest of the intersection, separated from TH 7 by a low-lying ditch with cattails. Southwest of the intersection is a parking lot with bituminous pavement. According to the City, the parking caps a methane venting system associated with the underlying methane gas-producing peat soils.

4.2.2 **Existing Pavement Conditions**

All existing roadways within the project area consist of bituminous pavements. The thickness of the bituminous sections varied for each roadway. See Tables 1a to 1d for summaries of the various pavement thicknesses. No apparent aggregate base section was observed in the soil borings along TH 7.

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Table 1a
TH 7 Pavement – West of Louisiana Avenue

Boring	Traffic Direction	Pavement Thickness (in.)	P200 of Granular Base (%)
B-1	Eastbound	12.5	
S-1	Eastbound	12.5	15
B-2	Westbound	13	12
S-2	Westbound	13.5	
B-3	Eastbound	13.5	
S-3	Eastbound	13	
B-5	Westbound	12	16
S-4	Westbound	12.5	
E-1	Westbound	11.5	
S-5	Westbound	13.5	
E-2	Eastbound	11	
S-6	Eastbound	13	
E-3	Westbound	11.5	
S-7	Eastbound	11	
1	Average	12.4	14.3

Table 1b
TH 7 Pavement – East of Louisiana Avenue

Boring	Traffic Direction	Pavement Thickness (in.)	P200 of Granular Base (%)
S-8	Westbound	12.5	
E-5	Eastbound	11	
S-9	Westbound	14.5	
S-10	Eastbound	14	
B-8	Eastbound	14	14
S-11	Westbound	13	
B-9	Westbound	15.5	14
S-12	Eastbound	14	13
B-10	Eastbound	14	
S-13	Westbound	13	
B-12	Westbound	19	5
S-14	Eastbound	14	16
B-13	Eastbound	18	21
S-15	Westbound	10	11
B-14	Westbound	12	
1	Average	13.9	13.4

Table 1c
Louisiana Avenue Pavement

Boring	Traffic Direction	Pavement Thickness (in.)	P200 of Granular Base (%)
S-17	Northbound	17	
S-18	Northbound	12	8
R-6	Median	4	
R-5	Northbound	10.5	
S-19	Northbound	12	
S-20	Northbound	8.5	8
S-21	Centerline	22	16
Average	for Louisiana Avenue	13.7	10.7

Table 1d
Adjacent Streets Pavement

Boring	Traffic Direction	Pavement Thickness (in.)	P200 of Granular Base (%)
B-4	North Frontage Road.	8.5	22
B-6	South Frontage Road.	8	
B-11	Lake Street West (median)	4	14

4.3 Soil Conditions

4.3.1 General

Fill consisting of generally sandy material was encountered to varying depths across the project site. Underlying the fill in many areas were organic soils ranging from peat to organic clay. Natural outwash sand with gravel and some alluvial sediment were encountered below the fill and organic soils. The outwash sands were generally medium dense to dense, extended to top of bedrock, and contained lenses of fine-grained glacial till.

4.3.2 Bridge

At the bridge location, fill thicknesses varied from approximately 17 feet at the north side of the intersection (R-6) to approximately 27 feet at the southwest portion of the intersection (R-4). The fill material was generally a mix of sand, loamy sand, sandy loam, clay, clay loam, sandy clay loam, and gravel. Fill material ranged in density from loose to medium dense.

Organic soils were encountered below the fill material. The organic soils consisted of peat; organic silt and silt loam; and organic clay and clay loam. The depth to the bottom of the organic soils ranged from approximately 20 feet (C-5) to 34 feet (R-4), with thicknesses ranging from less than one foot (R-5) to 10 feet (C-6, R-6). It's likely that the variation in depth and thickness is primarily due to displacement of the organics during the original highway embankment construction in 1934.

Natural soils encountered below the fill and organics consisted mainly of medium dense to dense outwash sand with varying degrees of gravel and silt and clay. In R-4 and R-5 the outwash sand deposits contained layers mostly gravel. A few lenses of sandy loam till were

also encountered at depth. Possible floating cobbles or boulders within the outwash were noted by the driller at depths of approximately 45 feet in R-1 and 65 feet in R-4.

4.3.3 TH 7 Embankment

Within the footprint of the new embankment west of Louisiana Avenue, fill depths ranged from approximately 6 feet (C-3) to approximately 27 feet at the southwest portion of the intersection (R-4). East of Louisiana Avenue, fill depths varied from 12 feet at the east end of the embankment (R-9, C-12) to 30 feet at the intersection (C-7). The fill material was generally a mix of sand, loamy sand, sandy loam, clay, clay loam, sandy clay loam, and gravel. Fill material ranged in density from loose to medium dense.

Organic soils were encountered below the fill material. The organic soils consisted of peat; organic silt and silt loam; and organic clay and clay loam. West of Louisiana Avenue the depth to the bottom of the organic soils ranged from approximately 15 feet (E-1) to 34 feet (R-4), with thicknesses ranging from 3 feet (C-4) to 20 feet (C-1, C-2). East of Louisiana Avenue the depth to the bottom of the organic soils ranged from approximately 17 feet (R-9, C-12) to 39 feet (C-9), with thicknesses ranging from 5feet (R-9, C-12) to 14 feet (C-9). It's likely the variation in organic depths and thicknesses is primarily due to displacement of the organic soils during the original highway embankment construction in 1934.

It should be noted that no discernible layers of organic soils were identified in boring E-5 or sounding C-11, which were located in the approximate location of the old bridge carrying TH 7 over a railroad line. This finding would seem to corroborate the complete muck excavation of organic soils from under the bridge as shown in the 1934 MnDOT historical record.

Natural soils encountered below the fill and organics consisted mainly of medium dense to dense outwash sand with varying degrees of gravel and silt and clay. In E-1, E-4, C-6, R-7, and E-5 the outwash sand deposits exhibited strata layers consisting of mostly gravel. A few lenses of sandy loam till were also encountered at depth. Possible cobbles or boulders within the outwash were noted by the driller in other borings between approximate depths of 35 and 75 feet.

4.3.4 Louisiana Avenue and Side Streets

Fill material beneath Louisiana Avenue consisted of sand and loamy sand (S-17 to S-21).

Approximately 5 ½ feet of loose sandy loam fill was encountered along Lake Street West at the entrance to the SW parking lot. Below the fill were a 2-foot layer of peat and a 2-foot layer of firm alluvial clay overlying medium dense outwash sand.

Four feet of dense loamy sand fill over medium dense outwash sand was encountered in B-11 at the Lake Street West entrance and exit along the north side of TH 7.

4.4 Rock Conditions

Bedrock consisted of dolomitic limestone of the Platteville Formation. The apparent top of bedrock was taken as the depth to which refusal of the hollow stem auger system was observed prior to commencing rock coring. The depth to bedrock was somewhat consistent, ranging from 70 to 76 feet, or elevation 820.3 to 822.0. The rock quality designation (RQD) for each 5-foot run of rock core collected is provided in Table 2. The average RQD for the first core run was 47, or poor. For the second core run the average RQD was 90, or good/excellent. A definition of the RQD measurement is provided in the 2011 Braun soil report (Appendix A).

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Table 2
Bedrock Conditions.

Boring	Bedrock Depth (ft)	Bedrock Elevation	RQD, Run 1	RQD, Run 2
R-1	73	820.9	42	90
R-2	75	817.9	55	98
R-3	70	822.0	20	90
R-4	75	820.3	77	91
R-5	75	822.0	84	82
R-6	76	821.0	68	98
R-7	73	823.6	50	88
R-8	70	818.0	0	93
R-9	72	825.7	26	84
Average	73	821.3	47	90

4.5 Groundwater

Groundwater measurements were recorded in each boring A) during drilling operations while hollow stem auger was in the ground, B) when full depth was reached with hollow stem auger in the ground, and C) immediately after withdrawal of the hollow stem auger.

Groundwater was encountered in a majority of the borings. Groundwater was observed between elevations of 878 and 893 across the project site. The average elevation was 884.9 with a standard deviation of 2.8 feet.

The subsurface investigation performed as part of the project's Phase II evaluation included 33 geoprobe borings. The Phase II investigation measured groundwater elevations between elevations 873 and 891. A previous geotechnical investigation performed by Braun Intertec for SEH in 2009, which included 12 soil borings, found groundwater elevations 874 and 885.

Water level data from an observation well located just northeast of the project site was provided from Summit Environmental, an environmental consultant monitoring groundwater behavior for the City of St. Louis Park. The observation well, W425, is screened to collect water levels within the drift zone, or the collection of outwash sands and surface fills above bedrock. The well data consisted of local water table elevation measurements from January 2009 to April 2011. Over that period, the minimum recorded elevation was approximately 880.9 and the maximum was approximately elevation 882.5; the maximum elevation reading occurred in April 2011 at the limit of the plotted observation period and appeared to be trending upward.

The observation well data was compared to the groundwater measurements recorded from the 2009 soil borings, which were performed from March 25 to 29, 2009. The average groundwater elevation recorded from the 2009 soil borings was 881.1 with a standard deviation of 3.2 feet. From the observation well data, the groundwater elevation within the drift zone at the end of March, 2009 was approximately 881.7. From this comparison, there appears to be a reasonable corroboration between the observation well data and the soil boring groundwater measurements.

In general, based on the 2011 and 2009 soil borings and the 2011 geoprobe borings, groundwater observed within and above organic soil layers appears to be mainly perched and

thus more susceptible to daily and seasonal fluctuations. A table summarizing the approximate groundwater depths and elevations measured at boring locations is provided in the Appendix.

Groundwater measurements during drilling operations in sandy soils can be representative of current levels. However, long term water levels in organic and predominantly silty and/or clayey soils may not be indicative of the long term water table. Measurements should be performed with the aid of an open pipe piezometer in order to obtain a more accurate depiction of water levels over a period of time. In general, groundwater levels should be expected to fluctuate based on a variety of reasons, including season, temperature, runoff, and other factors.

5.0 Geotechnical Evaluations

The recommendations provided in this report are based on the proposed project layout, results of the subsurface investigation, discussions with MnDOT Foundations staff, our review of relevant information made available to us, and our understanding of the nature of the proposed project. If any project elements change, or soil and groundwater conditions are encountered that vary from those described in this report, it is necessary that we be notified so we may review our recommendations to determine if revisions are required.

5.1 Bridge Foundations

The new TH 7 Bridge will be a two-span structure. Substructures will be supported on steel HP 12x53 non-displacement piles driven to bear on bedrock. Analyses were performed for the purpose of evaluating the static pile capacity for the bridge foundations. A static capacity calculation using the Nordlund-Thurman method for cohesionless soils was performed using soil conditions from boring R-5, which depicted the least amount of organic soil. The calculation yielded an ultimate static capacity of only 117 tons at elevation 822. For reference, the average bedrock elevation is 821.1. The analyses indicate that the outwash sands located at depth across the site do not have sufficient skin friction and end-bearing capacity for support of the bridge foundations. Therefore it is recommended that the piles be driven to bedrock obtain capacity in end bearing.

Per the 2010 AASHTO LRFD Bridge Design Manual, steel piles supported on top of competent bedrock should be assumed to have a static end-bearing capacity governed by the yield strength of the steel. HP 12x53 piles composed of A572 steel will be used for support of the bridge. Table 10.2.1 from the MnDOT LRFD Bridge Design Manual stipulates HP 12x53 piles to be limited to a factored axial load (P_u) of 140 tons (this includes downdrag load, discussed below). When driven to bear on rock, a factored design load (ϕR_n) of 140 tons should be used. Pile lengths will be governed by the top of bedrock elevation (see Table 2). Table 3 provides a summary of the foundation recommendations for the abutments and central pier.

Table 3
Bridge Pile Foundation Summary

Substructure	West Abutment	Central Pier	East Abutment
Assumed Base Elevation	898.8	886.6	899.2
LRFD Axial Capacity, ϕR_n			
(tons)	140	140	140
Boring	R-4	R-5, R-6	R-7
Estimated Tip Elevation	820.3	821.5	824.6
Estimated Pile Length (ft)	79	65	75

Organic soils up to 10 feet thick may contribute up to an additional 20 tons of negative skin friction (i.e. downdrag) load on the piles. Below the organic soils, driven piles will penetrate through predominantly granular soils that are not anticipated to generate downdrag forces.

For a detailed evaluation and further discussion regarding the bridge foundation recommendations, please refer to Memorandum regarding Subsurface Conditions and Foundation Recommendations for Bridge No. 27301, dated July 28, 2011, included in the Appendix.

5.2 Abutment Backfill

Abutment backfill must be well-drained in order for the following recommendations to be valid. It is recommended that any material placed as backfill behind the abutments consist of granular borrow meeting the requirements of MnDOT 3149.2B1. Material meeting this specification is recommended to be consistent with the suitable on-site fill that will be re-used to construct the adjacent approach embankments. Compaction of materials is recommended to comply with the requirements of MnDOT 2451. Lifts should be limited to no more than 1 foot in loose thickness.

For abutment backfills so constructed, the lateral earth load may be computed using the following equivalent fluid density (efd) expressed in pounds per cubic foot (pcf). This is based on the assumption that the compacted granular backfill soils will have a moist unit weight of 125 pcf, an angle of internal friction (ϕ) of 30°, and there is not lateral loading due to water.

Active Earth Pressure: efd = 42 pcf At Rest Earth Pressure: efd = 63 pcf

5.3 Retaining Walls

Two cast-in-place (CIP) concrete retaining walls will be constructed along the north side of the west approach embankment (NW wall) and the south side of the east approach embankment (SE wall). Both walls will be supported on steel HP 12x53 non-displacement piles. MnDOT standards for pile supported CIP concrete retaining walls require the piles to develop a working load capacity of 60 tons (see MnDOT Standard Plan Sheet No. 5-297.630, 2 of 4). The piles are recommended to be driven to bear on bedrock where the allowable factored load of 140 tons for the steel HP 12x53 piles provides sufficient capacity to develop the 60 ton working load. Table 4 provides a summary of retaining wall pile recommendations. Wall foundations will be buried a minimum of 4 feet per MnDOT guidelines.

Table 4
Retaining Wall Foundation Summary

Wall	NW Wall	SE Wall
Footing Elevations	892.2-899.1	893.4-899.4
Borings	R-2, R-6	R-5, R-8, R-9
Estimated Tip Elevation	819.5	821.9
Estimated Pile Lengths (ft)	73-80	72-78
Estimated Pile Capacity,		
Working Load (tons)	60	60

It is recommended that any material placed as backfill behind the retaining walls consist of granular borrow meeting the design criteria of MnDOT standard plan sheets for retaining walls (e.g. 5-297.630). Compaction of materials is recommended to comply with the requirements of MnDOT 2451. Lifts are recommended to be limited to no more than 1 foot in loose thickness.

For wall backfill so constructed, the lateral earth load may be computed using the following equivalent fluid densities (efd) expressed in pounds per cubic foot (pcf). These are based on MnDOT criteria that the compacted soils will have a moist unit weight of 125 pcf, an effective angle of internal friction (ϕ ') of 35°, and be well-drained so there is minimal lateral loading due to water pressure. They are valid for level backfill with no surcharge load and no hydrostatic load.

Active Earth Pressure: efd = 34 pcf At Rest Earth Pressure: efd = 54 pcf

5.4 General Embankment

Unless otherwise recommended below, embankment fill sections are recommended to be constructed in accordance with MnDOT 2105. Compaction is recommended to follow the Specified Density Method as outlined in MnDOT 2105. Outside of specific areas discussed herein, on-site non-organic granular and loamy soils are suitable for re-use as common borrow. However, due to environmental concerns, it is recommended to refer to the Phase II Investigation Report for further information regarding the disposition of on-site soils.

5.5 East Approach Embankment

5.5.1 Muck Excavation (Remove/Replace)

The east approach embankment will extend from the east bridge abutment at approximate Station 986+05 to Station 993+00. The SE retaining wall extends along the south side of the embankment from the east abutment to Station 990+80. Side slopes along the main alignment range from 2.3H:1V to flatter than 6H:1V; outer fill slopes along the ramp sections are as steep as 2H:1V. The maximum embankment height will be approximately 15 feet above existing grade at the east abutment.

Compressible organic soils consisting of peat and organic clay and silt were encountered beneath variable fill soils within the east embankment footprint. Settlements up to 22 to 27 inches due to consolidation of the organic soils are estimated to occur at the east abutment if no ground improvement measures are taken. Additional settlement due to secondary compression would also occur in the long term. Beyond settlement, consolidation and secondary compression would generate downdrag forces acting on the east abutment and SE retaining wall piles. Such settlements and the associated downdrag forces are not acceptable beneath bridge approach embankments.

The findings of the Phase II investigation indicate that some soils encountered in the area of the east embankment footprint qualify as unrestricted reuse material or may be eligible for reuse on the project site. The final disposition of the soil will be determined in the approved Response Action Plan (RAP).

It is therefore recommended to muck excavate the compressible organic soils from beneath the east approach embankment and northeast and southeast ramp fill areas and to replace with select fill. A muck excavation would eliminate the potential for unacceptable embankment settlements

Geotechnical Report City of St. Louis Park and pile downdrag forces. Vertical and horizontal limits of the muck excavation should be in accordance with guidelines provided in the MnDOT Geotechnical and Pavement Manual.

Dewatering will likely be required to accomplished removal of all organic soils. Drawdown of groundwater levels by construction dewatering may impact adjacent structures and ground areas. Possible measures for monitoring adjacent structures include, but are not limited to, crack gauges, photo documentation, structure surveys, and water level readings.

Excavation stability should follow OSHA standards and should be the responsibility of the contractor. If a temporary shoring system is required, the contractor should submit for review a muck excavation plan providing for temporary shoring. The contractor should also be required to submit a dewatering plan for construction that includes both a pre-condition survey and provisions for monitoring and repairing adjacent structures and ground areas. Both the muck excavation plan and dewatering should be prepared and bear the stamp of a professional engineer licensed in the state of Minnesota and experienced with similar projects.

Replacement fill placed below the water table and up to a minimum of 3 feet above the water table is recommended to be a MnDOT 3149.2B2 Select Granular Borrow modified so that no more than five percent by weight of the material passes the US No. 200 sieve. Compaction of the modified Select Granular Borrow is recommended to be in accordance with the Quality Compaction Method of MnDOT 2105. Embankment fill and replacement fill placed above the modified Select Granular Borrow can be suitable common borrow material.

5.6 West Approach Embankment

The west approach embankment will extend from Station 975+00 to the west bridge abutment at approximate Station 983+76. The NW retaining wall extends along the north side of the embankment from Station 979+25 to the west abutment. Side slopes along the main alignment range from 2H:1V to 4.6H:1V; outer fill slopes along the ramp sections will be as steep as 2H:1V. The maximum embankment height will be approximately 15 feet above existing grade at the west abutment.

Similar to the east approach embankment area, compressible organic soils consisting of peat and organic clay and silt were encountered beneath variable fill soils within the west embankment footprint. However, unlike beneath the east embankment, the organic soils and underlying outwash sands beneath the west approach embankment are known to contain elevated levels of contamination. The Phase II investigation identified that the contaminant concentrations are above standard soil reference values established by the Minnesota Pollution Control Agency (MPCA). Additional cost would be associated with the disposal of the soil from this area.

A Value Engineering Study Report dated August 10-13, 2010, which was commissioned by MnDOT and prepared by HDR Engineering, Inc., suggested the option of employing a pile supported embankment design as one of three alternative options for fill areas west of Louisiana Avenue. The other two options included 1) use of lightweight fill within embankment fill, and 2) use of ground improvement techniques such as deep soil mixing, stone columns, vibrocompaction, etc. A pile supported embankment design was deemed the best fit for this project because A) it poses less risk associated with long term embankment settlements even when using lightweight fill, and B) a specialty contractors, which are typically required for the various ground improvement methods presented in the report, would not be needed. Please refer to the HDR report for further discussion regarding alternative options.

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5.7 Pile Supported Embankment

Although pile supported embankments have seen wide use in the United States, at the outset of this project's design, only one such embankment had been constructed in Minnesota (TH 241 in St. Michael in 2005). The TH 241 pile supported embankment was designed by Jim Collin of The Collin Group, Inc., under contract to MnDOT, and the plans were prepared by the MnDOT Foundations unit.

In general, the function of a pile supported embankment is transfer the load from new embankment fill via steel piles to a firm bearing stratum below poor soils. The two primary design concerns are: 1) determining the site's capacity to support pile foundations, and 2) designing the Load Transfer Platform that conveys the embankment load to the piles.

Many publications exist that discuss the history, design, and performance of pile supported embankments. The paper, "Column Supported Embankment Design Considerations" by Dr. Jim Collin was used as the primary basis for this evaluation. Additionally, MnDOT Foundations personnel were consulted and provided input based on their experience with the TH 241 project.

5.7.1 Pile Foundations and Pile Caps

Similar to the bridge and retaining walls, HP 12x53 non-displacement piles composed of A572 steel are recommended for support of the west approach embankment. The piles should be driven to bear on competent bedrock. Based on borings R-1 to R-4, which were drilled west of Louisiana Avenue, the top of the Platteville Limestone is estimated to be at approximate elevation 818 to 820 (see Table 2 for a summary of bedrock elevations). Outer piles not adjacent to the retaining wall should be battered 1H:4V. Per Table 10.2.1 from the MnDOT LRFD Bridge Design Manual, the factored design load for the piles should be limited to 140 tons.

To the extent possible, the pile cap elevations beneath the west embankment should be equivalent to the pile caps for the adjacent NW retaining wall. Assuming a maximum fill height of 15 feet and a maximum bury depth of 5 feet for the retaining wall foundation, a height of 20 feet was used as a basis to determine the embankment design load to be imparted to the piles below the west embankment. For a square pile layout (i.e. perpendicular rows of piles) and a pile spacing of 10 feet, the maximum design load per pile is 133 tons. Pile caps should have a minimum dimension of 24 inches. The outside edge of the outermost pile caps should be no more than 18 feet from the toe of the embankment.

A global stability analysis was performed to assess edge stability of the embankment slope outside of the pile supported footprint. MnDOT and FHWA guidelines for reinforced soil slopes require a minimum factor of safety (FS) of 1.3 with respect to external stability. In considering the outer portions of the pile supported embankment to be a form of reinforced soil slope due to the presence of geosynthetic elements required for the LTP (discussed below), the minimum required FS was increased to 1.5 due to the presence of organic soil deposits that vary in thickness and shear strength. By requiring that the outside edge of the outermost pile cap to be located no more than 18 feet from the embankment toe, a FS of 1.5 was calculated with respect to global (external) stability.

In order to provide reinforcement against edge stability failures and to counteract the potential for lateral spreading of the embankment over weak organic soils, placement of a geosynthetic elements are required. The geosynthetic elements are discussed in more detail in the following section. Recommended design properties are provided in Table 5b.

5.7.2 Load Transfer Platform (LTP)

In order to transmit the embankment load to the pile caps, a Load Transfer Platform (LTP) must be constructed. In accordance with the Collin Method, the LTP is assumed to function as a beam or platform facilitating the load transfer. Performance is predicated on fully developed soil arching occurring within the LTP. The Collin Method requires that the design thickness of the LTP be no less than one half the clear span distance between pile caps. The method also requires an assumption of the soil arching angle within the platform. Provided a suitable well-graded material is used as backfill within the LTP, the standard of practice indicates that arching can be assumed to occur at an angle of 45 to 60 degrees (as measured from the horizontal plane).

In practice, the LTP is a reinforced soil mass consisting of geosynthetic layers and well-graded select fill. The geosynthetic layers provide confinement for the select fill so that soil arching develops within the design thickness of the LTP. The Collin Method stipulates that a minimum of three (3) layers of geosynthetics (typically geogrids) be employed within the select fill and that a base geosynthetic (typically a reinforcement geotextile) be deployed at the bottom of the LTP on top of the pile caps. The geogrids and reinforcement geotextile are designed using equations provided by the Collin Method that are based on tension membrane theory.

Based on a square pile spacing of 10 feet and pile cap width of 2 feet, the LTP is recommended to be a minimum of 4 feet thick. Backfill within the LTP is recommended to be a MnDOT 3138 Class 5 aggregate base material and should be compacted in accordance with MnDOT 2451.

For a 4-foot thick platform, the geogrids should be spaced 12 inches apart, with the bottom geogrid no more than 12 inches above the base reinforcement geotextile. The geogrids are recommended to be biaxial geogrids with minimum values specified in both the machine and cross machine directions for the tensile strength at 2% strain and the tensile strength at 5% strain. Similarly, the base reinforcement geotextile is recommended to have minimum values specified in both the machine and cross machine directions for the tensile strength at 2% strain and the tensile strength at 5% strain. It is recommended that the base reinforcement geotextile be placed in continuous panels perpendicular to the embankment centerline. The geogrids are recommended to be placed in alternating layers both parallel to and perpendicular to centerline (i.e. the top and bottom layers aligned parallel with the middle aligned perpendicular). Overlap of adjacent layers is recommended to be a minimum of 18 inches. The base reinforcement geotextile is recommended to extend from toe to toe and the geogrids are recommended to extend all the way through to the slope face. For situations where a portion or all of the LTP will be below final grade, the geogrids and the base geotextile are recommended to extend laterally to the same offset distance as the embankment toe.

Table 5a
Recommended Material Properties for LTP Geogrids.

Property	MD ¹	CD1	Units	Test Method
Minimum Tensile Strength at 2% Strain	600	600	pounds per foot	ASTM D6637
Minimum Tensile Strength at 5% Strain	400	400	pounds per foot	ASTM D6637
Minimum Coefficient of Interaction, Ci	0.	.8	n/a	ASTM D6706

¹MD = Machine Direction (also referred to as Roll Direction), CD = Cross Machine Direction

Table 5b
Recommended Material Properties for LTP Base Geotextile1.

Property	MD^2	CD ²	Units	Test Method
Minimum Tensile Strength at 2% Strain	600	600	pounds per foot	ASTM D6637
Minimum Tensile Strength at 5% Strain	400	400	pounds per foot	ASTM D6637
Minimum Coefficient of Interaction, Ci	0.	.8	n/a	ASTM D6706
Minimum Permittivity	0.	.1	sec ⁻¹	ASTM D4491

The Base Geotextile required in both LTP design and lateral spreading evaluation should be the same product. Properties provided satisfy recommendations for both applications.

5.8 West Embankment Ramps and Temporary Bypass

The northwest and southwest ramps along the west approach embankment will be constructed on fill areas over compressible organic soils. Up to 8 feet of fill is expected to be placed in the ramp areas. Also, prior to construction of the pile supported west approach embankment, a temporary bypass alignment will be constructed on fill along the south edge of the project for the purposes of maintaining TH 7 traffic. Up to 3 feet of fill is expected to construct the temporary bypass.

The final grades along the west embankment ramps and bypass areas are at lower elevations than the final grades along centerline of the main approach embankment. Any pile support of these areas in conjunction with the main embankment would require additional excavation beneath the main embankment in order to keep the pile caps and LTP at consistent elevations. A consistent LTP elevation is necessary in order to maintain continuous geosynthetic elements within the LTP. Any additional excavation beneath the main embankment would likely penetrate into contaminated soils. Therefore the ramp and bypass fill areas are recommended to receive embankment surcharges.

5.8.1 Surcharges

As the ramp embankment areas cannot be incorporated into the main pile supported section, it is recommended the underlying compressible soils be surcharged prior to final grading and pavement construction. Without surcharging (also referred to as preloading or precompression), settlements of up to 15 inches are expected due to primary consolidation with an additional 5 inches of settlement due to secondary compression occurring over the long term, or approximately 50 years.

The surcharge sections are recommended to compress the underlying organic soils beyond the primary consolidation and secondary compression estimates. Surcharge heights are recommended to consist of 5 feet of fill placed above final embankment grade. The surcharge fill should be a suitable non-organic material with a minimum in-place unit weight of 120 pcf (pounds per cubic foot). Placement of fill over compressible organic and cohesive soils results in build-up of excess pore pressures that can cause slope instability. A reinforcement geotextile is recommended at the base of embankment fills in surcharge areas to provide additional resistance against slope instability.

With a reinforcement geotextile, a FS of at least 1.3 with respect to slope stability was calculated for a full height surcharge embankment assuming undrained (i.e. end of construction) conditions. Surcharge fill is recommended to be placed in staged lifts wherein subsequent lifts are placed upon dissipation of excess pore pressures that resulted from the previous lift. Excess pore pressures and settlement are recommended to be monitored

² MD = Machine Direction (also referred to as Roll Direction), CD = Cross Machine Direction

throughout the surcharge period. Refer to Construction Monitoring and Instrumentation section below for discussion regarding monitoring of surcharge settlement and excess pore pressures.

The locations (by station), estimated time of surcharge, and estimated total settlement due to both primary consolidation and secondary compression for each surcharge area are provided in Table 6.

Table 6
Surcharge Summary

Surcharge Area	Stations	Estimated Total Settlement (in.)	Estimated Surcharge Period (days)
NW Ramp	976+50 to 981+00	20	46
SW Ramp	975+00 to 981+00	18	47
Temp. Bypass	979+50 to 983+54 ¹	14	30

¹ Approximate station at intersection with Louisiana Avenue

5.9 Pavement and Subgrade

Outside of the bridge approach and ramp embankment fill areas, existing subgrade soils consisted primarily of sandy fill with varying amounts of silt and loam. R-value tests were conducted on two samples of sandy loam fill. The samples were from B-3 and B-13, respectively located west and east of the proposed approach embankments along TH 7. R-value testing returned values of 28 and 71 from B-3 and B-13, respectively. Because of the wide variability within existing fill material, the lower R-value of 28 was used as the basis for evaluation of pavement support.

Evaluation of pavement support considered traffic data for TH 7 and Louisiana Avenue using 2010 as the base year and 2030 as the design year. Equivalent single-axle loads (ESAL) were calculated using criteria provided in the MnDOT Pavement Manual for the seven county Twin Cities area. The ESAL and R-value parameters were used in conjunction with Table 5-3.7 from the MnDOT Pavement Manual to determine the required Granular Equivalent (GE) for TH 7 and Louisiana Avenue pavement sections. Assuming minimum bituminous and aggregate base sections for both TH 7 and Louisiana Avenue, it is recommended to incorporate a 1.5 foot (18 inch) subcut backfilled with MnDOT Select Granular Borrow in order to satisfy the total required GE. Table 7 provides a summary of the pavement evaluation.

Table 7
Summary of Pavement Evaluation

	TH 7	Louisiana Avenue ¹
AADT, 2010	35,000	12,400
AADT, 2030	40,000	20,900
20-yr ESAL	7,128,000	3,163,000
R-value	28	28
Required Total GE	31	29
Minimum Bituminous GE	16	14
Minimum Aggregate Base GE	6	6
Required Additional GE	9	9
Recommended Subcut ²	1.5 ft	1.5 ft

The pavement section for Louisiana Avenue is also recommended for Walker Street,

W. Lake Street, and W. 37th Street

Backfilled with MnDOT 3149.2B2 Select Granular material

5.10 Utilities

Existing sanitary sewer, water main, and force main lines will be removed and replaced (the force main service carries contaminated groundwater to a City-operated pump house). All three new utilities are proposed to be re-aligned along Louisiana Avenue, pass beneath the new bridge, and remain outside of pile support, surcharge, and most muck excavation areas. Only a segment of force main line approximately 250 feet long will intersect a portion of the recommended east approach embankment muck excavation. The depth of the new utilities is expected to be between 5 to 10 feet below finished grade, or approximately elevation 880-885.

Deposits of organic soils between 8 and 13 feet thick were identified in borings performed as part of multiple subsurface investigations (see Table 8). Utilities supported within or over organic soils can experience unacceptable deflections. It is recommended to either A) excavate the organic soils from beneath the utilities and replace with suitable compacted fill and bedding, or B) support the utilities on a deep foundation system such as steel piles or helical piles. In general, it is recommended to align utilities as much as possible beneath the center of Louisiana Avenue to minimize overlap with either the muck excavation or pile support installation. Construction of the force main segment within the muck excavation south of TH 7 will need to be staged and coordinated with that effort. Table 8 presents a summary of the soil conditions for borings located along the new utility alignments.

Table 8
Utility Soil Conditions (approx. north to south along Louisiana Ave.)

Boring	Approx. Surface Elev.	Approx. Bottom Elev. Of Org. Soils	Thickness of Org. Soils (ft)	Notes
ST-5 ¹	893.6	881.6	10	Slightly organic fill with peatSlightly organic soft clay
GP-9 ²	895.0	880.0	8	 Slightly organic sand and clay fill Peat Foreign odors detected Significant sheen noted on soil and groundwater
GP-8 ²	896.0	875.0	13	Slightly organic sand and clay fillPeatOrganic silt
B-10 ³	896.2	877.2	12	Organic clay fillPeat
R-6	897.0	870.0	10	PeatSlightly organic clay (very soft to firm)Foreign odors detected
R-5	897.0	n/a	n/a	No organic soils encountered
GP-16 ²	888.0	872.5	11.5	PeatOrganic silt
ST-1 ¹	891.4	873.4	10	PeatOrganic clayForeign odors detected

²⁰⁰⁴ Subsurface Investigation by Braun Intertec for City of St. Louis Park

² 2010 Phase II Investigation

³ 2009 Subsurface Investigation by Braun Intertec for SEH

5.11 Ponds

New stormwater ponds will be situated in the northeast and southeast quadrants. Geosynthetic liners will be installed at both ponds. The liners are required to maintain separation of groundwater and stormwater. Both ponds will maintain a minimum permanent water level. Excavation for both ponds will occur within and adjacent to the east approach embankment. Perform excavation for ponds in accordance with the recommendations provided herein for muck excavation.

6.0 Construction Monitoring and Instrumentation

6.1 Construction Monitoring

Monitoring during construction will be critical for the pile supported embankment and surcharge embankments. Construction of these features requires that special instrumentation be installed to record data and that a monitoring program be developed to collect and evaluate the data. The following provides recommendations for type of instrumentation, installation details, and data evaluation. All instruments discussed are capable of continuously recording data to an automatic data logging system.

6.1.1 Load Transfer Platform

A key requirement for acceptable performance of the pile supported embankment is that all of the vertical embankment load above the LTP must be transferred to the pile caps. Field measurement of this load transfer can be accomplished in a few different ways, using earth pressure cells, piezometers, geotextile strain gages, or the ShapeAccelArrayTM system. Use of at least two different instrument types is recommended for redundancy so that estimates of load transfer from one device can be correlated and confirmed to those of another device.

6.1.2 Embankment Surcharges

Measurements of excess pore pressure and settlement are important when constructing surcharges. Excess pore pressures are typically recorded using piezometers. Settlement plates are simple and economical devices for monitoring settlements beneath embankments.

6.2 Instrumentation

6.2.1 Earth Pressure Cells

Measurement of non-hydrostatic force and stress within soil materials is typically accomplished with earth pressure cells (EPCs). As it is not technically possible to measure actual stress, EPCs estimate stress by one of two ways: 1) using a strain gage to measure the strain imposed on an internal diaphragm due to external loads and then converting the strain to stress, and 2) using a pressure transducer to directly measure the change in hydrostatic pressure imposed on a fluid-filled cell. Field stress measurements are dependent on many factors, such as the geometry of the measuring device, its relative stiffness compared to the surrounding material, and its method of calibration. For example, EPCs fabricated with a rigid casing will typically record a lower stress as load is shed to the ridged casing and away from the measuring diaphragm, leading to an under-registration of the true in-situ stress field. These factors can be accounted for with appropriate laboratory calibration of the EPC under conditions expected to mimic those to be encountered in the field.

For the pile supported embankment, EPCs are recommended to be installed at four typical locations: 1) directly above the pile cap at the bottom of the LTP, 2) directly above the pile cap at the top of the LTP, 3) between pile caps at the top of the LTP, and 4) between pile caps at the bottom of the LTP. A report prepared for MnDOT by the University of Minnesota

documented the instrumentation and performance of the TH 241 pile supported embankment. EPCs were installed as part of that study and they indicated that the majority of the load transfer to the pile caps occurred above – and not within – the LTP.

6.2.2 Piezometers

When fill is placed over soil under saturated conditions, the vertical load from the fill is immediately transferred to the surrounding groundwater where it is manifested as excess pore pressure. In granular soils, the excess pore pressure dissipates quickly. In cohesive soils, such as peat and organic silt and clay, the dissipation occurs over time and allows field measurements to be made.

Piezometers are recommended to be installed within the organic soils beneath surcharge areas. The buildup and dissipation of excess pores pressures provide an indication of consolidation progress and how fast or slow staged fill placement should progress. Fill that is placed too fast and to too great of a height can risk failure of the underlying compressible soils. Therefore monitoring of pore pressure increases and dissipation with time is critical to field decisions regarding staging of fill placement and prevention of embankment failure.

Piezometers should be installed between pile caps, within the underlying organic soils, and monitored during fill placement. Any increases in pore pressure that are detected could be an indication of embankment loads not being fully transferred to the pile caps.

6.2.3 Geotextile Strain Gages

Strains within geotextiles can be measured via a series of strain gages. Strain measurements from individual gages can be used to provide an estimate of the overall strain in the geotextile. The estimate of overall strain is converted to a corresponding estimate of stress, which is then compared to design assumptions.

Strategically placed gages within the LTP base reinforcement geotextile can be used to provide indications of whether soil arching is occurring within or above the LTP. Any strains that develop during construction, after much of the embankment has been placed, may indicate that arching is not occurring. Strain gages should be placed in clusters on both the bottom and top of the base reinforcement geotextile, located both over pile caps and midway between pile caps, and aligned in both parallel and perpendicular to embankment centerline. A minimum of two clusters are recommended for purposes of redundancy with other instruments and as backup in the event one or more gages at a clusters fail.

6.2.4 ShapeAccelArrayTM System

The ShapeAccelArray (SAA) system is a cylindrical array of jointed sensors contained in a flexible casing. The sensors consist of orthogonally-aligned accelerometers that are capable of continuously recording displacements in three dimensions. In geotechnical applications, SAA systems are typically used to measure slope movements (similar to an inclinometer) and vertical deflections beneath embankments. MnDOT owns a number of SAA devices that have been used with well known success on various projects, including the TH 2 landslide in Crookston, Minnesota.

SAA systems could be installed horizontally at the bottom, top, and middle of the LTP, as well as beneath surcharges for the purposes of measuring vertical deflections. Any deflections measured could be evaluated to asses efficiency of load transfer to the pile caps and soil arching, as well as converted to estimates of strain within the LTP geosynthetic elements. SAA can also provide vibration data, which may be advantageous considering the

quantity and extent of piles proposed to be driven for the bridge, retaining wall, and pile supported embankment.

6.2.5 Settlement Plates

Settlement plates are simple and economical devices used to measure settlement of compressible soils beneath embankments. Settlement plates are recommended for all surcharge areas.

6.2.6 Vibration Sensors (Geophones) and Noise Sensors

Given the quantity of piles proposed to be driven at the site, a vibration and noise monitoring program should be considered. Such a program should include a pre-condition survey of selected structures for each aspect of construction to be monitored (e.g. vibrations, structure movement during dewatering). The pre-condition survey should include, but not be limited to, a visual documentation of existing structural cracks and a baseline elevation survey of structures and ground monuments. This includes the recommended televising and/or pressure testing of existing utilities.

7.0 General Conditions and Considerations

This report has been prepared in order to assist the City of St. Louis Park and SEH in design of the proposed interchange. The scope is limited to the specific project and location described herein, and the description of the project represents an understanding of the significant aspects relevant to geotechnical characteristics. In the event that any changes in the project layout, as outlined in this report, are planned the conclusions of this report should be reviewed and modified in writing.

The analysis and recommendations submitted in this report are based on the data obtained from specific soil borings drilled through existing public right-of-way areas, and from other available information discussed in this report. This report does not reflect any variations that may occur between these borings, variations that may occur outside of public right-of-way areas, or variations occurring near structural foundations at adjacent private and commercial properties.

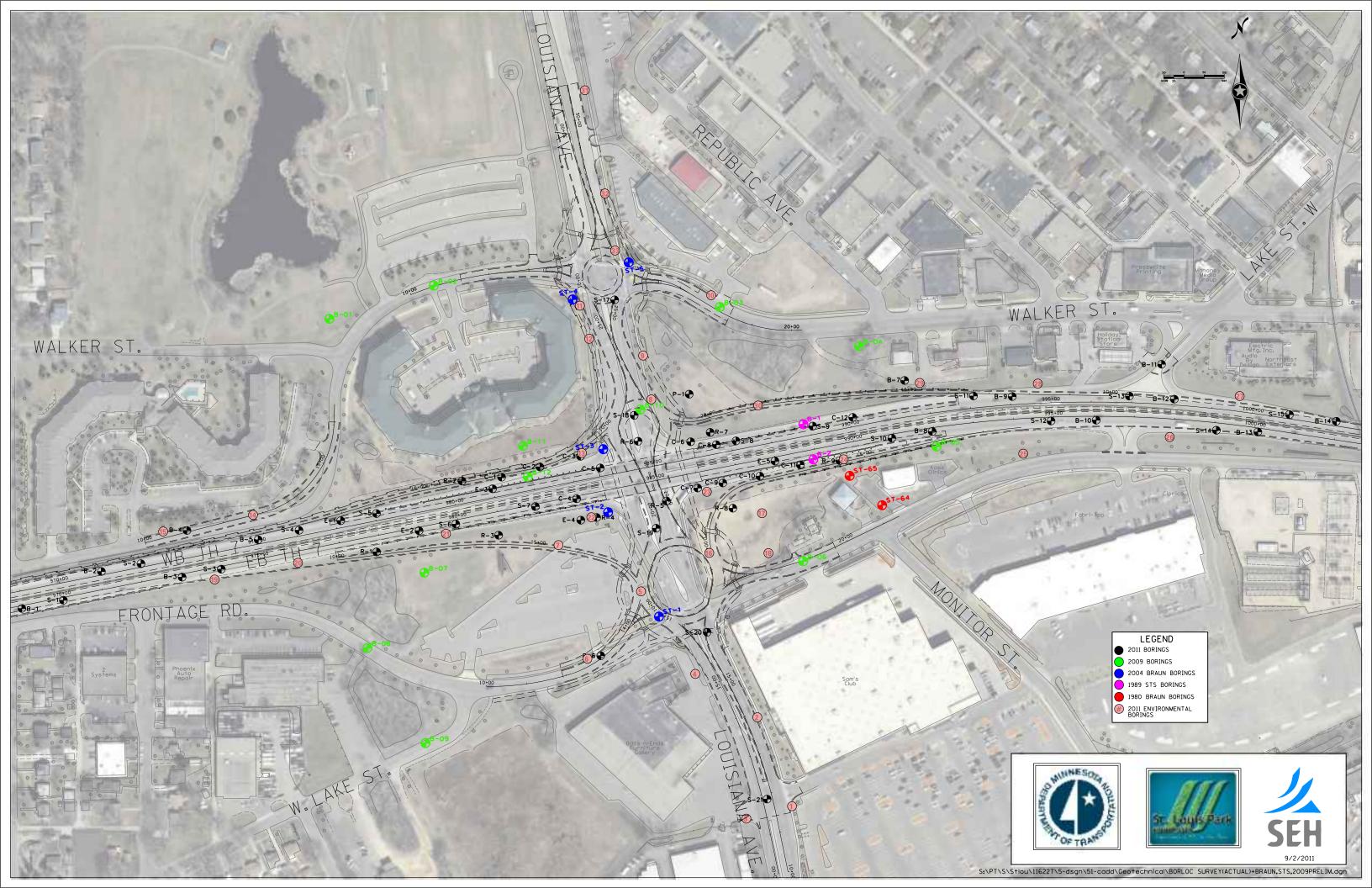
During a subsurface exploration, specific information is obtained at specific locations and at specific times. However, it is a well-known fact that variations in soil and groundwater conditions may not become evident until the course of construction. If variations then become evident, it will be necessary for a re-evaluation of the recommendations in this report after performing on-site observations during construction and noting the characteristics of any variations.

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Appendix A

Boring Location Map



Appendix B

Braun Soil Boring Report, 2011

Results of Soil Borings and **Laboratory Testing**

TH 7 and Louisiana Avenue Reconstruction St. Louis Park, Minnesota

Prepared for

Short Elliott Hendrickson, Inc.

Project BL-09-00745A September 26, 2011

Braun Intertec Corporation



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September 26, 2011

Project BL-09-00745A

Mr. Brent Theroux, PE Short Elliott Hendrickson, Inc. 3535 Vadnais Center Drive St. Paul, MN 55110

Re: Soil Borings and Laboratory Testing

TH 7 and Louisiana Avenue Reconstruction

St. Louis Park, Minnesota

Dear Mr. Theroux:

We have completed the soil borings and laboratory testing requested by Short Elliott Hendrickson, Inc. (SEH) for the reconstruction of Trunk Highway 7 (TH 7) and Louisiana Avenue in St. Louis Park, Minnesota.

Scope of Services

Our work was completed in general accordance with our Proposal for Soil Borings and Laboratory Testing to SEH, dated May 23, 2011 and SEH authorized scope changes.

For the project, our scope of services included the following:

- Site reconnaissance and onsite meeting with SEH to coordinate access.
- Clearance of public utilities.
- Acquiring a MnDOT Trunk Highway Right-of-Way and City of St. Louis Park Public Works Permits.
- Coordination of traffic control in accordance with the approved permits.
- Performing twenty auger borings in pavement areas to nominal depths of 5 to 10 feet below grade.
- Performing fourteen standard penetration test (SPT) borings in road areas to a nominal depth of 20 feet below grade.
- Performing five SPT borings in embankment areas to a nominal depth of 40 feet below grade.
- Performing nine SPT borings in bridge, retaining wall and embankment areas to a nominal depth of 70 feet below grade (or auger refusal).
- Performing one SPT boring in a pond area to a nominal depth of 15 feet below grade.
- Performing rock coring to a nominal depth of 10 feet below auger refusal at the nine 70-foot SPT borings in bridge, retaining wall and embankment areas.

- Performing twelve cone penetration test (CPT) soundings to a nominal depth of 70 feet below grade (or to cone refusal).
- Collecting excess drilling fluid and soil cuttings, placing in steel drums and moving to an onsite location for temporary storage and disposal by the owner.
- Laboratory testing as requested by SEH.
- Preparation of this factual soil boring report.

Documents Provided

SEH provided us with an aerial figure of the project area denoting the boring locations. The figure was titled TH 7/Louisiana and was dated February 2011.

For the purposes of this report, SEH provided us with an untitled soil boring location map reflecting the surveyed boring locations. A copy of this map in included in Appendix A for reference.

Boring Locations and Elevations

As requested, we performed a total of twenty auger borings, twenty-nine SPT borings and twelve CPT soundings. The borings were performed and named as listed in Table 1.

Table 1. Boring and Sounding Summary

Boring Type	Quantity	Location	Unique Name
CPT	12	Embankment/Bridge/Retaining Wall	C-1 to C-12
Auger	20	Pavement Areas	S-1 to S-21*
SPT	5	Embankment Areas	E-1 to E-5
SPT	1	Pond	P-1
SPT with Coring	9	Embankment/Bridge/Retaining Wall	R-1 to R-9
SPT	14	Road	B-1 to B-14

^{*}Note: S-16 was omitted from scope.

The borings were performed at the approximate locations shown on the attached soil boring map provided by SEH.

The boring locations were selected and staked by SEH. Boring coordinates and ground surface elevations at the boring locations were provided by SEH.

Drilling and Sampling

Auger Borings

Auger borings were drilled with truck-mounted core and auger drills with solid stem auger in accordance with ASTM D 1452.

Standard Penetration Test Borings

The SPT borings were drilled with off-road vehicle and truck-mounted core and auger drills equipped with hollow-stem auger in accordance with ASTM D 1586. A 110-pound calibrated hammer was used for the borings. The 110-lb hammer for Drill Rig 7514 was calibrated to 63 percent efficiency on June 10, 2010, the hammer for Drill Rig 7506 was calibrated to 62.2 percent efficiency on January 6, 2011 and the hammer for Drill Rig 7503 was calibrated to 68.5 percent efficiency on November 12, 2010.

During drilling, penetration test samples were taken at 2 1/2- and 5-foot intervals. Thinwall samples were attempted in areas where cohesive or organic soils were encountered at Borings E-1 to E-5 and R-1 to R-9. Actual sample intervals and corresponding depths are shown on the boring logs.

Rock Coring

Coring of the bedrock was performed with off-road vehicle and truck-mounted core drills in general accordance with ASTM D 2113. Rock cores were taken with an NQ-3 core barrel. The bit and casing were first lowered to the bottom of the previously advanced borehole. The core barrel was then lowered into the casing with a wire line, and locked into place. The bit and barrel were advanced by rotating the assembly while applying pressure. Bentonite drilling mud was used to cool the bit and wash cuttings to the surface.

After each 5-foot core run was completed, the core barrel was unlocked from the bit and brought to the surface. The split inner tube was then extruded from the barrel and opened to reveal the core sample. After field classification and logging, the core was packed into a 5-foot wooden storage box.

Cone Penetration Test Soundings

The CPT soundings were performed with an off-road CPT rig by advancing a Vertek piezocone with pore pressure and seismic capabilities. The soundings were performed in accordance with ASTM D 5778. As the cone was advanced, tip resistance (Q_t), sleeve friction (F_s) and pore pressure (U_2) were measured continuously.

Sample Storage

Representative soil and rock samples will remain in our Minneapolis office for a period of 60 days to be available for your examination.

Log of Boring Sheets

Log of Boring sheets for our SPT and auger borings, including rock coring, are included in Appendix A of this report. The logs identify and describe the geologic materials that were penetrated, present the results of penetration resistance tests (for the penetration test borings), laboratory tests performed on penetration test and auger samples retrieved from them, and groundwater measurements. Provided rock coring information includes percent recovery, rock quality designation (RQD), average core length (ACL) and cores breaks per foot.

Strata boundaries were inferred from changes in the penetration test samples and the auger cuttings. Because sampling was not performed continuously, the strata boundary depths are only approximate. The boundary depths likely vary away from the boring locations, and the boundaries themselves may also occur as gradual rather than abrupt transitions.

Cone Penetration Test Sounding Logs

CPT Sounding Logs are included in Appendix B of this report. The CPT sounding logs report the tip resistance, sleeve friction and pore pressure that was measured continuously by the cone as it was advanced. The normalized friction ratio, undrained shear strength, and soil behavior type were calculated from the raw data. The graphical SBT is based upon the relationship between normalized tip resistance and friction ratio (Robertson 1990). Direct observation of the soils does not occur with CPT soundings.

Soil and Rock Classification

The soils encountered were visually and manually classified in general accordance with the MnDOT Triangular Textural Soil Classification System. A chart explaining the classification system is attached. Supplemental to the chart, soil containing more than 50 percent gravel by weight was classified as Gravel. Classification of recovered rock cores was based on US. Army Corps of Engineers EM 1110-1-2908.

Laboratory Testing

Testing Performed and Procedures

Laboratory testing was performed as requested by SEH. For Borings E-1 to E-5 and R-1 to R-9, testing was performed in general accordance with the MnDOT Specifications for Subsurface Investigation (except as listed below). Tests performed included moisture content, organic content, sieve analysis, Atterberg limits, hand penetrometer, unconfined compression, unconsolidated-undrained triaxial shear (U-U test), consolidation, standard Proctor and R-value tests on recovered jar, thinwall and bag samples (of auger cuttings). Tests were performed in accordance with MnDOT or ASTM procedures and as referenced on the specific test reports.

The tests are shown or noted on the right side of the Log of Boring Sheets, across from the associated sample. Moisture content, dry density and cohesion results listed on the Log of Boring sheets are typically derived from the unconfined compression test results. Where only a U-U test was performed (on a thinwall sample) due to limited sample recovery or quality, the moisture content, dry density and cohesion included on the Log of Boring Sheet were derived from the U-U test.

The sieve analysis, Atterberg limits, unconfined compression, U-U test, consolidation, standard Proctor and R-value tests test results are shown graphically on separate sheets included in Appendix C of this report.

Exceptions

As noted on the boring logs, laboratory testing was not performed on several borings in general accordance with the MnDOT Specifications for Subsurface Investigation (or as requested by SEH) due to contamination within the recovered samples. Borings where this situation occurred included Borings R-1, R-2 and R-3.

Where unconfined compression and U-U tests were both requested on a thinwall sample, the U-U test was performed first, and the unconfined compression test was not performed if the remaining sample was insufficient for testing. A requested consolidation test was also not performed on the thinwall sample from 29 to 31 feet at Boring R-4 due to insufficient sample after unconfined compression and U-U testing.

Testing (moisture content) was also not performed in accordance with the MnDOT Specifications for Subsurface Investigation on a few samples from Borings R-1 and R-2 as a result of the samples being accidentally discarded prior to completion of these tests.

Groundwater Observations and Borehole Abandonment

The drillers checked for groundwater as the penetration test borings were advanced. The borings were typically checked again for the presence of groundwater after auger withdrawal, unless mud rotary drilling methods or coring was performed. The boreholes were then backfilled with cuttings and/or bentonite grout after completion in accordance with Minnesota Department of Health regulations.

As requested by SEH, excess soil cuttings and drilling fluid generated during completion of the borings was collected and placed in steel drums. The drums were labeled and dated and moved to the City owned parking lot on the southwest corner of TH 7 and Louisiana Avenue. Braun Intertec holds no responsibility for the storage or disposal of the cuttings after collection and placement at the designated storage location.

Groundwater Fluctuations

Groundwater measurements were made under the conditions reported herein and shown on the exploration logs, and interpreted in the text of this report. It should be noted that the observation period was relatively short, and groundwater can be expected to fluctuate in response to rainfall, flooding, irrigation, seasonal freezing and thawing, surface drainage modifications and other seasonal and annual factors.

Level of Care

In performing our services, Braun Intertec has used that degree of care and skill ordinarily exercised under similar circumstances by reputable members of our profession currently practicing in the same locality. No warranty, express or implied, is made.

General

Please refer to the attached report for a detailed summary of our procedures and results. We appreciate the opportunity to be of service to you on this project. If you have any questions regarding this report, please contact Josh Van Abel at 952.995.2310 or Matt Ruble at 952.995.2224.

Sincerely,

BRAUN INTERTEC CORPORATION

Joshua J. Van Abel, PE

Associate - Senior Engineer

Matthew P. Ruble, PE

Principal Engineer

Appendix A:

Soil Boring Location Map (Provided by SEH)

Log of Boring Sheets B-1 to B-14 (SPT)

Log of Boring Sheets E-1 to E-5 (SPT)

Log of Boring Sheet P-1 (SPT)

Log of Boring Sheets R-1 to R-9 (SPT)

Log of Boring Sheets S-1 to S-21, excluding S-16 (Auger)

Appendix B:

Cone Penetration Test Results C-1 to C-12

Appendix C:

Grain Size Accumulation Curves (59 Sheets)

Atterberg Limits Result (1 Sheet)

Consolidation Test Reports (6 Sheets)

Unconfined Compression Test Reports (15 Sheets)

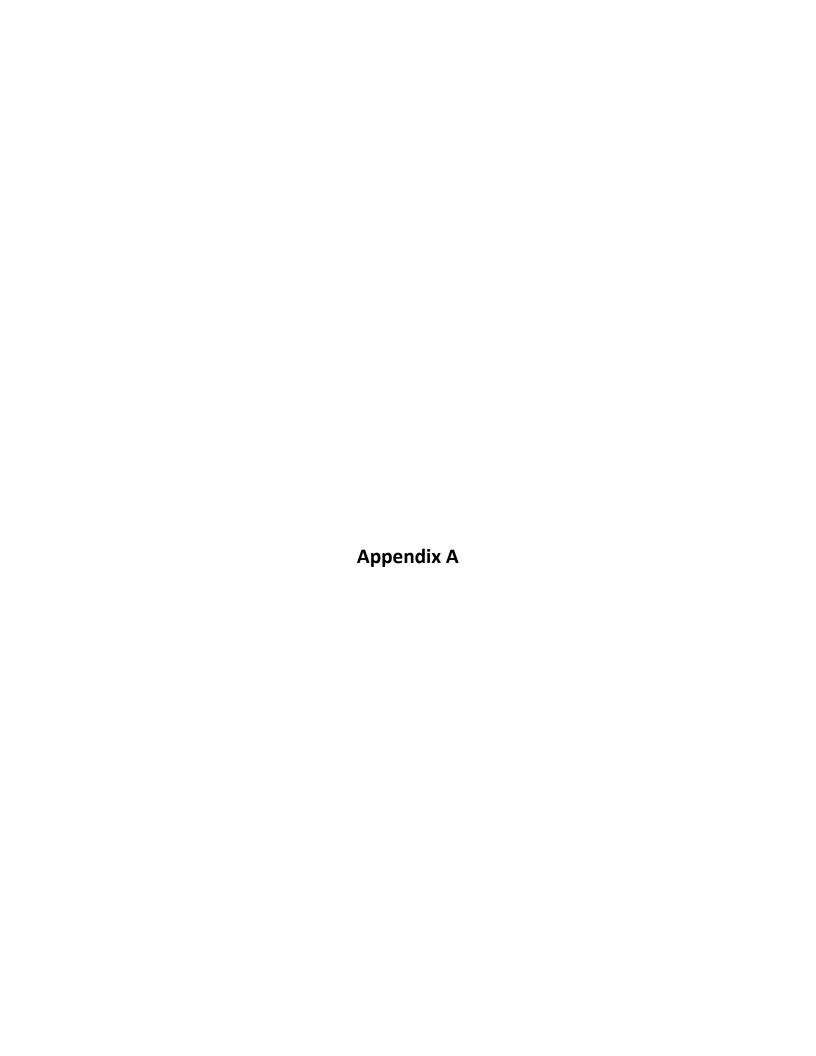
Unconsolidated-Undrained Test Reports (8 Sheets)

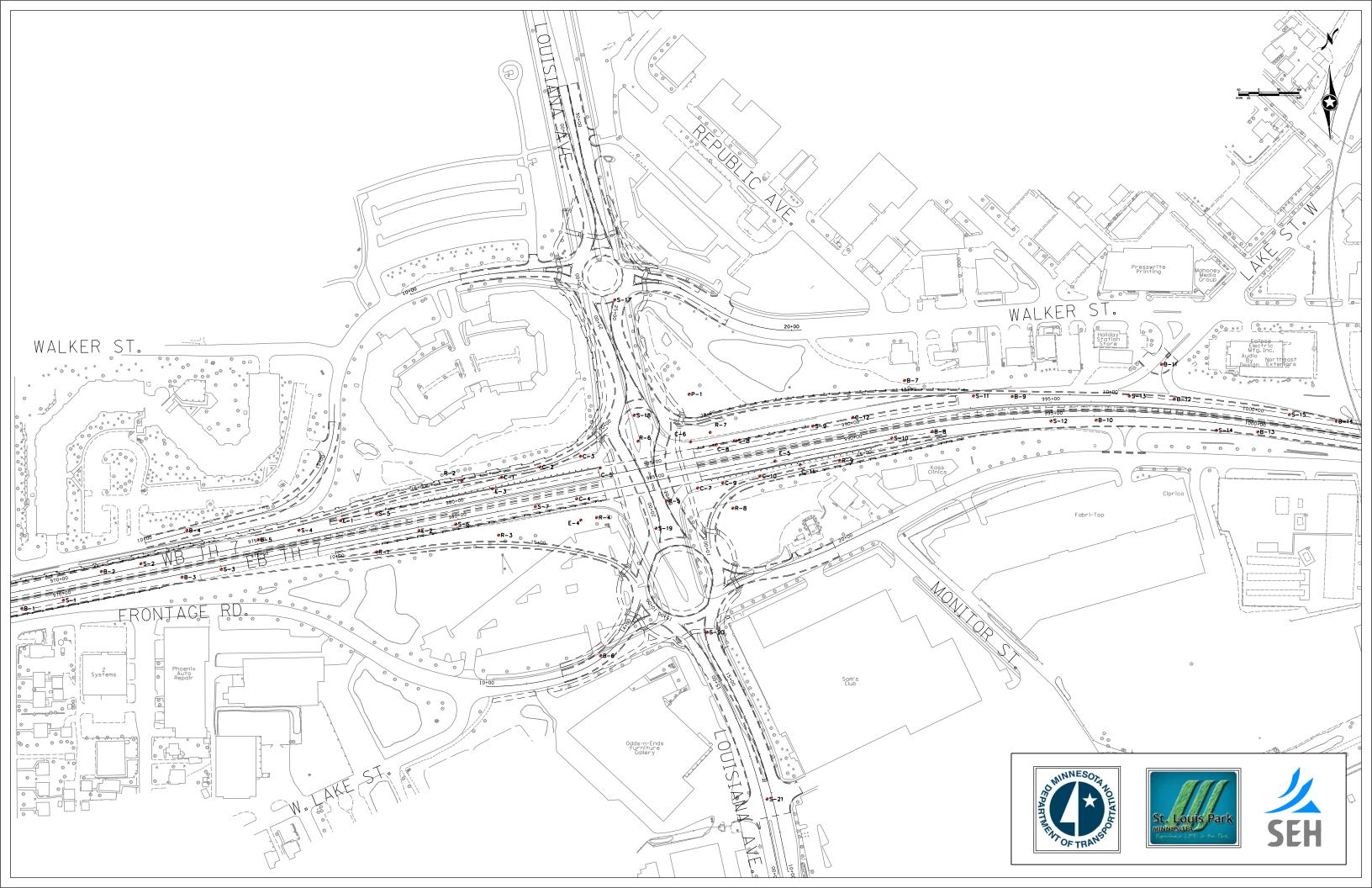
Moisture-Density Relationship Reports (Standard Proctor – 2 Sheets)

Material Test Reports (R-Value – 2 sheets)

Descriptive Terminology of Soil

Soil Boring Rpt

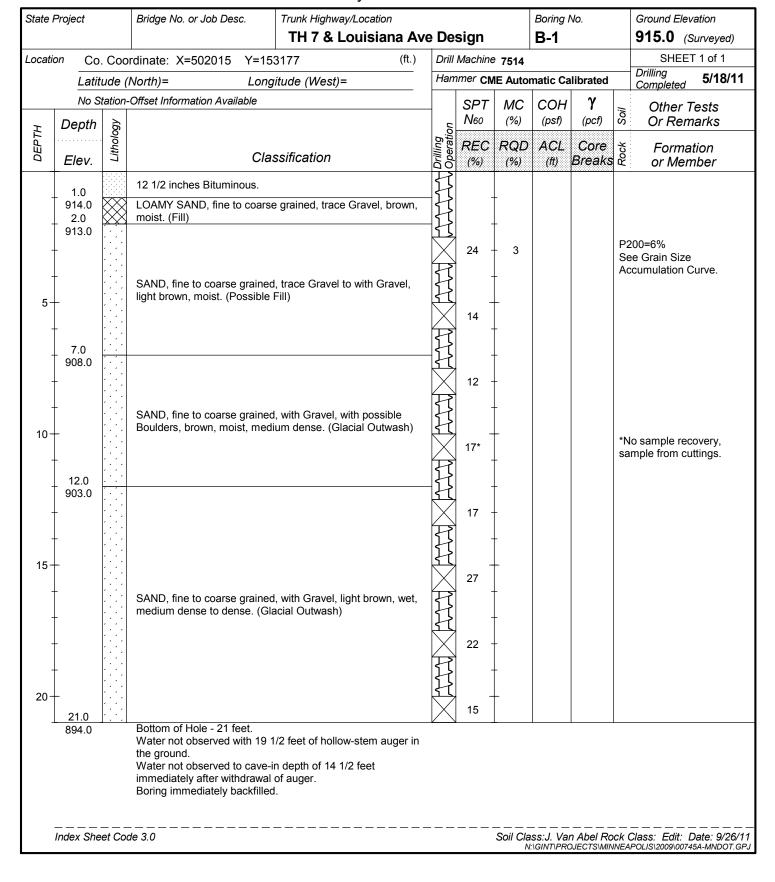






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20-	21.0	× · · × · · × · · × · · × · · × · · × · · ×	SANDY LOAM, non plastic, waterbearing, medium dense			\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	16	<u>-</u>				
T	884.9	1	Bottom of Hole - 21 feet. Water observed at 14 feet wi auger in the ground. Water not observed to cave-i after withdrawal of auger. Boring immediately backfilled	n depth of 17 feet im		<i>V</i>	_		1	1	1	
- I	 Index She	 et Cod	 de 3.0		. – – – –							



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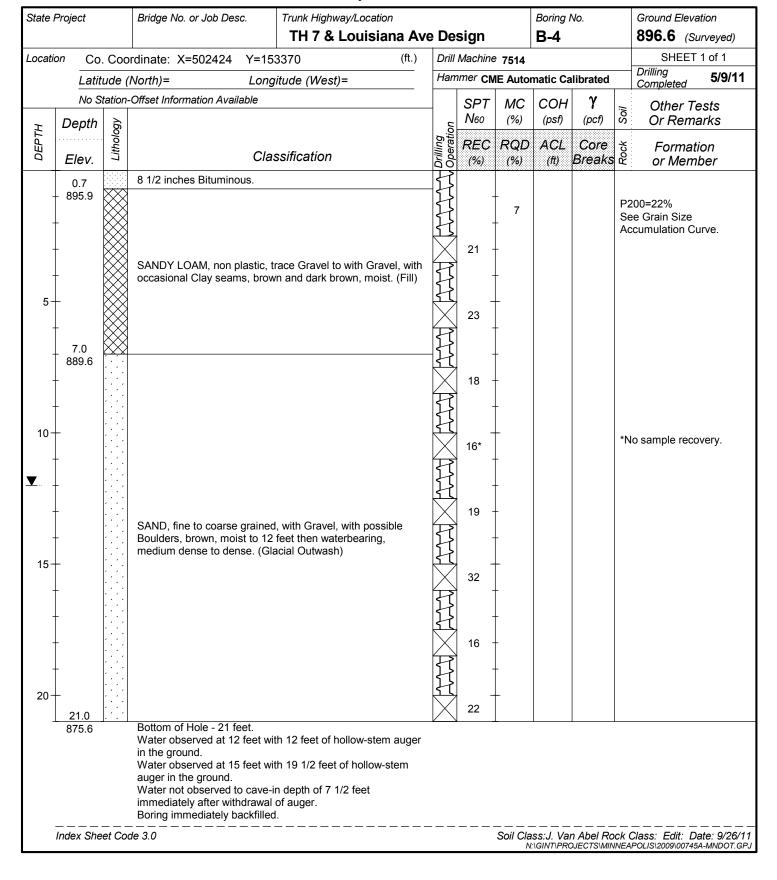


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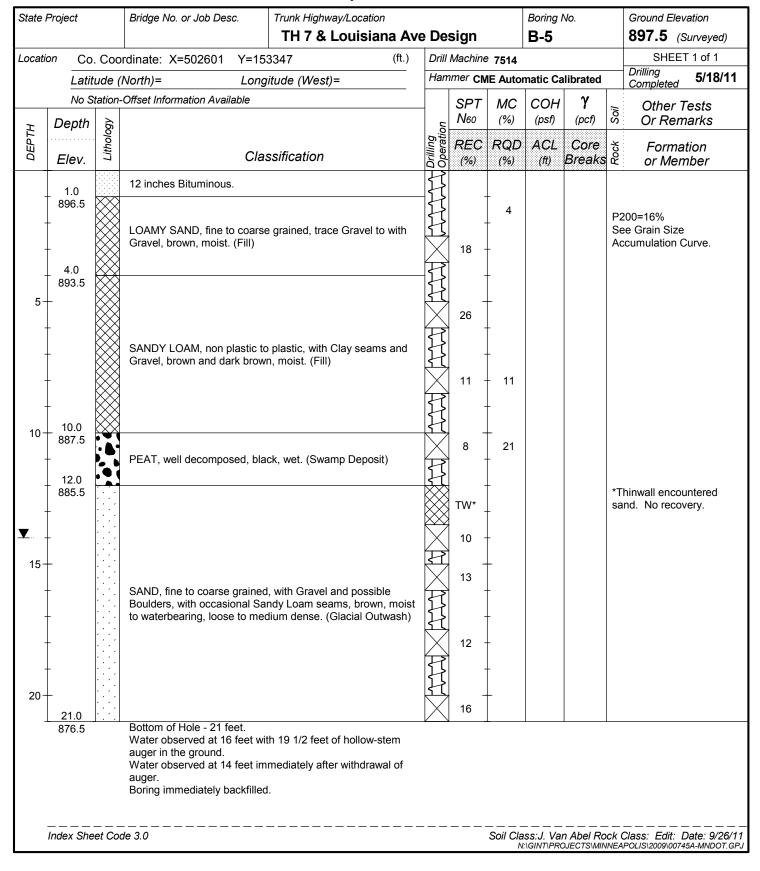






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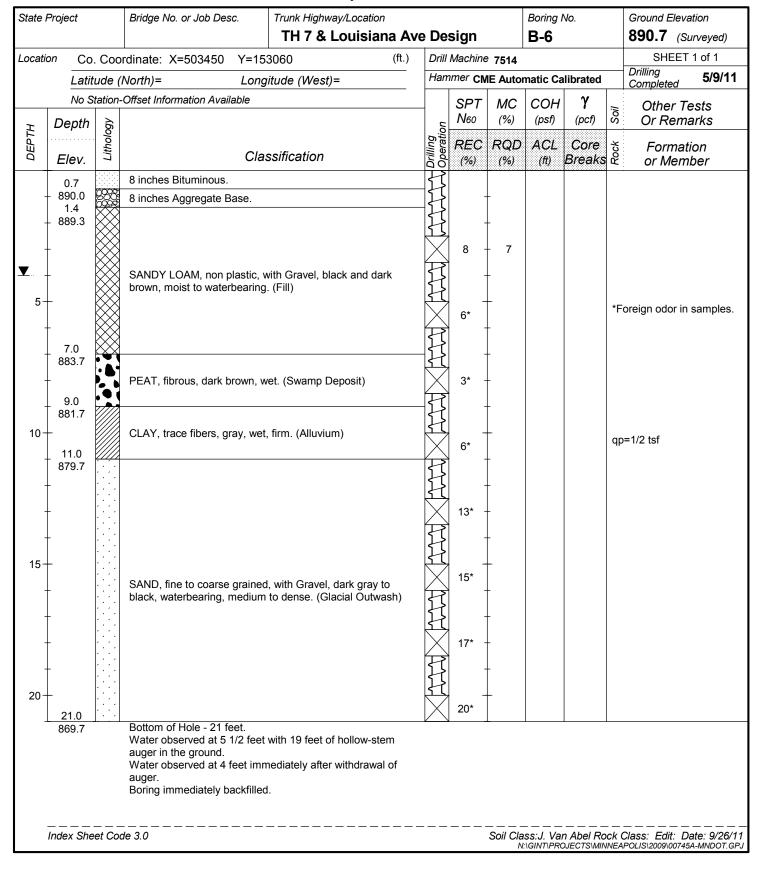






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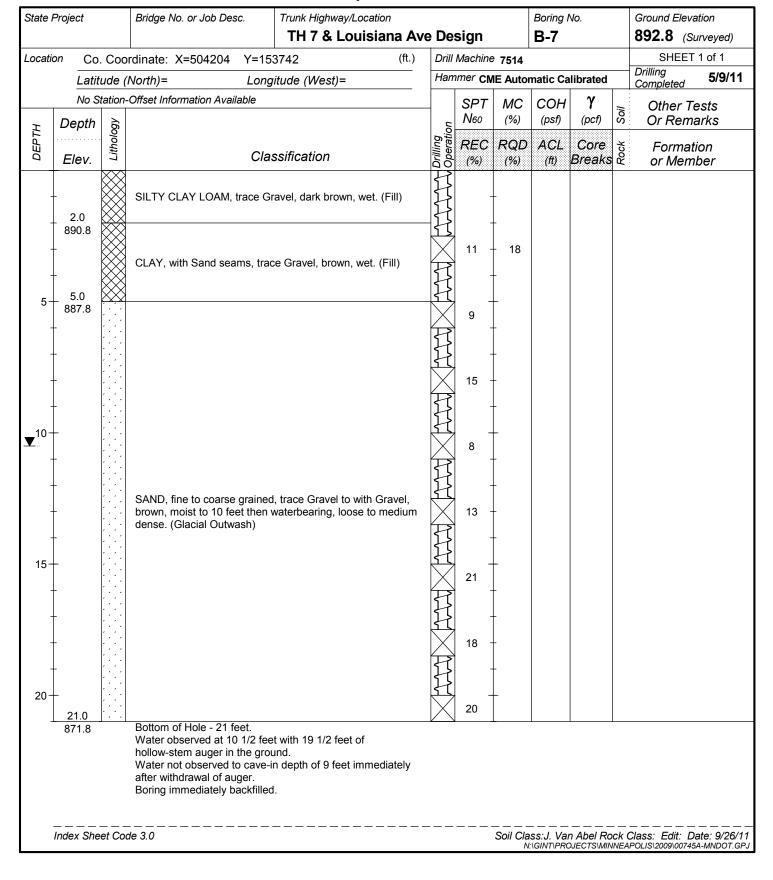






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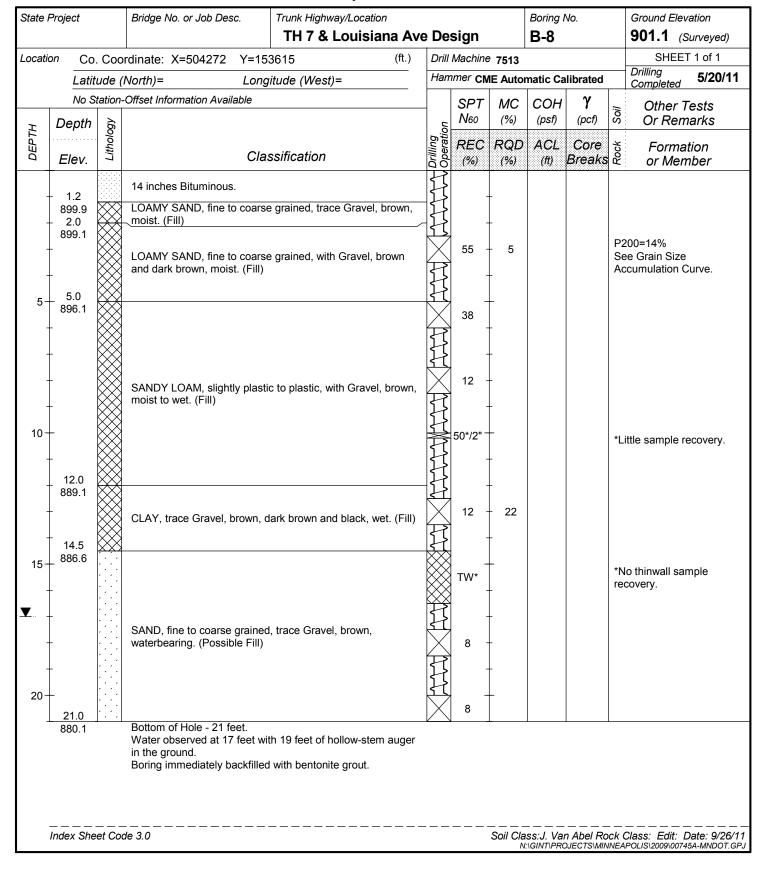






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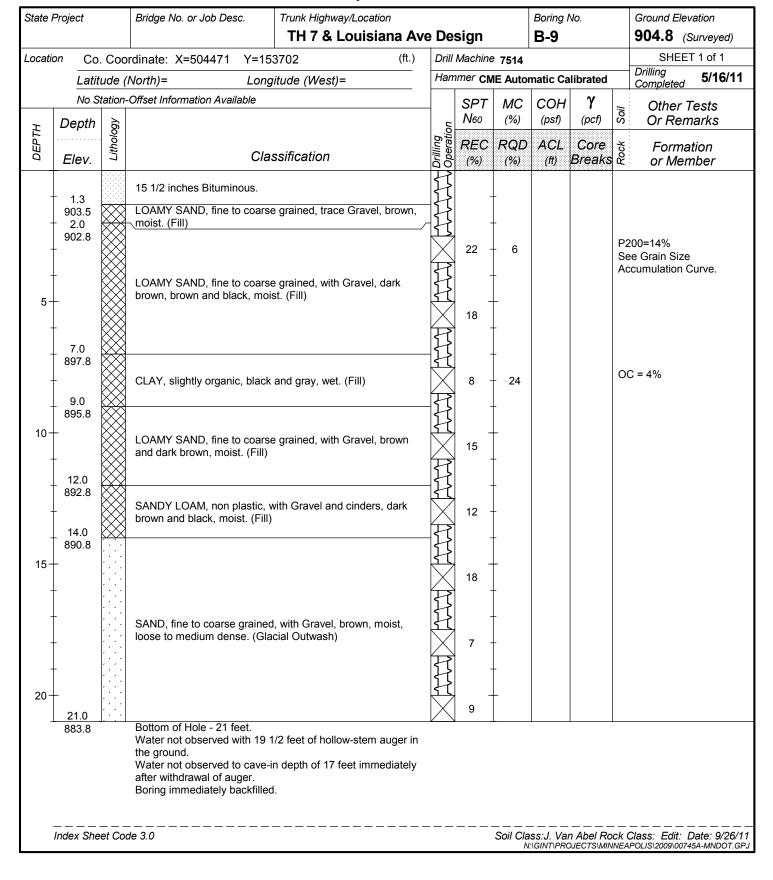






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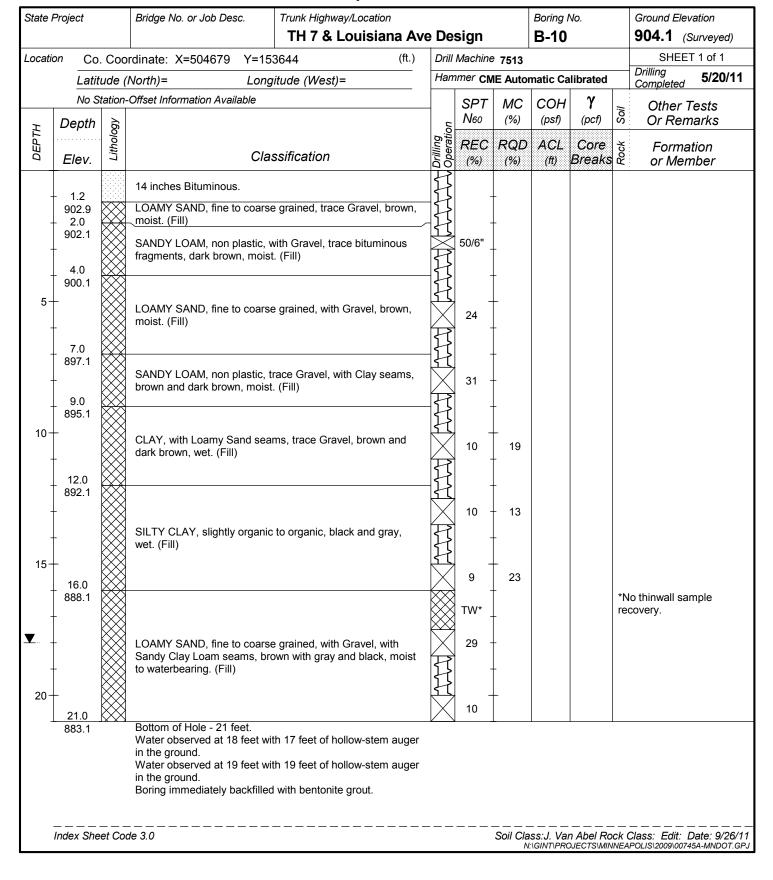






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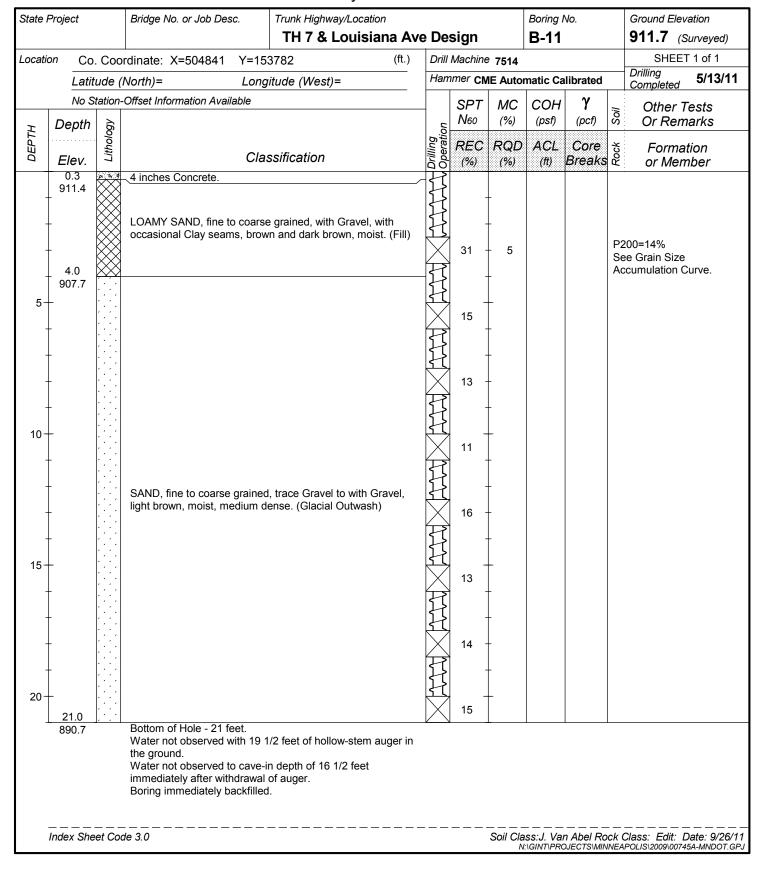






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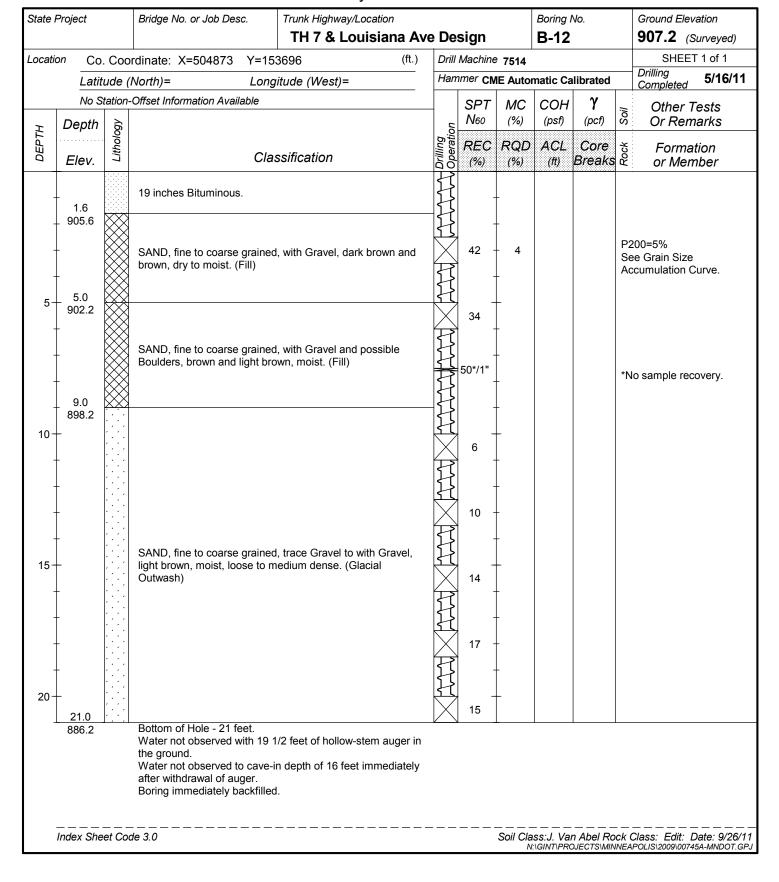






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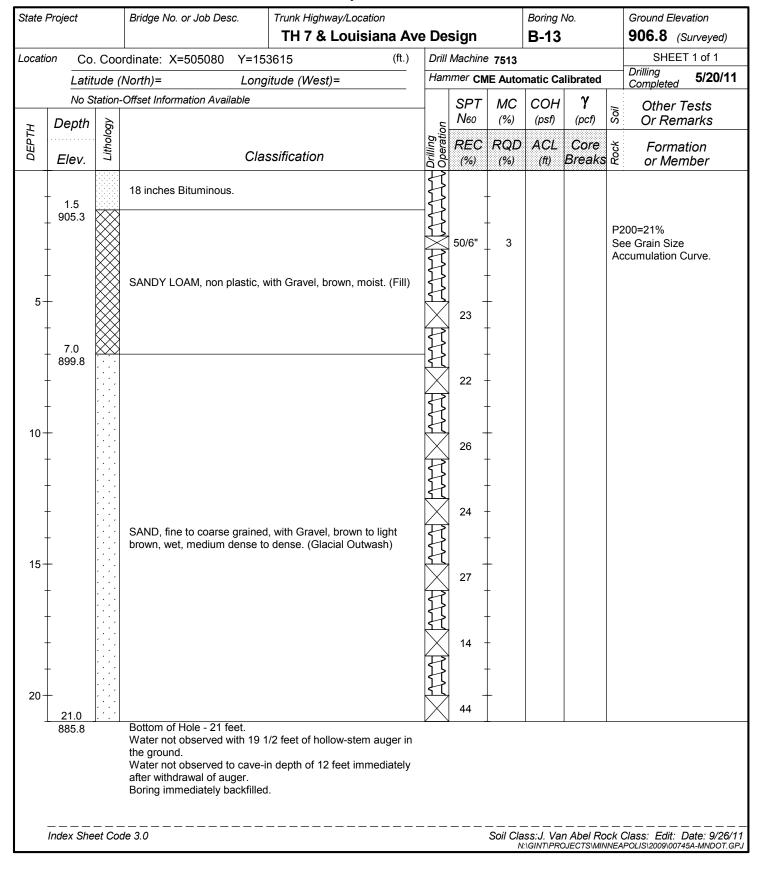






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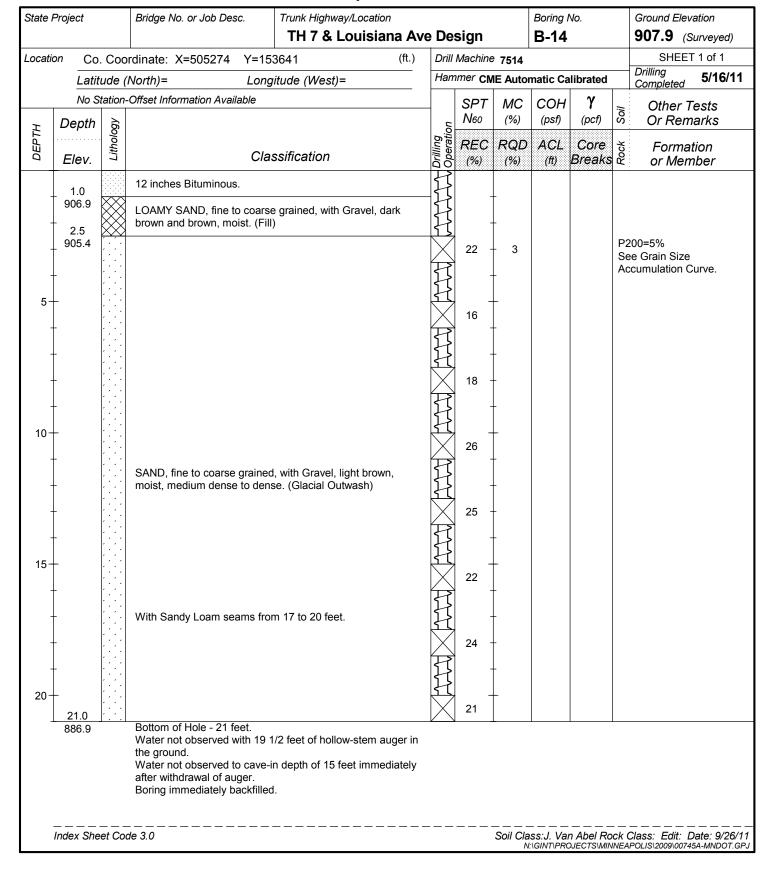






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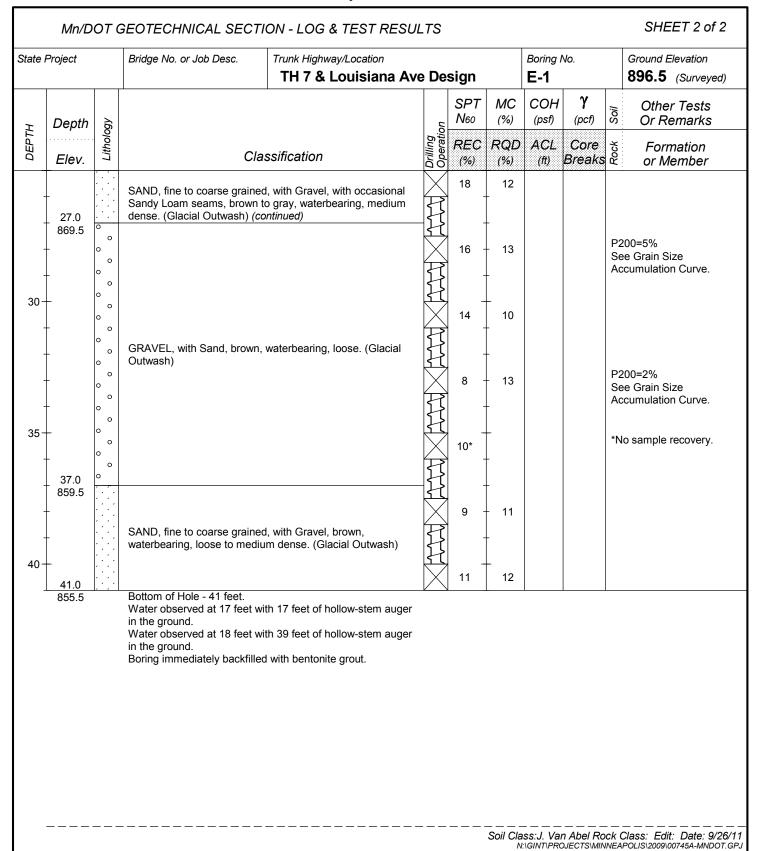


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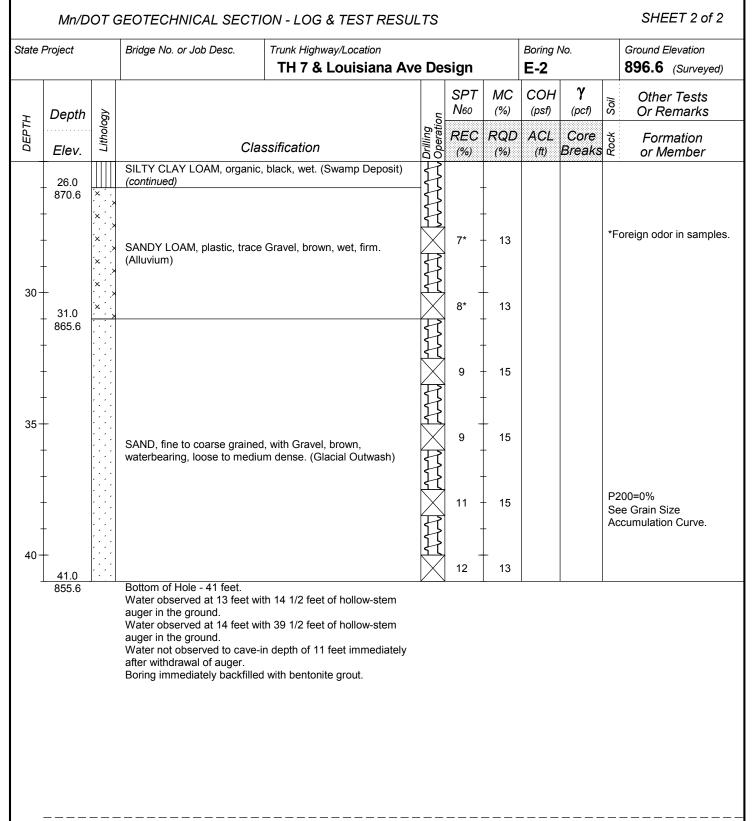


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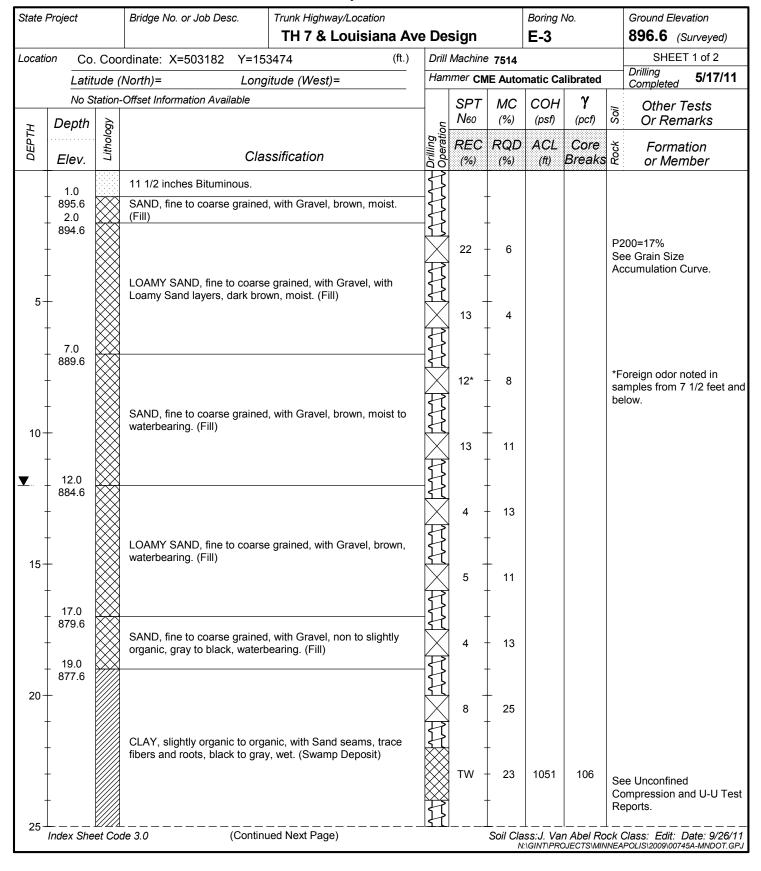






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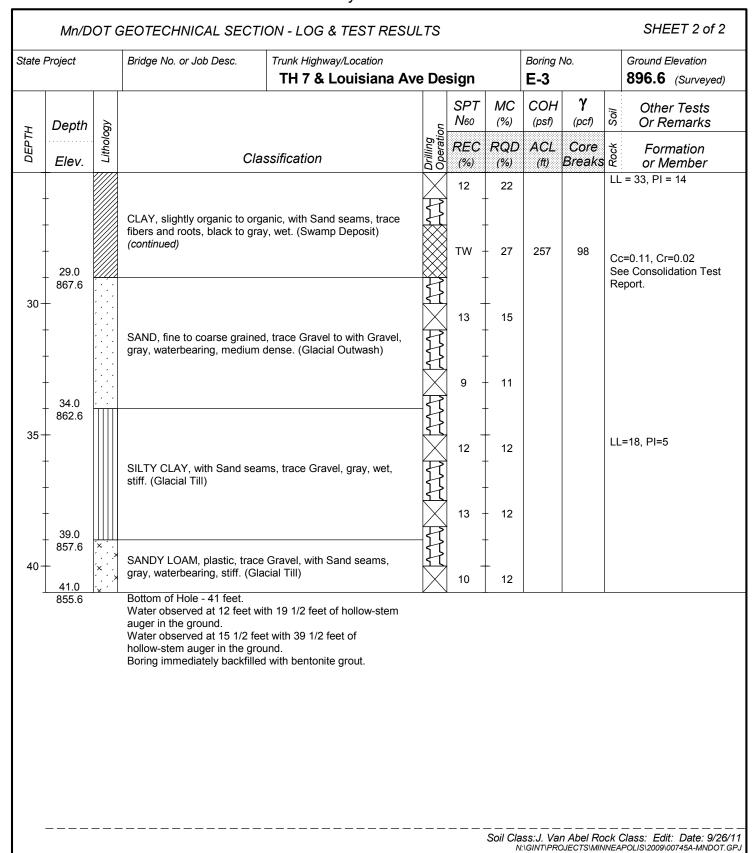






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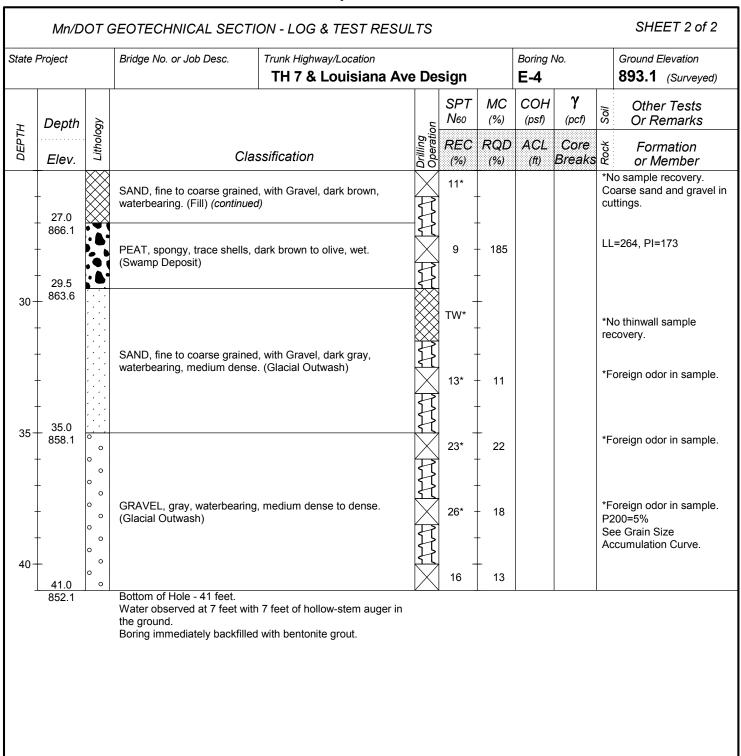
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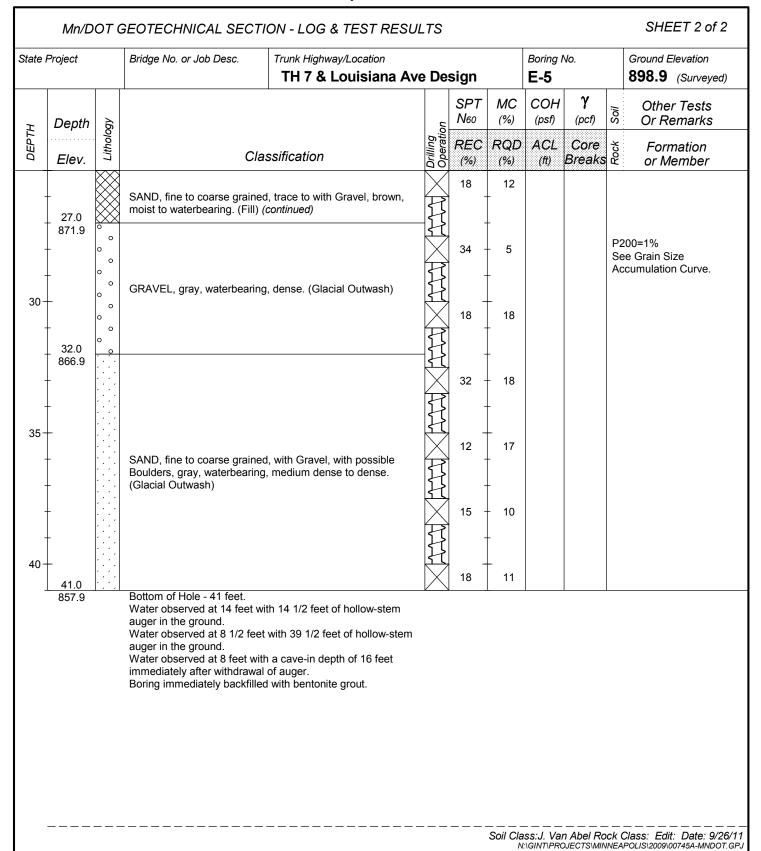


State F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve D	nniee		Boring E-5	No.		Ground Elev 898.9 (S	
Locatio	on Co	Coo	 			ll Machin	00 7544	L-3			SHEET	
Localic								matic Ca	alibrated		Drilling	5/18/11
			North)= Long Offset Information Available	gitude (West)=	-				l		Completed	
			Onset information Available			SPT N60	(%)	COH (psf)	(pcf)	Soil	Other T Or Rem	
DEРТН	Depth	Lithology	Cla	ssification	Drilling	REC	RQD		Core Breaks		:	tion
7	Elev.	7		SSIIICALIOII	20	3 (%)	(%)	(ft)	Breaks	œ	or Mem	ber
1	0.9		11 inches Bituminous.		_{	>	1					
-	898.0 2.0 896.9		LOAMY SAND, fine to medi- brown, moist. (Fill)	um grained, trace Gravel,	1	>	4					
	- 4.0		LOAMY SAND, fine to coars and dark brown, moist. (Fill)	e grained, with Gravel, brown	X	42	9					
5-	894.9 -				-}	>	‡ <u> </u>					
	-				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	32	7					
▼	-		SANDY LOAM, slightly plast Clay seams, dark brown and	ic, with Gravel, with occasional brown, moist. (Fill)	<u></u>	23	7					
10-	-				4	>	+					
	12.0				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	28	6					
	886.9 - -				\ <u>\</u>	11	7					
15-	-				\ \ \	5	14					
-	-		SAND, fine to coarse graine moist to waterbearing. (Fill)	d, trace to with Gravel, brown,	\ \ \ \	4	+ + 15 +			Se	200=9% ee Grain Size ccumulation C	urve.
20	-		With trace black Clay at 20 t	eet.	\ \ \ \	2	18					
	-				\ \ \	10	14					
		$ \rangle\rangle$	With gray Clay seam at 25 f	eet.		>						
25 -	Index She	ı∠∠∖ı et Cod	de 3.0 (Contir	ued Next Page)		-					— — — — — — — — — — — — — — — — — — —	



UNIQUE NUMBER

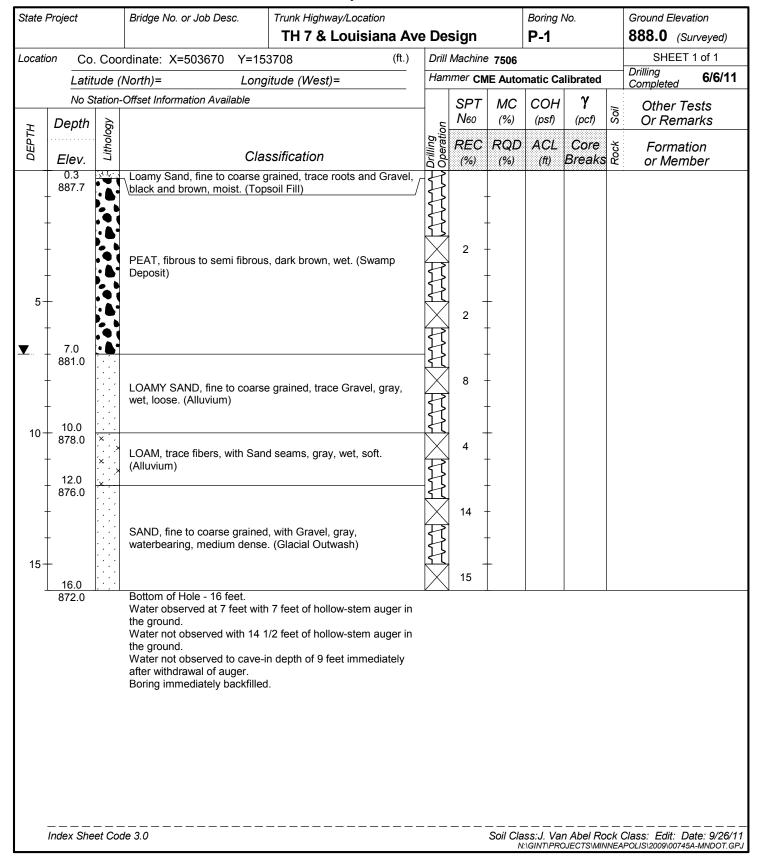






UNIQUE NUMBER

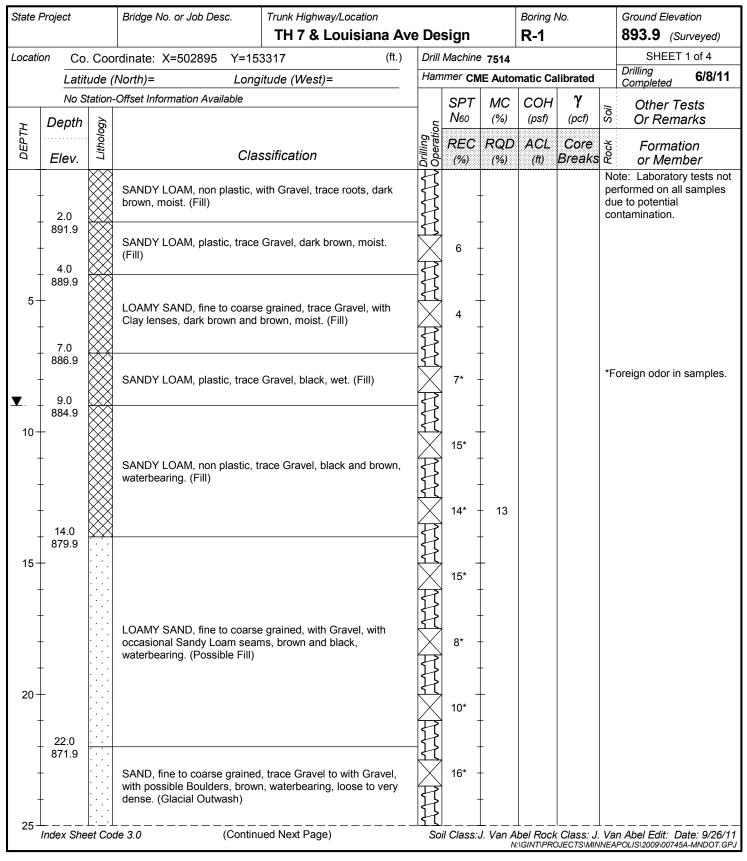






UNIQUE NUMBER

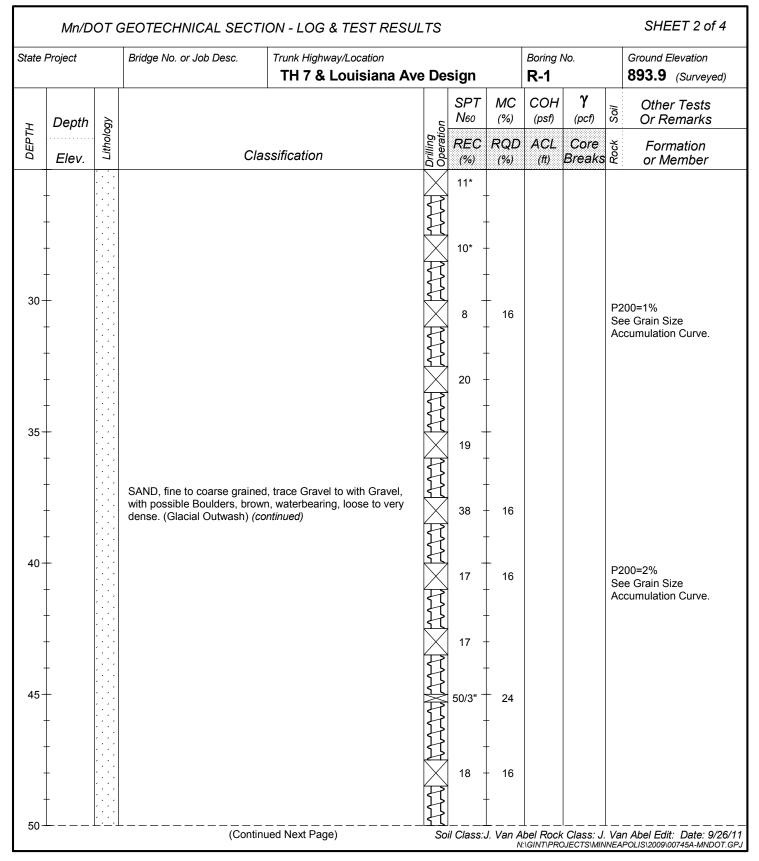






UNIQUE NUMBER







UNIQUE NUMBER



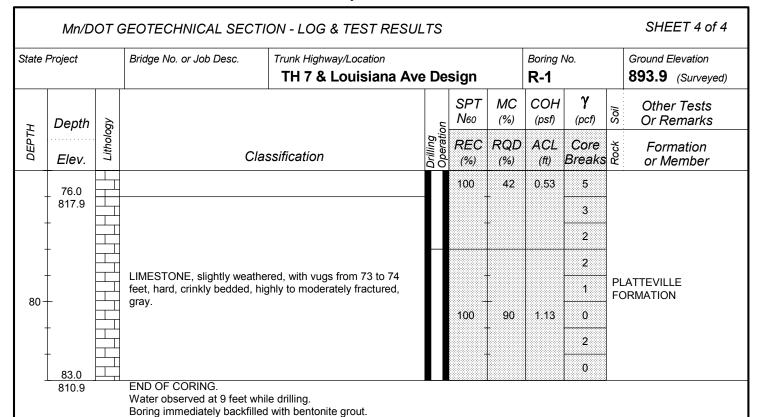
tate I	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	Vo.		Ground Elevation 893.9 (Surveyed)
I	Depth	ogy			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	CI	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	- 54.0		SAND, fine to coarse grains with possible Boulders, brodense. (Glacial Outwash) (G	ed, trace Gravel to with Gravel, wn, waterbearing, loose to very continued)	XXXXXX	20	11				
55-	839.9 - - 57.0		CLAY, with frequent Sand s brown, wet, very stiff. (Glac	seams and lenses, gray and ial Till)		35	21			LI	_=24, PI=15
60 -	836.9	X	SANDY LOAM, non plastic, (Glacial Outwash)	, brown, waterbearing, dense.		31	24			Se	200=31% ee Grain Size ccumulation Curve.
65 -	831.9		SAND fine to coarse grains	ed, with Gravel and possible	1111111 X 111	23	37				
- 70 - -	73.0		Boulders, brown, waterbear (Glacial Outwash)	ring, dense to very dense.		50/5" - -	20			Aı	uger refusal at 73 feet,
-	73.0 820.9			nered, with vugs from 73 to 74 ntensely to highly fractured, dark	15				6	SV Al Pl	witched to rock coring. pparent Top of Bedrocl LATTEVILLE ORMATION



UNIQUE NUMBER



U.S. Customary Units

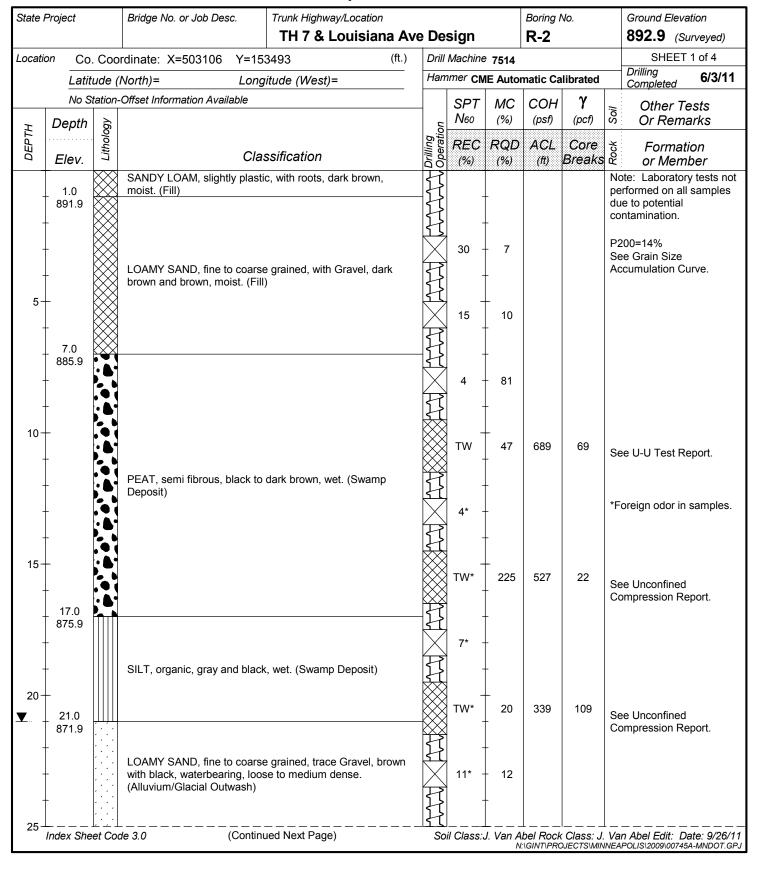


Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER







UNIQUE NUMBER



State I	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring I	No.		Ground Elevation 892.9 (Surveyed)
Ţ.	Depth	ygv			no	SPT N ₆₀	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cl	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
	-				X	16*	12				
_	-		LOAMY SAND, fine to coar with black, waterbearing, lo (Alluvium/Glacial Outwash)	se grained, trace Gravel, brown ose to medium dense.	}	-	_				
-	29.0		(Alluvium/Olacial Outwash)	(continued)	X	8* -	18				
30-	863.9					_	_				
_	-				X	4 -	23				
_	-				1	-	_				
-	-				X	9 -	20				
35-	-				}	9	20			P2	200=1%
-	-				F	9 -					ee Grain Size ccumulation Curve.
-	-				11	11 -	16				
_	-		SAND, fine to coarse graine	ed, trace Gravel to with Gravel,	}	-	_				
40-	-		Outwash)	oose to medium dense. (Glacial	\$1 \$1	- 14	19				
-	-				1	-	_				
-	-	· · · · · · · · · · · · · · · · · · ·				15 -	_				
45	-				 	-					
45-	-					16	_				
_	-				} }	-	_				
_	_				X	17 -	_				
50-						-					



UNIQUE NUMBER



ate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring N R-2	Vo.		Ground Elevation 892.9 (Surveyed)
_	Depth	gy			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPIH	Elev.	Lithology	CI	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
55	- 69.0 823.9		SAND, fine to coarse grains brown, waterbearing, very loutwash) (continued)	ed, trace Gravel to with Gravel, oose to medium dense. (Glacial	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	20	16			Se	200=6% ee Grain Size ecumulation Curve.
70 -			SAND, fine to coarse grain dense. (Glacial Outwash)	ed, brown, waterbearing, very		52 -	19			Se	200=7% ee Grain Size ccumulation Curve.
-	74.0 818.9	× .	SANDY LOAM slightly plas	stic, with Gravel, Limestone and	_}}	-	-			*5	Switched to rock coring



UNIQUE NUMBER



U.S. Customary Units

	וויויו	0, 0	GEOTECHNICAL SECTION	on Loo a reorned	0270					SHEET 4 of 4
State	Project		Bridge No. or Job Desc.	Trunk Highway/Location				Boring I	Vo.	Ground Elevation
				TH 7 & Louisiana A	ve De	sign		R-2		892.9 (Surveyed)
7	Depth	gy			u	SPT N60	MC (%)	COH (psf)	γ (pcf)	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Clas	ssification	Drilling Operation	REC	RQD (%)	ACL (ft)	Core Breaks	Formation or Member
_	817.9		\dense. (Glacial Till)						4	Apparent Top of Bedrock
	_		LIMESTONE, slightly weather highly fractured, gray.	red, hard, crinkly bedded,					2	
-	78.0 814.9	\perp				100	55	0.91	5	PLATTEVILLE FORMATION
-	814.9	\perp							0	
80-	_	井			Ш				1	
	-								0	DIATTE VILLE
-	_		LIMESTONE, slightly weather moderately to slightly fracture			-			1	PLATTEVILLE FORMATION
-	_	井				100	98	1.22	2	
-	_								0	
85-	85.0								1	

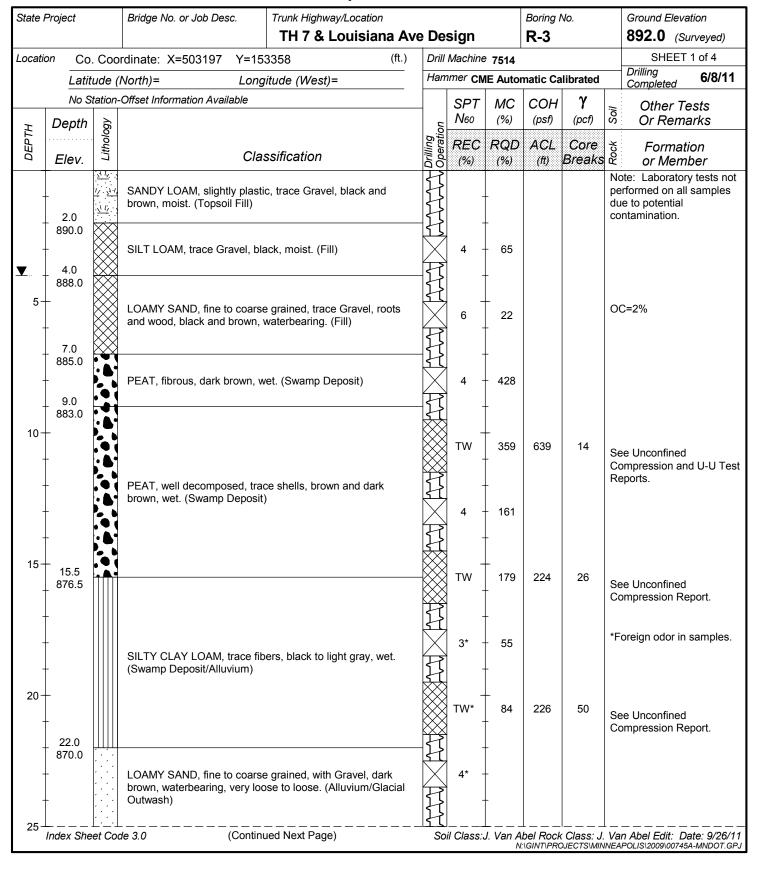
Water observed at 21 feet while drilling.
Boring immediately backfilled with bentonite grout.

Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER







UNIQUE NUMBER



lale F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring I	Vo.		Ground Elevation 892.0 (Surveyed)
Į	Depth	ЛВс			l uo	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cla	essification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	27.0		LOAMY SAND, fine to coars brown, waterbearing, very loo Outwash) (continued)	e grained, with Gravel, dark ose to loose. (Alluvium/Glacial	X 17	7*					
 	865.0				1	6* -	20				
30					\{\f\}	4* -	18				
+					1	5 -	- 16				
35-	-				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	- 7 	17			Se	200=1% ee Grain Size ccumulation Curve.
+			SAND, fine to coarse grained brown, waterbearing, very loo Outwash)	d, trace Gravel to with Gravel, ose to medium dense. (Glacial	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	13 -	15				
40 +					1	14 -	19				
+					\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	12 -	13				
45 -					1	11 -	13				
-					1	13 -	14				



UNIQUE NUMBER



State I	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring I	Vo.		Ground Elevation 892.0 (Surveyed)
Ŧ.	Depth	Убс			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cla	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks		
-	-		SAND, fine to coarse graine brown, waterbearing, very lo Outwash) (continued)	d, trace Gravel to with Gravel, lose to medium dense. (Glacial	XXXXXXX	16	16			Se	00=6% e Grain Size cumulation Curve.
55-	55.0 837.0 				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	31* -	18			*Li	ttle sample recovery.
60-	-		SAND, fine to coarse graine Boulders, brown, waterbeari	d, with Gravel and possible ng, dense. (Glacial Outwash)	11111111111111111111111111111111111111	38* - -	17			*Lii	ttle sample recovery.
65-	-				THE THE	35 -	19				
70-	- _ 70.0 _ 822.0 -		With Shale seam at 71 feet. LIMESTONE, slightly weath		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-			6 4	sw X// Ap PL	ger refusal at 70 feet, itched to rock coring. parent Top of Bedrock ATTEVILLE RMATION
-	- 75.0		intensely to highly fractured,	dark gray to gray.		100	20	0.50	6 6 5		



UNIQUE NUMBER



U.S. Customary Units

State	tate Project Bridge No. or Job I		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	Vo.		Ground Elevation 892.0 (Surveyed)
ı	Depth	gy			uc.	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cl	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
	817.0		LIMESTONE, slightly weath highly to moderately fractur With Shale seam at 77 feet			100	90	1.13	0 1 4 0	1	LATTEVILLE DRMATION

Water observed at 4 feet while drilling.

Boring immediately backfilled with bentonite grout.

Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



tate P	Project		Bridge No. or Job	Desc.	Trunk Highway/Location TH 7 & Louisia		e:	sign		Boring I	VO.		Ground Elev 895.3 (S	
ocatio	n Co.	Coo	rdinate: X=5034	140 Y=				Machine	 ₹ 7514				SHEET	Γ 1 of 4
			North)=		ngitude (West)=		am	mer CN	IE Autor	natic Ca	librated		Drilling Completed	5/25/1
			Offset Information	Available				SPT N ₆₀	MC (%)	COH (psf)	γ (pcf)	Soil	Othor T	
DEPTH	Depth Elev.	Lithology		С	lassification	Drilling	Operation	REC (%)			Core Breaks		1	tion
	2.0		SANDY LOAM, p	olastic, sli	ghtly organic, black, moist.	5	7777	-	17					
5-	893.3		Gravel and roots	OAM, with	slightly organic layers, tra ark brown and black, mois	ace st to	1	5 -	- 13					
+			wet. (Fill)			\ 	777	6 -	26					
10-	7.5 887.8						777777	4 - - 8 -	- 21 - 14					
+			LOAMY SAND 1	ine to coa	rse grained, with Gravel, b	prown to	1	2* -	- 18			*F	Foreign odor ir	n sample.
15	-		dark brown, wate With Clay layer a	erbearing.	(Fill)		\ \ \ \ \	4	19					
 - -						\frac{\x}{\x}	1 777	7 -	9					
20 -	22.0 873.3						1 7 7 7	- 11* -	17			*F	Foreign odor ir	n sample.
†			SAND, fine to co waterbearing. (Fi		ed, trace Gravel, dark bro	wn,	777	10 -	- 17					



UNIQUE NUMBER



State I	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	Vo.		Ground Elevation 395.3 (Surveyed)
Н	Depth	ogy			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	CI	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	27.0		SAND, fine to coarse grain- waterbearing. (Fill) (continu	ed, trace Gravel, dark brown, ed)		11	20			at 2: take	e: Switched to 3" casing feet. No thinwalls we in due to use of casing porehole advancement
_	868.3 - - 30.0		PEAT, spongy, trace shells (Swamp Deposit)	s, organic, dark brown, wet.	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	14 -	104			29 1	e: Thinwall taken from /2 to 31 1/2 feet in et auger boring.
30-	865.3 -		SILTY CLAY LOAM, organ Deposit/Alluvium)	ic, olive to gray, wet. (Swamp	1	9	79 -	313	52		Unconfined npression and U-U Te orts.
_	34.0		Deposit/Alluvium		- - - - - -	11 -	22			qp= LL=	1 tsf 40, PI=21
35-	861.3 - -			ossible Boulders, brown to dark um dense to dense. (Glacial	17. Y.1.	25	12			See	0=5% Grain Size umulation Curve.
-	- - 40.0	0 0 0	Outwash)			18*	- 14 -			*For	eign odor in sample.
40 -	_ 40.0 855.3 -	× . · · · × · · · × · · · ×	SANDY LOAM, plastic, with	n Gravel, gray, wet, very stiff.	1	18	12				
 	- 44.0 851.3	× · . × · .	<u> </u>			20 -	13				
45-				ed, with Gravel, with possible ring, medium dense. (Glacial	17	16	14				
-	-		Outwash)		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	12 -	12				



UNIQUE NUMBER



tate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring I	Vo.		Ground Elevation 895.3 (Surveyed)
I	Depth	юy			nc	SPT N ₆₀	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	CI	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	-				1111111 X	24 - - -	13			Se	00=2% e Grain Size cumulation Curve.
55 -	-				1	- 22 -	17				
60 -	- - -		SAND, fine to coarse grained, Boulders, brown, waterbearing, Outwash) (continued) SAND, fine to coarse grained, Outwash)	ed, with Gravel, with possible ring, medium dense. (Glacial	11/11/11/11	- - - 15	33				
65 -	- - - -				TTTTTTTT	- - 100*/1" - -	- 32			*Sa	ample from cuttings.
70 -	69.0 826.3			ed, brown, moist, dense. (Glacial		- - 28 -	17			Se	00=3% e Grain Size cumulation Curve.
1	-				1	-	_			Au	ger refusal at 75 feet,



UNIQUE NUMBER

DEPARTAL DE TRANS

U.S. Customary Units

Mn	DOT	GEOTECHNICAL SECTI	ON - LOG & TEST RES	SULTS						SHEET 4 of 4
State Project		Bridge No. or Job Desc.	Trunk Highway/Location				Boring I	Vo.		Ground Elevation
			TH 7 & Louisiana	Ave De	sign		R-4			895.3 (Surveyed)
_I Dept	gy			u	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEP 1	itholc	Clas	ssification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
820.3 - - - - - - - - - - - - - - - - - - -		With Shale seam at 77 1/2 fe	red, hard, crinkly bedded,		100	91	1.52	3 2 3 1 1 0 1 1 1	PL	pparent Top of Bedrock ATTEVILLE DRMATION

Water observed at 7 1/2 while drilling.

Boring immediately backfilled with bentonite grout.

Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11
N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



iale r	Project		Bridge No. or Job Desc.	Trunk Highway/Loca TH 7 & Louis		De	sign		Boring I	VO.		Ground Elev 897.0 (S	
ocatio	on Co.	Coo	rdinate: X=503613	Y=153443	(ft.)	Drill	Machine	7514					Γ 1 of 4
	Latit	ude (North)=	Longitude (West)=		Han	nmer CN	/IE Autor	natic Ca	librated		Drilling Completed	5/12/ ⁻
	No Si	tation-	Offset Information Availab	ole			SPT	МС	сон	γ	lj.	Other 7	ests
Ŧ	Depth	ogy				00	N 60	(%)	(psf)	(pcf)	Soil	Or Rem	arks
DEPTH		Lithology		Classification		Drilling Operation	REC	1	ACL	Core Breaks	ck	Forma	
	Elev.	7		Ciassification		100 120	(%)	(%)	(ft)	Breaks	Ř	or Men	nber
	0.9		10 1/2 inches Bitumino			1							
	896.1 2.0	\bowtie	LOAMY SAND, fine to i moist. (Fill)	medium grained, with Grave	el, brown,	1							
1	895.0					13		Ť					
1	-	\bowtie				X	48	- 5					
+	-					[]		+					
5-	_	\bowtie				1	-	_					
		\bowtie				X	27	4					
		\bowtie	LOAMY SAND fine to	coarse grained, trace Grave	el to with	1							
†	-	\bowtie	Gravel, brown with dark			<u></u>		†					
t	-	\bowtie				X	24	- 5					
+	-	\bowtie				1		+					
10-	_	\bowtie				<u>}</u>	_	_					
		\bowtie				X	6	9					
Ī	12.0	\bowtie				3		Ī					
t	885.0					}}		†					
.	-	\bowtie				X	6	17					
+	-	\bowtie				3		<u> </u>					
15-	_	\bowtie				<u>}</u>	_	_					
		\bowtie				X	7	14				200=3% ee Grain Size	
Ī	-	\bowtie	SAND, fine to coarse g	rained, trace Gravel to with	Gravel,	3	•	Ī				cumulation C	curve.
†	-	\bigotimes		feet, brown, moist to water		<u>}</u>		†					
+	-	\bowtie	· ···/			\times	7*	12				witched to mi lling from 17	
+	-	\bowtie				3		-			fee		
20 -	_	X				<u></u>	_	_					
-		\bowtie				\times	8	14					
1		\bowtie				3		Ť					
-	22.0 875.0					1	-	†					
+	-	\bowtie	SAND, fine to coarse or	rained, with Gravel and pos	sible	\times	20	20					
-	-		Boulders, brown, water			<u>日</u>		1					
25		\bowtie				<u>}</u>		L	l		<u> </u>		



UNIQUE NUMBER



tate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	Vo.		Ground Elevation 397.0 (Surveyed)
ŗ	Depth	убс			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cla	essification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
30-			SAND, fine to coarse graine Boulders, brown, waterbeari	d, with Gravel and possible ng. (Fill) <i>(continued)</i>	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	25* - - 28 -	- 15			*No	sample recovery.
-	32.0 865.0				X -{{	27	20				
-	34.0		LOAMY SAND, fine to coars with Gravel, brown with gray	ee grained, with Clay seams, , waterbearing. (Fill)		26 -	10				
35-	863.0 - - 37.0		SANDY LOAM, non plastic, black, wet. (Fill)	trace Gravel, brown, gray and	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	30	15				
-	860.0	0 0 0 0	GRAVEL, brown, waterbeari	ng. (Possible Fill)		35 -	17				
40	- - _ 42.0	0 0				27* -	21			See Accu	0=3% Grain Size umulation Curve.
-	855.0 - - 45.0		SAND, fine to coarse graine waterbearing. (Possible Fill)		1	23 - -	14			hollo	tched to standard ow-stem auger drillir sample.
45 -	852.0		With lenses of Peat at 45 fe		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	21	57				
+++++++++++++++++++++++++++++++++++++++	-		SAND, fine to coarse graine waterbearing, medium dense	d, with Gravel, brown, e. (Glacial Outwash)	1	19 -	- 15				



UNIQUE NUMBER



tate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring I	Vo.		Ground Elevation 897.0 (Surveyed)
T	Depth	gy			<i>u</i>	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cla	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	-		SAND, fine to coarse graine waterbearing, medium dens	ed, with Gravel, brown, se. (Glacial Outwash) <i>(continued)</i>	XXXXXX	20	21				
55-			GRAVEL, brown, waterbear Outwash)	ring, medium dense. (Glacial	111 X 111	- 13 -	19			Se	200=3% ee Grain Size ccumulation Curve.
60-	- 59.0 838.0 -				1717171X	- - 11	13				
65 -	-		SAND, fine to coarse grains	od with Gravel brown	11111111	- - 25	- - - 19				
70-	-		SAND, fine to coarse graine waterbearing, medium dens	ee to dense. (Glacial Outwash)	11111111111111111111111111111111111111	-	- 17				
-	- - - 74.0 823.0		LOAMY SAND, fine to coan	se grained with Gravel and	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	28 - - -	17			*0	switched to rock coring



UNIQUE NUMBER

DEPARTMENT OF TRANS

U.S. Customary Units

	Mn/D	от с	GEOTECHNICAL SECTION	ON - LOG & TEST RESU	LTS						SHEET 4 of 4
State I	Project		Bridge No. or Job Desc.	Trunk Highway/Location				Boring I	Vo.		Ground Elevation
				TH 7 & Louisiana Av	e De	sign		R-5			897.0 (Surveyed)
7	Depth	gy			u	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTI	Depth Sologoutin		ssification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member	
	822.0	\pm	\waterbearing. (Glacial Till)						3	· · ·	pparent Top of Bedrock
-	-				Ш	•			1	- 1	, p. a
-	-	井			Ш	100	84	0.70	4		
-	-	긐			Ш				1		
-	-	\equiv	LIMESTONE, slightly weather	red hard with Shale	Ш	-			0	PI	.ATTEVILLE
80-	_	井	inclusions at 80 to 81 feet, cri						6	4	DRMATION
-	-	\pm			Ш				0		
-	-				Ш	100	82	1.02	1		
-	+	苗							3		
-	85.0					-			0		
85-	812.0		END OF BORING.			<u> </u>	<u> </u>	1	1		

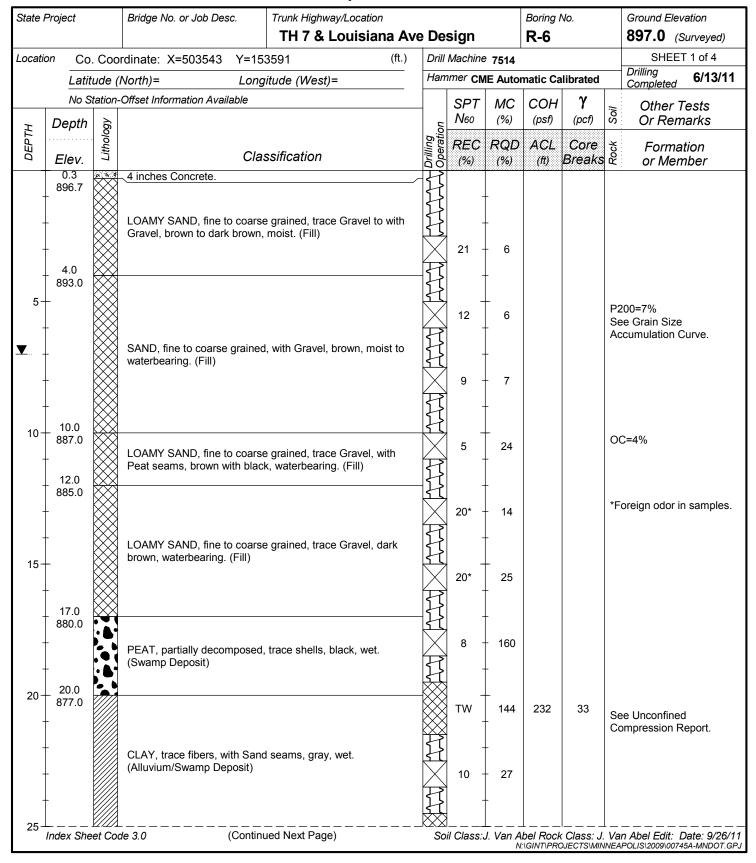
Water observed at 13 feet with 19 1/2 feet of hollow-stem auger in the ground.

Boring immediately backfilled with bentonite grout.



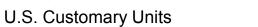
UNIQUE NUMBER



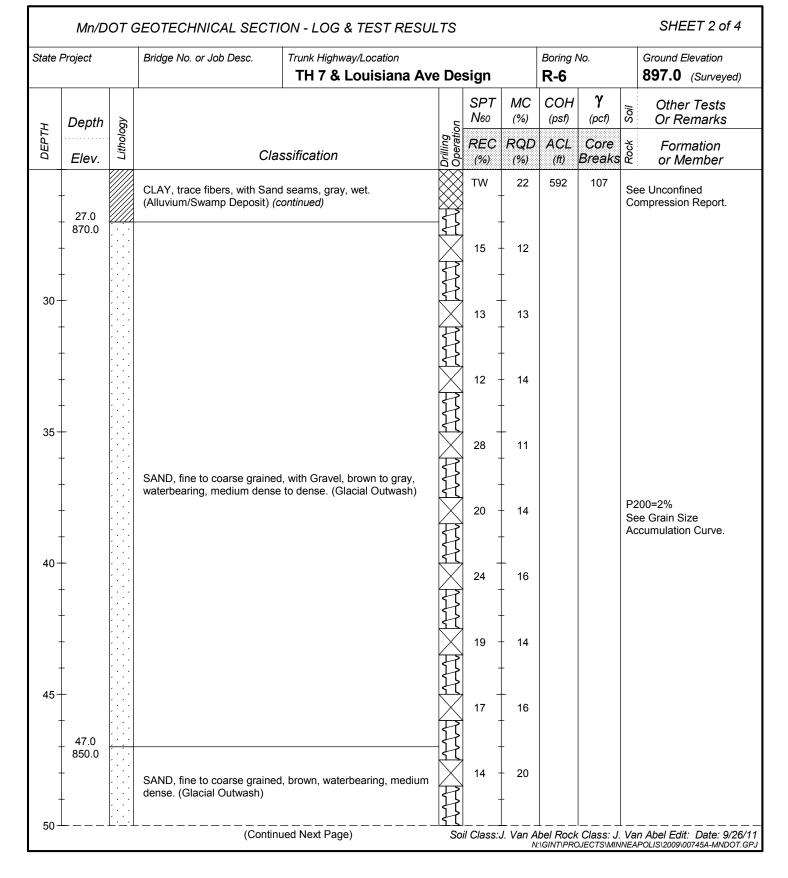




UNIQUE NUMBER









UNIQUE NUMBER



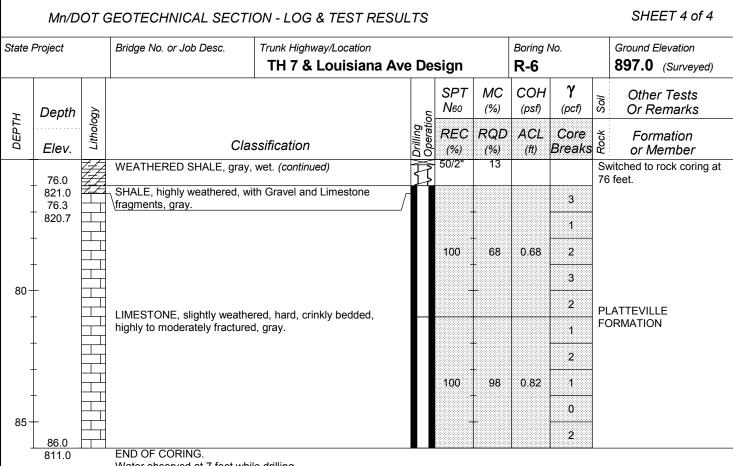
tate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana	Ave De	sign		Boring N	Vo.		Ground Elevation 897.0 (Surveyed)
ı	Depth	gy			u	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	CI	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	-					19 - - -	24				
55 - -	-					24 - -	23				
- - - -	69.0		SAND, fine to coarse graine dense. (Glacial Outwash) (ed, brown, waterbearing, medicontinued)		- 17 -	20			Se	200=3% ee Grain Size ccumulation Curve.
- 35 - -					- 21 -	26					
70 -		`' × 'x ' 'x ' 'x ' 'x ' 'x '	SANDY LOAM, plastic, with reddish brown, wet, very sti	n Gravel, with Sand seams, iff. (Glacial Till)		23	12			Se	200=32% se Grain Size scumulation Curve.
-	_ 74.0 823.0	×	WEATHERED SHALE, gra		_	-				V/	



UNIQUE NUMBER



U.S. Customary Units



Water observed at 7 feet while drilling.
Boring immediately backfilled with bentonite grout.

Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



State F	Project		Bridge No. or Job Desc.	Trunk Highway/Loca		e De	sign		Boring I	Vo.		Ground Elevation 896.6 (Surveyed)
Locatio	on Co.	. Coo	rdinate: X=503722 Y=1	 153613	(ft.)		Machine	 ₹ 7514				SHEET 1 of 4
	Latit	ude (North)= Lo	ngitude (West)=		Han	nmer CN	/IE Autor	natic Ca	librated		Drilling 5/10/1
			Offset Information Available	. ,			SPT	МС	сон	γ		Other Tests
_	Depth	gy				ءِ	Maa	(%)	(psf)	(pcf)	Soil	Or Remarks
DEPTH	Elev.	Lithology	C	lassification		Drilling Operation	REC	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
5-	-		SANDY LOAM, non to sligi wood, dark brown, moist. (ntly plastic, trace Grave Fill)	I and	THIN XHILL	5 -	- 41 - 12				
10-	7.0 889.6		SAND, fine to coarse grain (Fill)	ed, brown, moist to wat	erbearing.	11 X 11	10	6			Se	200=8% ee Grain Size ccumulation Curve.
15-	- 14.0 882.6 -		LOAMY SAND, fine to med waterbearing. (Fill)	dium grained, brown,		1	6 -	16				
+	17.0 879.6 19.0		PEAT, dark brown, wet. (S	wamp Deposit)		1111 X	8 -	106				
20-	877.6		SILTY CLAY LOAM, slight		ace fibers,	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	TW	25	625	100	Co	ee Unconfined ompression and U-U Te eports.
	-		gray, wet. (Swamp Deposit)		1 X X X X X X X X X X X X X X X X X X X	7	- 33			LL	=38, PI=10
25	 Index She	∐∐∐ et Cod	de 3.0 (Cont	inued Next Page)		KXX S∩	l il Class:	⊥ J. Van A	⊥ bel Rock	 : Class: .I	⊥ _ . Va	 In Abel Edit: Date: 9/26



UNIQUE NUMBER



tate Pr	roject		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	Vo.		Ground Elevation 896.6 (Surveyed)
I I	Depth	λbα			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	CI	assification	Drilling Operation	REC	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
	26.0 870.6		SILTY CLAY LOAM, slightly gray, wet. (Swamp Deposit	y organic to organic, trace fibers (continued)		TW	36	195	83	Se	e Unconfined mpression and U-U Te
-	070.0	0 0			H					Re	ports.
Ţ		0 0			1	36 -	9				
30+		odense. (Glacial Outwash)			\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	25 -	10			Se	00=3% e Grain Size cumulation Curve.
+	0	0	GRAVEL, with Sand, gray, dense. (Glacial Outwash)	waterbearing, medium dense to	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	25	- 14				
35+		0			\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	20	8				
+	39.0 857.6	0 0 0			<u> </u>	18 -	9			Se	00=0.5% e Grain Size cumulation Curve.
40+	307.3				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	26	14				
+			SAND, fine to coarse grains	ed, trace Gravel to with Gravel, ım dense to dense. (Glacial	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	18 -	14				
45			Outwash)	Schoo to derise. (Clauai	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	18	18				
T +					<u> </u>	21	- 15				



UNIQUE NUMBER



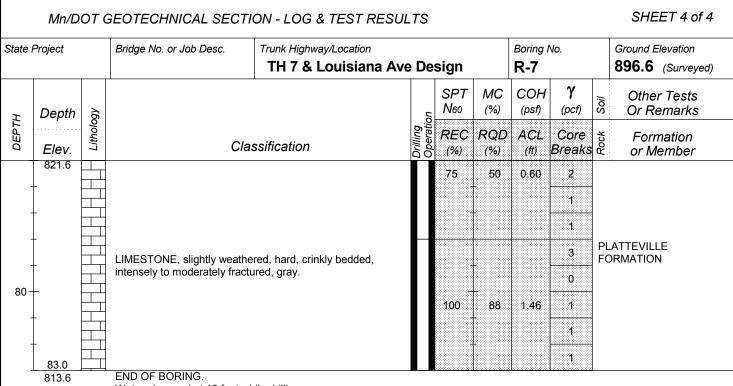
tate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	Vo.		Ground Elevation 896.6 (Surveyed)
Į	Depth	ygv.			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	CI	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	- - -				XXXXXXX	26 - -	14			Se	00=3% e Grain Size cumulation Curve.
55-			brown, waterbearing, mediu Outwash) (continued)	ed, trace Gravel to with Gravel, ım dense to dense. (Glacial	11	28	18				
60-	- 59.0 837.6 -	× · · · × · · · × · · · · × · · · · × · · · · · ×				36	20				00=49% e Grain Size
-	- - _ 64.0 _ 832.6	· · · · × · · · · · · · · · · · · · · ·	SANDY LOAM, reddish bro	wn, wet, very stiff. (Glacial Till)	777777	-	_			Ac	cumulation Curve.
65 -	- - -		SAND, fine to coarse grains waterbearing, medium dens			19 - -	17				
70 -	69.0 827.6		LOAMY SAND, fine grained dense. (Glacial Outwash)	d, brown, waterbearing, medium	1777	- 26	- - 14				witched to rock coring
	72.0 824.6 73.0		LIMESTONE, highly weather	ered, gray, waterbearing.		100*/3"	-			X/,	er sample. parent Top of Bedroc
-	75.0 823.6 - 75.0		LIMESTONE, highly weather gray, with Shale inclusion a	ered, hard, intensely fractured, t 75 feet.		75 -	50	0.60	NA NA	PL	ATTEVILLE PRMATION



UNIQUE NUMBER



U.S. Customary Units



Water observed at 12 feet while drilling.
Boring immediately backfilled with bentonite grout.

Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



State F	Project		Bridge I	No. or Job Des	SC.	Trunk Highway/Location TH 7 & Louisiana A	Ave	De	sign		Boring I	No.		Ground Eleva	
ocatio	on Co.	. Coc	rdinate:	X=503778	Y=15	3425 (ft.	.) [Drill	Machine	7503				SHEET	
	Latit	ude (North)=		Long	itude (West)=	- 7	Ham	mer CN	IE Autor	natic Ca	librated		Drilling Completed	6/9/1
	No S	tation	-Offset Inf	ormation Avail	lable				SPT	МС	сон	γ	11	Other T	ests
Į	Depth	уgс						on	N 60	(%)	(psf)	(pcf)	Soil	Or Rema	
DEPTH	Elev.	Lithology			Clas	ssification	Drilling	Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Format or Mem	
-	- _ 2.0	1/ 1/1/		SAND, fine to ark brown, mo		e grained, trace Gravel and osoil Fill)	•		-	_					
-	886.0		SAND, moist. (grained	, brown with dark brown,			5 -	- 11					
5-	884.0 -							<u> </u>	3	295					
+	-		PEAT, f	fibrous, dark b	orown, w	et. (Swamp Deposit)	\/ • •		-	_					
	- _ 9.0							\ !?	1 -	403					
10-	879.0 - -								2	159					
-	-			semi fibrous, t o Deposit)	race sh	ells, dark brown and black, we	et.		TW -	- 129		35	Se	c=1.33, Cr=0.2 ee Consolidatio eport.	9 on Test
15	-						\ \ \ \		5	110					
+	- _ 19.0 869.0							\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	TW* -	-				No thinwall sam covery.	nple
20	- - -		SILTY (organic,	gray and black, wet. (Swamp			5	71					
<u>-</u>	- _ 24.0 864.0		I OAM	SAND fine to	n coare	grained, with Gravel, gray,			TW -	- 27	688	98	_	ee Unconfined ompression Re	eport.
25				earing, loose.	(<u>Alluviu</u> r		[}		L	l		l_		



UNIQUE NUMBER



State F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring N	Vo.		Ground Elevation 888.0 (Surveyed)		
I	Depth	λbα			uc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks		
DEPTH	Elev.	Lithology	CI	lassification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member		
			LOAMY SAND, fine to coar waterbearing, loose. (Alluvi	rse grained, with Gravel, gray, um) <i>(continued)</i>	XXXXXX	6*	13 - - - 12			*L	ittle sample recovery.		
30	29.0 859.0				11	5	16						
+			SAND, fine to coarse grains waterbearing, loose to med	ed, with Gravel, gray,	17 17	7 -	- 18			Se	P200=3% See Grain Size Accumulation Curve.		
35-	waterbearing		waterbearing, loose to med	ig, 19000 to modulin conoc. (villaviani)		12	16						
+	39.0 849.0	· · · · · · · · · · · · · · · · · · ·			17	23	- 20						
40	42.0	× × × × × × × × × × × × × × × × × × ×	SANDY LOAM, plastic, trac Till)	ce Gravel, gray, wet, stiff. (Glacial	11	11	10						
+	846.0		SANDY CLAY LOAM, trace	e Gravel, gray, wet, stiff. (Glacial	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	15	11			LL	=22, PI=13		
45	45.0 843.0	.00			\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	19 -	10						
+	SAND, fine to coarse grained, with Gravel, with occasion Loamy Sand layers, brown, waterbearing, medium dens (Glacial Outwash)				11	15 -	- 21						



UNIQUE NUMBER



tate F	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	re De	sign		Boring I	Vo.		Ground Elevation 888.0 (Surveyed)
I	Depth	yb,			nc nc	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cla	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	-				X	15	14			P2	200=2% ee Grain Size ccumulation Curve.
-	SAND, fine to coarse grained, with Gravel, with occasio				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	24 -	16				
55 -			Loamy Sand layers, brown, (Glacial Outwash) (continue	<u></u>	13	10					
	-				1	-					
-	- _ 59.0 _ 829.0	· · · · · · · · · · · · · · · · · · ·			- <u> </u>	15	9				
60	-	`.`.X `x `. ``.X `x `. `x `.	SANDY LOAM, non plastic, moist to waterbearing, dens	trace Gravel, reddish brown, e. (Glacial Till)	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	29	10			S	200=29% ee Grain Size ccumulation Curve.
-	-	: : x · . : : x · .			\$1	29* -				*L	ittle sample recovery.
65 -	_ 64.0 824.0 _				11/1/11	.50*/3" ⁻	<u>-</u>			ΑĮ	pparent Top of Bedrock
-	-		LIMESTONE, highly weather	ered, gray.	777777	-	-				
70-	_ 70.0 818.0 -			nered, hard, crinkly bedded, , with Shale seams at 72-73					NA NA	Aı sv	uger refusal at 70 feet, vitched to rock coring.
-	73.0 815.0		feet, gray. LIMESTONE, slightly weathered, hard, crinkly bedded, highly to moderately fractured, with Shale seam at 75 feet,			70	0	0.00	6		LATTEVILLE ORMATION
75	L		gray. - — — — — — — — — — — — — —						6	_	



UNIQUE NUMBER

U.S. Customary Units

State	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana Av	e De	sign		Boring I	Vo.		Ground Elevation 888.0 (Surveyed)	
.	Depth	gy			u	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks	
DEPTH	 		CI	assification	Drilling Operation	REC	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member	
80-	80.0			nered, hard, crinkly bedded, red, with Shale seam at 75 feet,		100	93	0.78	0 2 2 2 2	1	LATTEVILLE DRMATION	

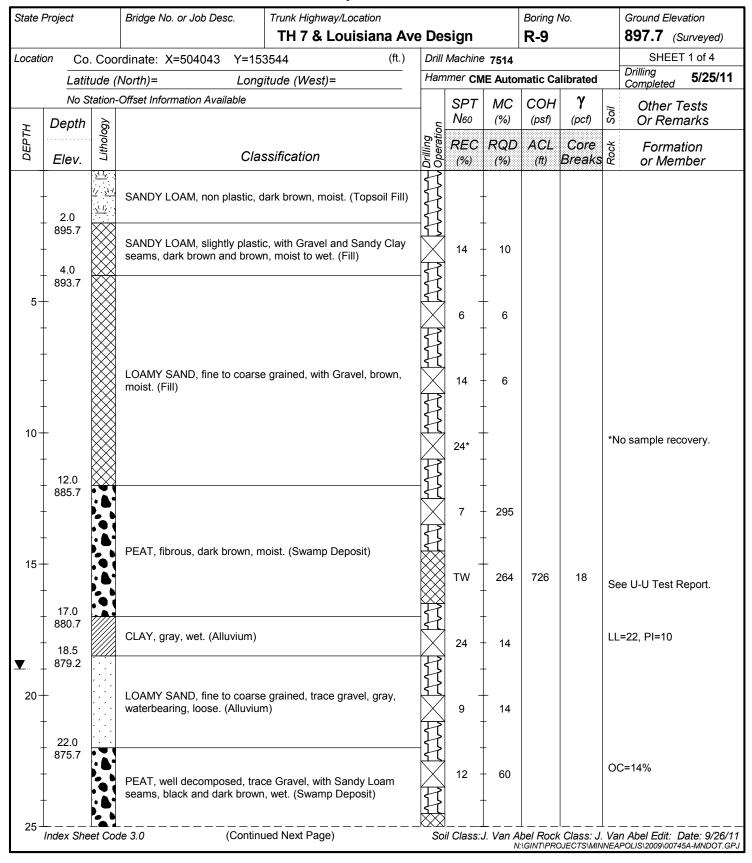
Boring immediately backfilled with bentonite grout.

Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11
N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER

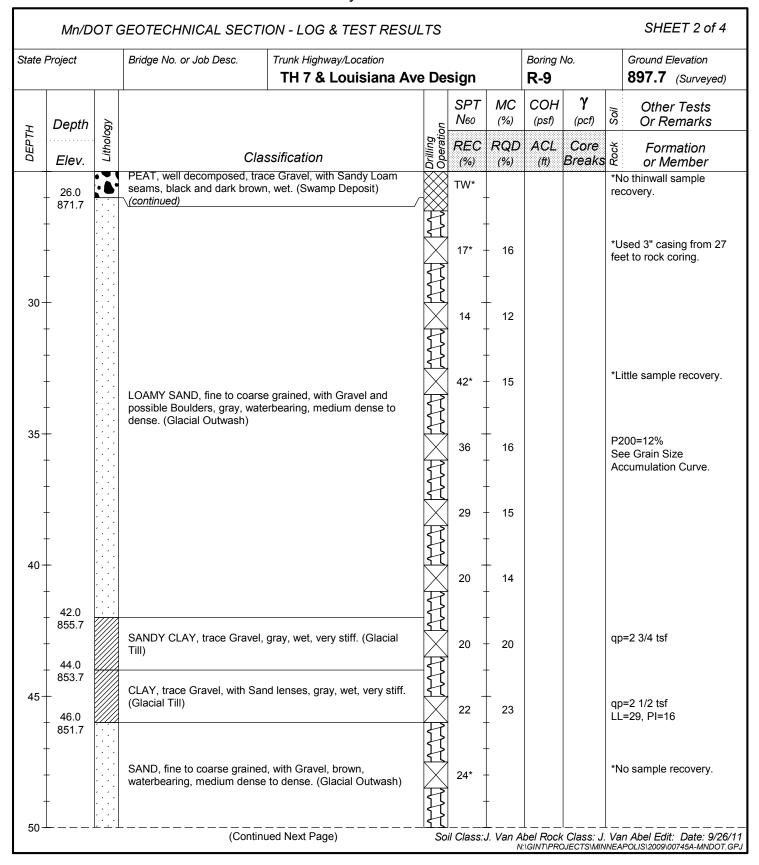






UNIQUE NUMBER







UNIQUE NUMBER



	Mn/D	от	GEOTECHNICAL SECT	ION - LOG & TEST RES	ULTS						SHEET 3 of 4
State I	Project		Bridge No. or Job Desc.	Trunk Highway/Location TH 7 & Louisiana A	ve De	sign		Boring I	No.		Ground Elevation 897.7 (Surveyed)
Н	Depth	gy			no	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks
DEPTH	Elev.	Lithology	Cla	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
-	54.0		SAND, fine to coarse graine waterbearing, medium dens (continued)	d, with Gravel, brown, e to dense. (Glacial Outwash)	XXXXXX	32	24			Se	00=2% e Grain Size cumulation Curve.
55- - -	843.7 - -				\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	, - 19 .	20				
- 60 - -	-		SAND, fine to medium grain medium dense. (Glacial Out	ed, brown, waterbearing, wash)		, - 16 .	23			Se	00=3% e Grain Size cumulation Curve.
- 65 -	64.0 833.7 65.0	0 0	GRAVEL, with Limestone fravery dense. (Weathered Be	agments, brown, waterbearing, drock)		100/7"	12			. _	
- - -	832.7 - - -		Gravel, Cobbles and Limest	one fragments.							ritched to rock coring at feet to advance boring.
70 - - -	- - 72.0 825.7				$\ $	-			5		parent Top of Bedrock
- -	-		LIMESTONE, moderately w intensely fractured, gray, wit			90	26	0.43	2 5	PL	ATTEVILLE PRMATION
75 -		1	(Contir	nued Next Page)	Sc	il Class:					n Abel Edit: Date: 9/26/11 POLIS\2009\00745A-MNDOT.GPJ

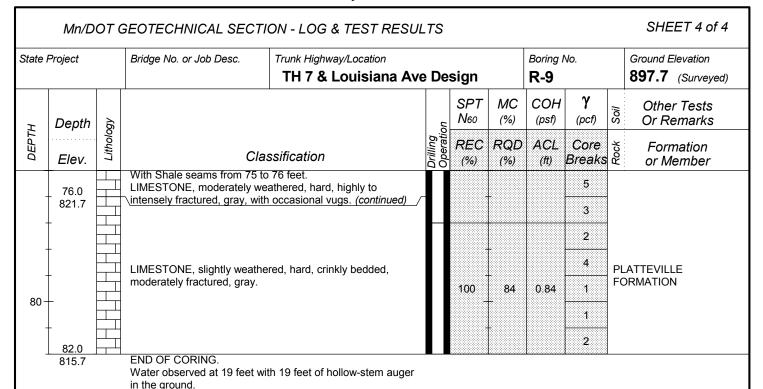


UNIQUE NUMBER



U.S. Customary Units

Boring immediately backfilled with bentonite grout.



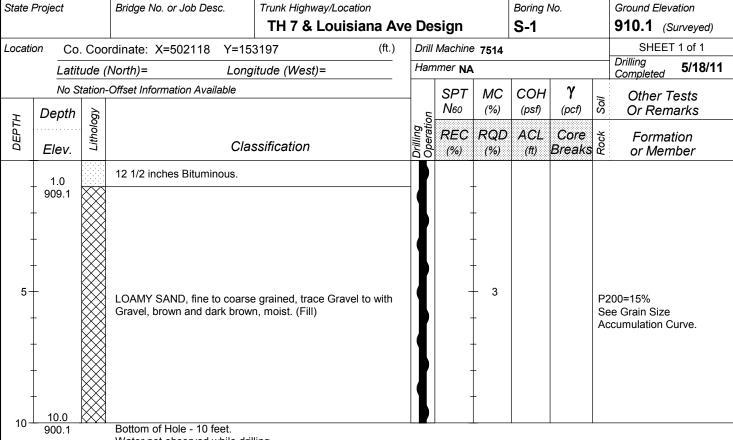
Soil Class: J. Van Abel Rock Class: J. Van Abel Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER

U.S. Customary Units





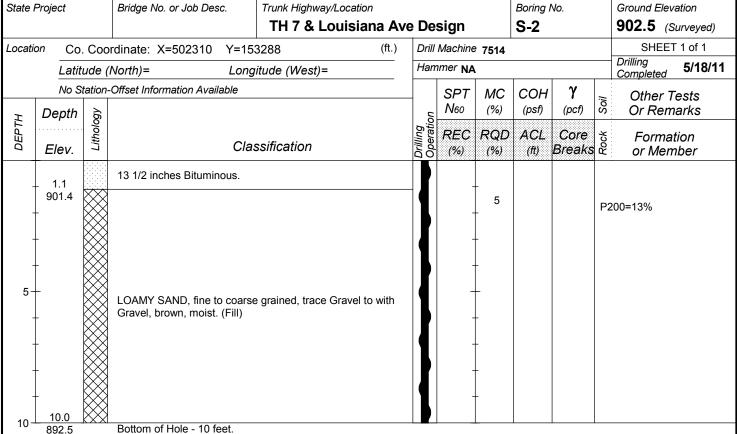
Water not observed while drilling.
Water not observed to cave-in depth of 8 feet immediately after withdrawal of auger.
Boring immediately backfilled.



UNIQUE NUMBER



U.S. Customary Units



Water not observed while drilling.

Water not observed to cave-in depth of 8 feet immediately

after withdrawal of auger.

Boring immediately backfilled.



UNIQUE NUMBER

U.S. Customary Units



State	Project		Bridge No. or Job Desc.	Trunk Highway/Locat	ion				Boring I	No.		Ground Elevation
				TH 7 & Louisi	ana Av	e De	sign		S-3			898.4 (Surveyed)
Locati	on Co.	. Coo	rdinate: X=502509 Y=15	3274	(ft.)	Drill	Machine	7514				SHEET 1 of 1
	Latit	ude (North)= Long	nitude (West)=		Han	nmer NA	1				Drilling 5/18/11
	No S	tation-	Offset Information Available				SPT	МС	сон	γ	ij	Other Tests
I	Depth	gy				2	N 60	(%)	(psf)	(pcf)	Soil	Or Remarks
DEPTH	Elev.	Lithology	Cla	ssification		Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
_	1.1		13 inches Bituminous.				-					
-	897.3		SAND, fine to coarse grained (Fill)	d, with Gravel, brown, ı	noist.		-	- 8			P2	200=9%
5-	895.4		SANDY LOAM, slightly plast moist. (Fill)	c, trace Gravel, dark b	rown,		- - - -	-				
10-	10 10.0		Bottom of Hole - 10 feet. Water not observed while dri Water not observed to cave- after withdrawal of auger		ediately							

after withdrawal of auger. Boring immediately backfilled.

Index Sheet Code 3.0

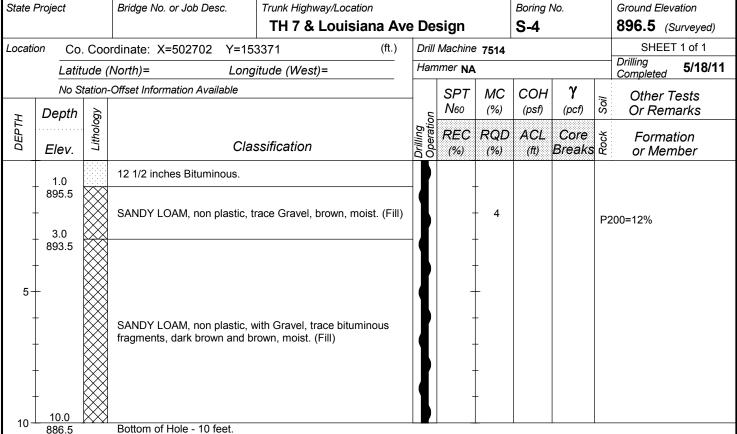
Soil Class: J. Van Abel Rock Class: Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



U.S. Customary Units



Index Sheet Code 3.0

Water not observed while drilling.

Water not observed to cave-in depth of 7 1/2 feet

immediately after withdrawal of auger.

Boring immediately backfilled.



UNIQUE NUMBER





State	Project		Bridge No. or Job Desc.	Trunk Highway/Location					Boring	No.		Ground Elevation
				TH 7 & Louisiana	Ave	De	sign		S-5			896.6 (Surveyed)
Locati	on Co.	. Coo	rdinate: X=502894 Y=15	3412 (ft.)	Drill	Machine	7514				SHEET 1 of 1
	Latit	ude (North)= Long	itude (West)=		Ham	mer NA	.				Drilling 5/17/11
	No S	tation-	Offset Information Available				SPT	МС	сон		Soil	Other Tests
E	Depth	ogy				ion	N 60	(%)	(psf)	(pcf)	Ŋ	Or Remarks
нтаэа	Elev.	Lithology	Cla	ssification		Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
_	1.1		13 1/2 inches Bituminous.				_	_				
-	895.5		SAND, fine to coarse grained (Fill)	I, with Gravel, brown, moist.		1	-	-				
5-	893.6		LOAMY SAND, fine to coarse brown, moist. (Fill)	e grained, with Gravel, dark			- - - -	-				
10-	886.6		Bottom of Hole - 10 feet. Water not observed while dri Water not observed to cave-i		ely					•	•	

Index Sheet Code 3.0

after withdrawal of auger. Boring immediately backfilled.

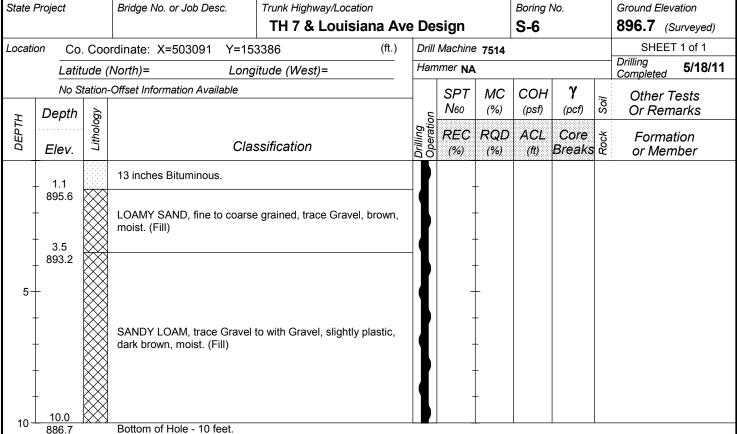
> Soil Class: J. Van Abel Rock Class: Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



U.S. Customary Units



Index Sheet Code 3.0

Water not observed while drilling.

Water not observed to cave-in depth of 5 1/2 feet

immediately after withdrawal of auger.

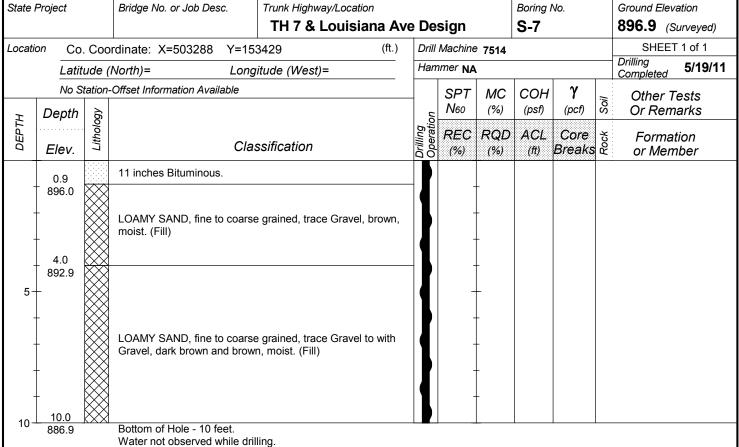
Boring immediately backfilled.



UNIQUE NUMBER

U.S. Customary Units





Water not observed write drilling.

Water not observed to cave-in depth of 7 feet immediately after withdrawal of auger.

Boring immediately backfilled.



UNIQUE NUMBER

U.S. Customary Units



State	tate Project Bridge No. or Job Desc. Trunk Highway/Location TH 7 & Louisiana								Boring	No.		Ground Elevation	
				TH 7 & Louisiana Av	ve D	es	ign		S-8			898.5 (Surveyed))
Locati	on Co	. Coo	rdinate: X=503786 Y=15	3592 (ft.)	Dr	rill N	/lachine	7514				SHEET 1 of 1	
	Latit	ude (i	North)= Long	itude (West)=	Há	amr	ner NA					Drilling 5/17/	11
	No S	tation-	Offset Information Available			- 1	SPT	МС	сон	γ	ji.	Other Tests	
Į	Depth)gy				0	N 60	(%)	(psf)	(pcf)	Soil	Or Remarks	
DEPTH	Elev.	Lithology	Clas	ssification	Drilling	Operati	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member	
	1.0		12 1/2 inches Bituminous.										
-	897.5 2.0		SAND, fine to coarse grained (Fill)	, trace Gravel, brown, moist.	1		-	_					
5- -	7.0		LOAMY SAND, fine to coarse Gravel, dark brown and brow	e grained, trace Gravel to with n, moist. (Fill)			- - - -	-					
	891.5		SANDY LOAM, non plastic, v (Fill)	vith Gravel, dark brown, moist.			-	-					
10-	888.5	<u> </u>	Bottom of Hole - 10 feet. Water not observed while dril Water not observed to cave-i				-				1		

Index Sheet Code 3.0

after withdrawal of auger. Boring immediately backfilled.

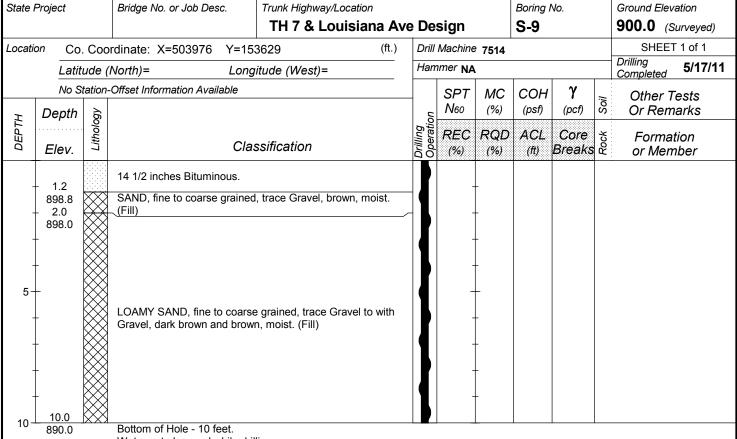
> Soil Class: J. Van Abel Rock Class: Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER



U.S. Customary Units



Water not observed while drilling.

Water not observed to cave-in depth of 8 feet immediately

after withdrawal of auger.

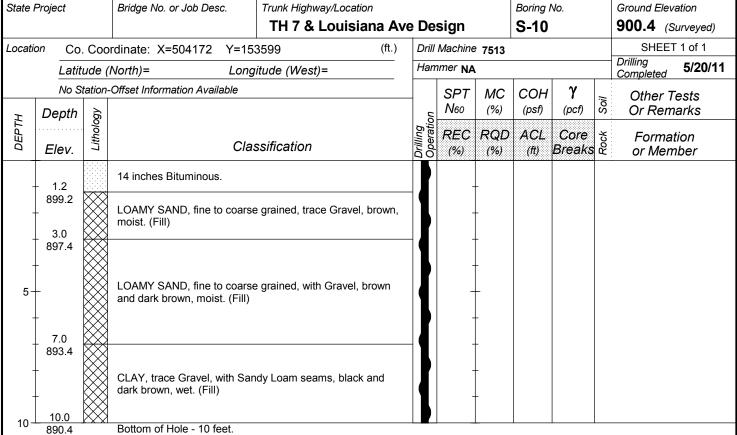
Boring immediately backfilled.



UNIQUE NUMBER



U.S. Customary Units



Water not observed while drilling.

Water not observed immediately after withdrawal of auger.

Boring immediately backfilled.



UNIQUE NUMBER

U.S. Customary Units



State	Project		Bridge No. or Job Desc.						Boring I	No.		Ground Elevation
				TH 7 & Louisiana Av	e De	sigr	1		S-11			904.3 (Surveyed)
Locati	on Co.	Coo	rdinate: X=504375 Y=15	3704 (ft.)	Drill	Mach	nine	7514				SHEET 1 of 1
	Latit	ude (i	North)= Long	itude (West)=	Har	nmer	NA					Drilling 5/17/11
	No Station-Offset Information Available Depth						T	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests
DEРТН	Elev.	Lithology	Clas	ssification	Drilling Operation	RE (%		RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member
5-	1.1 903.2 2.0 902.3		Aggregate Base), brown, moi	e grained, trace Gravel to with			+					
10-	894.3		Bottom of Hole - 10 feet.			•				•		

Water not observed while drilling.
Water not observed to cave-in depth of 7 1/2 feet immediately after withdrawal of auger.
Boring immediately backfilled.



UNIQUE NUMBER



U.S. Customary Units

State Project			Bridge No. or Job Desc. Trunk Highway/Location TH 7 & Louisiana Ave			n Dosian			Boring No. S-12			Ground Elevation 903.4 (Surveyed)	
Location Co. Coordinate: X=504567 Y=153642 (ft.) Latitude (North)= Longitude (West)=						Drill Machine 7513 Hammer NA						SHEET 1 of 1 Drilling Completed 5/20/1	
<i>+</i>	No Si		n-Offset Information Available			u	SPT N60	MC (%)	COH (psf)	γ (pcf)	Soil	Other Tests Or Remarks	
DEРТН	Elev.	Lithology	Clas	ssification	Drilling	Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member	
5-	3.0 902.2 3.0 900.4 4.0 899.4 6.0 897.4		moist. (Fill) CLAY, trace Gravel, slightly of (Fill) LOAMY SAND, fine to coarse moist. (Fill)	e grained, trace Gravel, brown organic, black and brown, wet. e grained, with Gravel, brown, non plastic, dark brown, moist	,		-	3 17			Se	200=13% se Grain Size scumulation Curve.	

Water not observed while drilling.

Water not observed to cave-in depth of 7 feet immediately

after withdrawal of auger.

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UNIQUE NUMBER



U.S. Customary Units

State Project			Bridge No. or Job Desc.	Trunk Highway/Location			Boring No.			Ground Elevation			
			TH 7 & Louisiana Ave Design				S-13			906.6 (Surveyed)			
Locati	on Co.	Coo	rdinate: X=504761 Y=15	3703 (ft.)	Dril	l Machine	7514				SHEET 1 of 1		
	Latitude (North)= Longitude (West)=						\				Drilling 5/16/11		
	No Station-Offset Information Available						МС	сон	γ		Other Teets		
7	Depth	gy			2	SPT N60	(%)	(psf)	(pcf)	Soil	Or Remarks		
рертн	Elev.	Lithology	Clas	ssification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member		
	1.1		13 inches Bituminous.		▋								
	905.5 2.0		LOAMY SAND, fine to coarse (Fill/Possible Aggregate Base										
5- -	904.6		SANDY LOAM, non plastic, trace Gravel to with Gravel, dark brown, moist. (Fill)			-	7			Se	P200=21% See Grain Size Accumulation Curve.		
- - 10-	899.6 10.0 896.6		SAND, fine to coarse grained (Possible Fill) Bottom of Hole - 10 feet.	l, with Gravel, brown, moist.									

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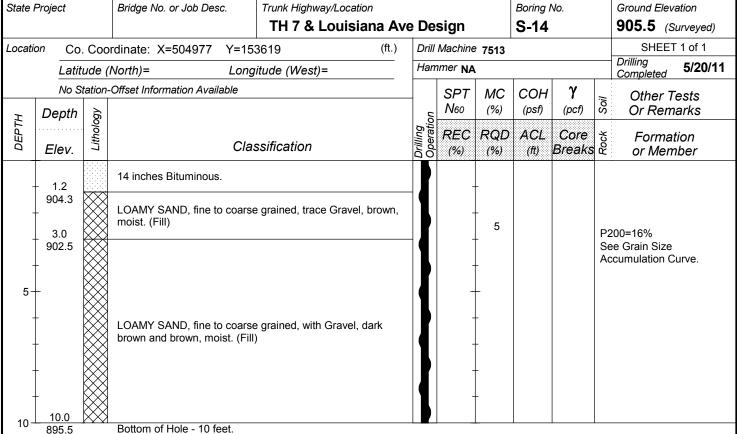
Water not observed while drilling.
Water not observed to cave-in depth of 7 1/2 feet

immediately after withdrawal of auger.



UNIQUE NUMBER

U.S. Customary Units



Water not observed while drilling.

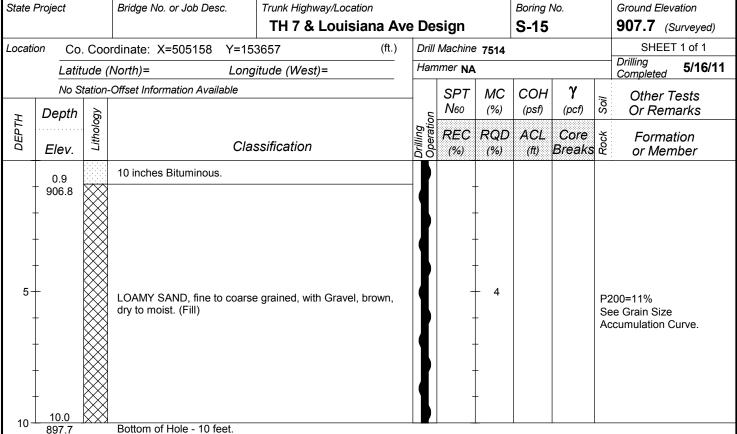
Water not observed immediately after withdrawal of auger.



UNIQUE NUMBER



U.S. Customary Units



Water not observed while drilling.

Water not observed to cave-in depth of 7 1/2 feet

immediately after withdrawal of auger.

Boring immediately backfilled.

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UNIQUE NUMBER



U.S. Customary Units

State Project			Bridge No. or Job Desc.	Trunk Highway/Location			Boring No.			Ground Elevation		
			TH 7 & Louisiana Ave De			Design					893.8 (Surveyed)	
Locatio	n Co	. Coo	rdinate: X=503485 Y=15	linate: X=503485 Y=153942 (ft.)		Drill Machine 7514					SHEET 1 of 1	
	Latitude (North)= Longitude (West)=						Hammer NA				Drilling 5/13/11	
		Station-Offset Information Available				SPT N60	MC	СОН	γ	Soil	Other Tests	
Ŧ	Depth	logy			ion	1400	(%)	(psf)	(pcf)	S	Or Remarks	
DEPTH	Elev.	/ Kbolo third Class		ssification	Drilling Operation	REC (%)	RQD (%)		Core Breaks		Formation or Member	
-	1.4		17 inches Bituminous.		ŀ							
+	892.4 3.0		LOAMY SAND, fine to coars moist. (Fill)	e grained, with Gravel, brown,	 }		_					
5-	890.8		SAND, fine to coarse grained brown, dry to moist. (Fill)	d, trace Gravel to with Gravel,		2				Se	200=4% se Grain Size scumulation Curve.	
	887.8	. A XI	Bottom of Hole - 6 feet. Water not observed while dri	lling	1		L		1			

Water not observed while drilling. Water not observed to cave-in depth of 5 feet immediately

after withdrawal of auger.



UNIQUE NUMBER



U.S. Customary Units

State Project			Bridge No. or Job Desc.	Trunk Highway/Location			Boring No.			Ground Elevation	
			TH 7 & Louisiana Ave			e Design					896.2 (Surveyed)
Locati	on Co.	Coo	rdinate: X=503533 Y=15	53656 (ft.)	Dril	Drill Machine 7514					SHEET 1 of 1
	Latit	Latitude (North)= Longitude (West)=				nmer NA	4				Drilling 5/13/11
	No S	tation-	tion-Offset Information Available			SPT	МС	сон	γ		Other Tests
7	Depth	gy			2	N 60	(%)	(psf)	(pcf)	Soil	Or Remarks
DEPTH	Elev.	Lithology	Cla	essification	Drilling Operation	REC	RQD (%)	ACL (ft)	Core Breaks		Formation or Member
	1.0		12 inches Bituminous.								
- - - 5-	895.2		SAND, fine to coarse graine (Fill)	d, with Gravel, brown, moist.		-	5			Se	200=8% ee Grain Size ecumulation Curve.
-	890.2		Bottom of Hole - 6 feet.	III a a		•	-	•			
			Water not observed while dr	IIIIna.							

Water not observed while drilling.
Water not observed to cave-in depth of 5 feet immediately

after withdrawal of auger. Boring immediately backfilled.



UNIQUE NUMBER



U.S. Customary Units

State Project			Bridge No. or Job Desc.	Trunk Highway/Location			Boring No.			Ground Elevation		
			TH 7 & Louisiana Ave			e Design					894.6 (Surveyed)	
Locati	on Co.	. Coo	rdinate: X=503587 Y=1	53376 (ft.)	Dril	Drill Machine 7514					SHEET 1 of 1	
	Latit	Latitude (North)= Longitude (West)=				nmer NA	4				Drilling 6/10/11	
	No S	tation-	ation-Offset Information Available			SPT	МС	сон	γ		Other Tests	
1	Depth	gy			2	N 60	(%)	(psf)	(pcf)	Soil	Or Remarks	
DEPTH	Elev.	Lithology	Cla	assification	Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks		Formation or Member	
	1.0		12 inches Bituminous.									
- - - 5-	893.6		SAND, fine to coarse graine brown, moist. (Fill)	d, trace Gravel to with Gravel,		-	4			Se	P200=8% See Grain Size Accumulation Curve.	
-	888.6	Bottom of Hole - 6 feet.				•	-	•				
			Water not observed while dr	IIIING.								

Water not observed while drilling.
Water not observed to cave-in depth of 5 feet immediately

after withdrawal of auger.

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UNIQUE NUMBER





State Project			Bridge No. or Job Desc.	Trunk Highway/Location			Boring No.			Ground Elevation		
				TH 7 & Louisiana A	TH 7 & Louisiana Ave Design						891.4 (Surveyed)	
Locati	on Co.	Coo	rdinate: X=503714 Y=15	3118 (ft.)	18 (ft.) Drill Machine 7514						SHEET 1 of 1	
	Latitu	ıde (ı	North)= Long	itude (West)=	Hai	nmer NA	4				Drilling 5/13/11	
	No Station-Offset Information Available					SPT	MC	СОН	γ	Soil	Other Tests	
E	Depth	/go/			į	N 60	(%)	(psf)	(pcf)	Ň	Or Remarks	
DEPTH	Elev.	Lithology	Classification		<i>Drilling</i> Operation	Operat (%)	RQD (%)		Core Breaks		Formation or Member	
	0.7		8 1/2 inches Bituminous.									
- - - 5-	6.0		SAND, fine to coarse grained moist. (Fill)	l, with Gravel, brown, dry to		-	3			Se	P200=8% See Grain Size Accumulation Curve.	
-	885.4		Bottom of Hole - 6 feet. Water not observed while dril Water not observed to cave-in after withdrawal of auger.	n depth of 5 feet immediately								

Index Sheet Code 3.0

Boring immediately backfilled.

Soil Class: J. Van Abel Rock Class: Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ



UNIQUE NUMBER

U.S. Customary Units

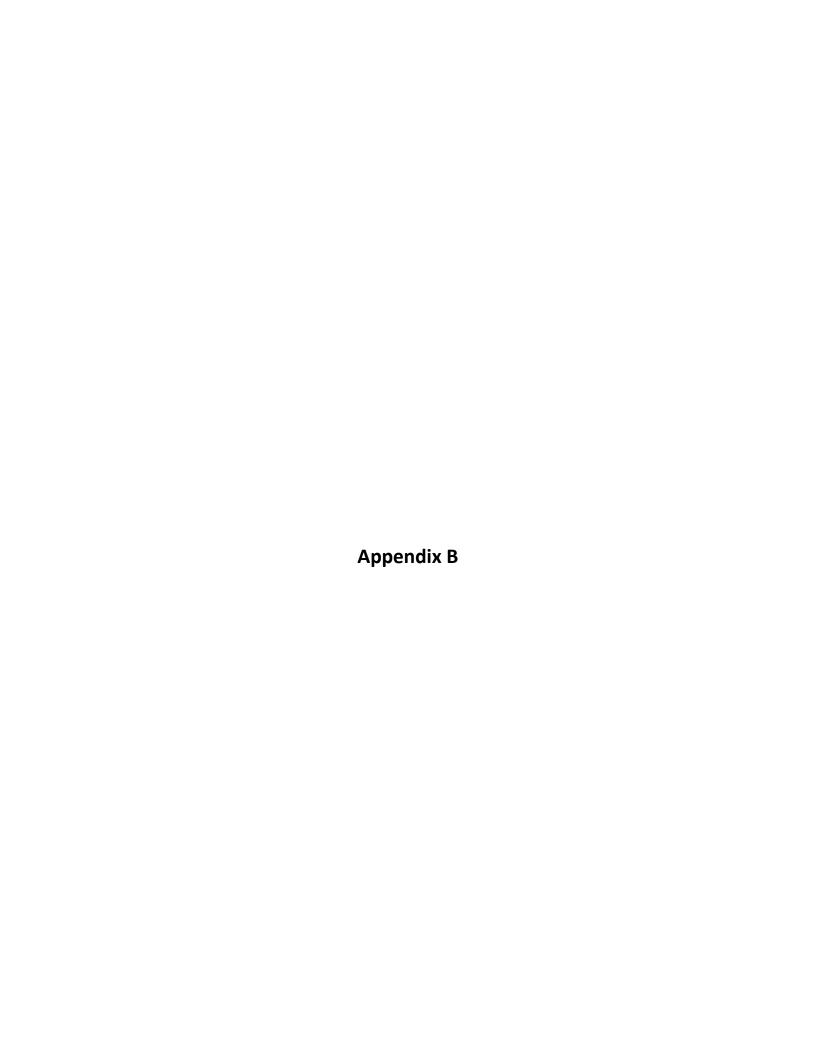


State Project			Bridge No. or Job Desc. Trunk Highway/Location TH 7 & Louisiana Ave		e De	e Design		Boring No. S-21			Ground Elevation 892.2 (Surveyed)		
Locatio			ordinate: X=503863 Y=152704 (ft.) (North)= Longitude (West)= n-Offset Information Available			Drill Machine 7514 Hammer NA					SHEET 1 of 1 Drilling 5/13/11		
						SPT	МС	сон	γ		Other Tests		
	Depth	оду			o	Neo	(%)	(psf)	(pcf)	Soil	Or Remarks		
DEРТН	Elev.	Lithology	Classification		Drilling Operation	REC (%)	RQD (%)	ACL (ft)	Core Breaks	Rock	Formation or Member		
-	- 1.8	1.8	22 inches Bituminous.										
5-	LOAMY SAND, fine moist. (Fill)			e grained, with Gravel, brown,			4			Se	200=16% ee Grain Size ccumulation Curve.		
	6.0 886.2	ΚΧΧΙ	Bottom of Hole - 6 feet. Water not observed while dri Water not observed to cave-i after withdrawal of auger.	lling. in depth of 5 feet immediately		<u> </u>	L						

Index Sheet Code 3.0

Boring immediately backfilled.

Soil Class: J. Van Abel Rock Class: Edit: Date: 9/26/11 N:\GINT\PROJECTS\MINNEAPOLIS\2009\00745A-MNDOT.GPJ

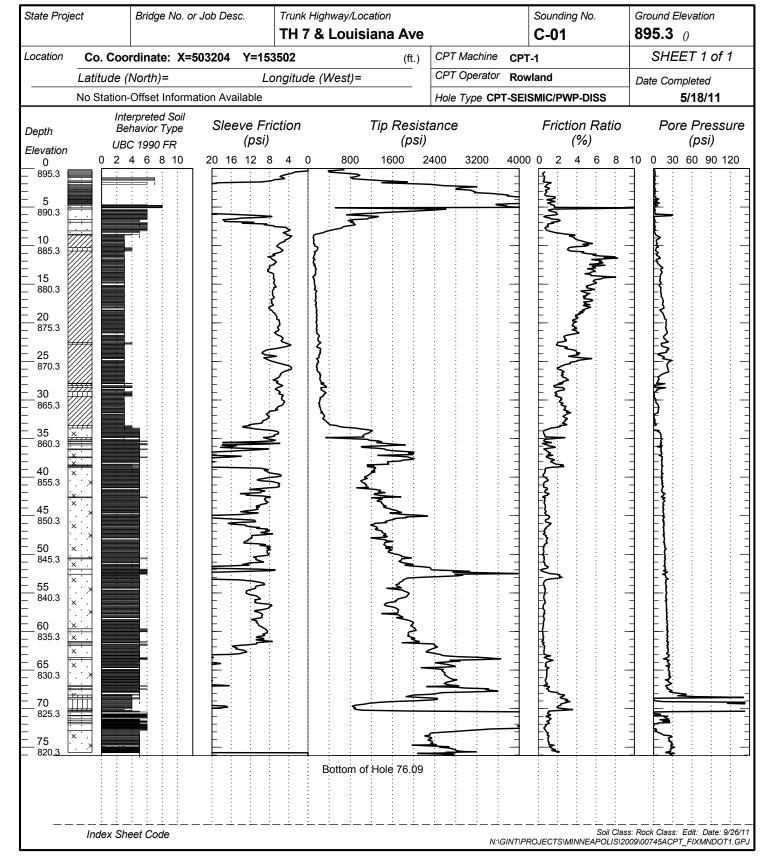




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



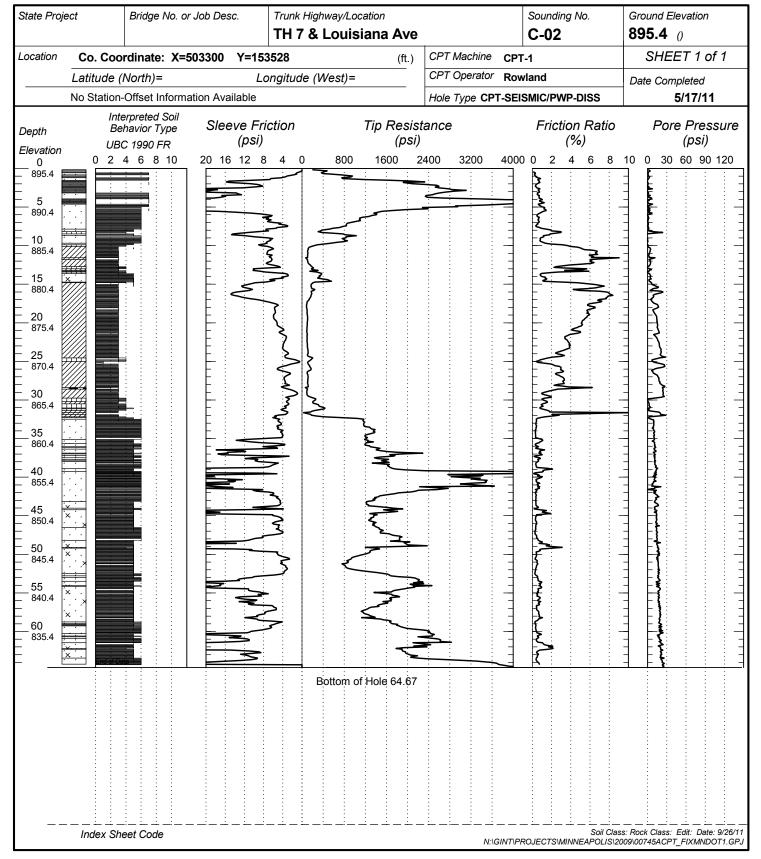




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



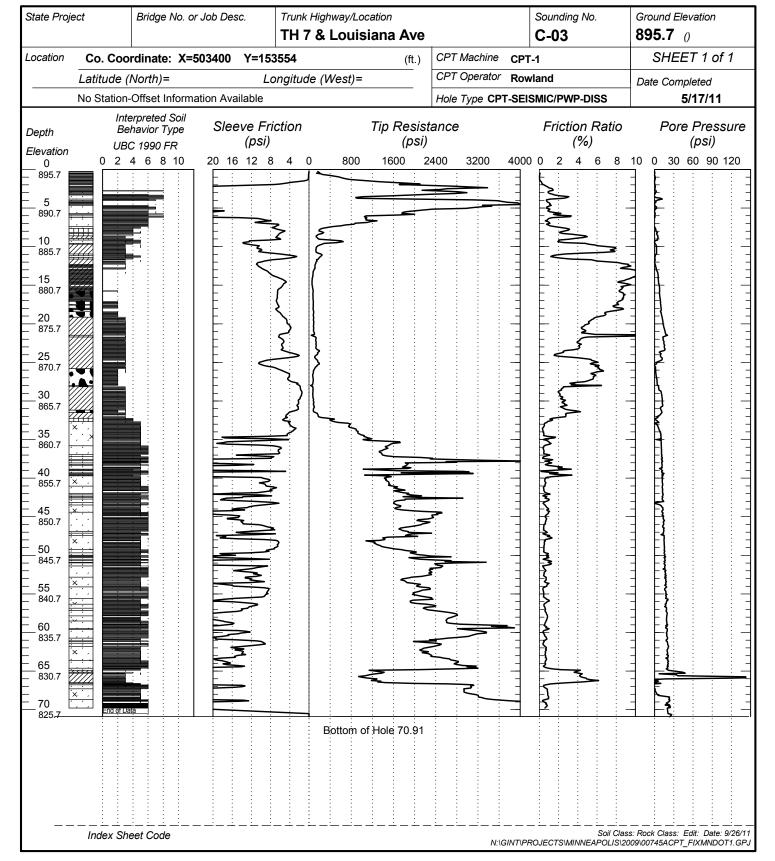




CONE PENETRATION TEST RESULTS

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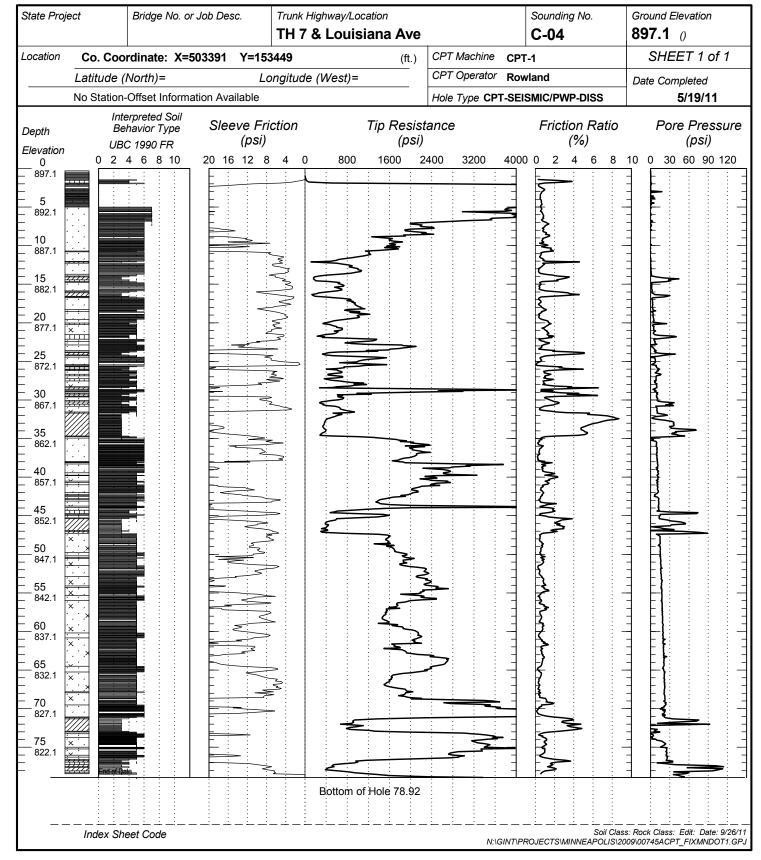




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



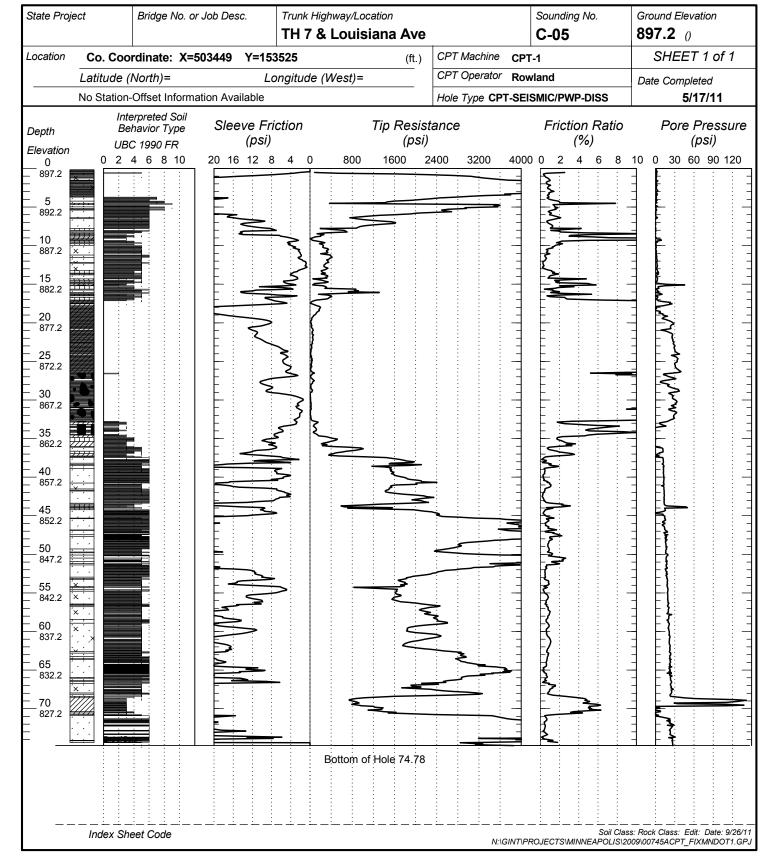




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



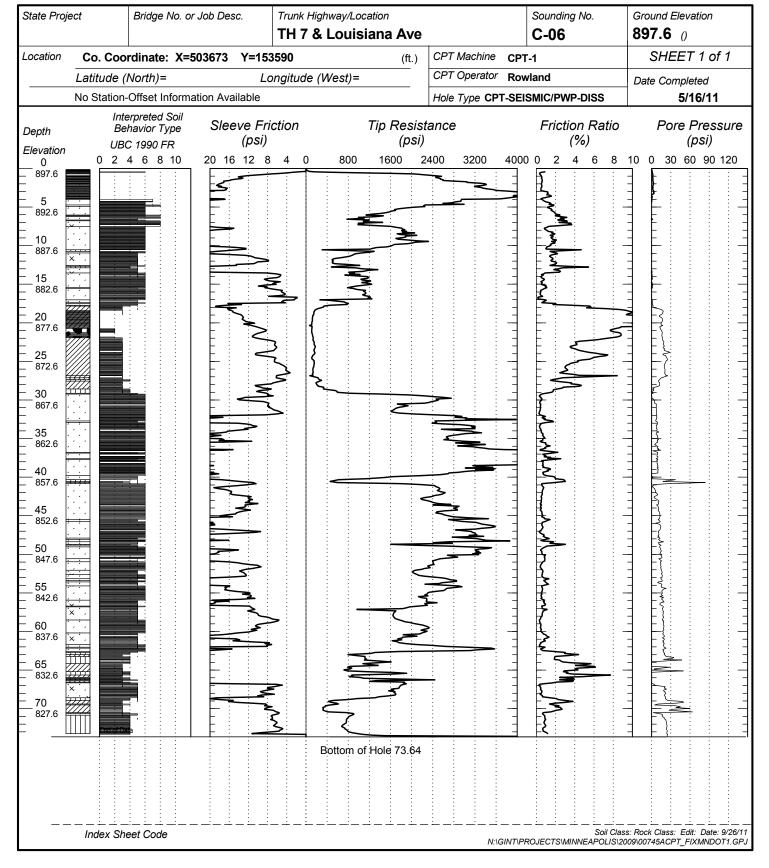




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER

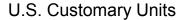




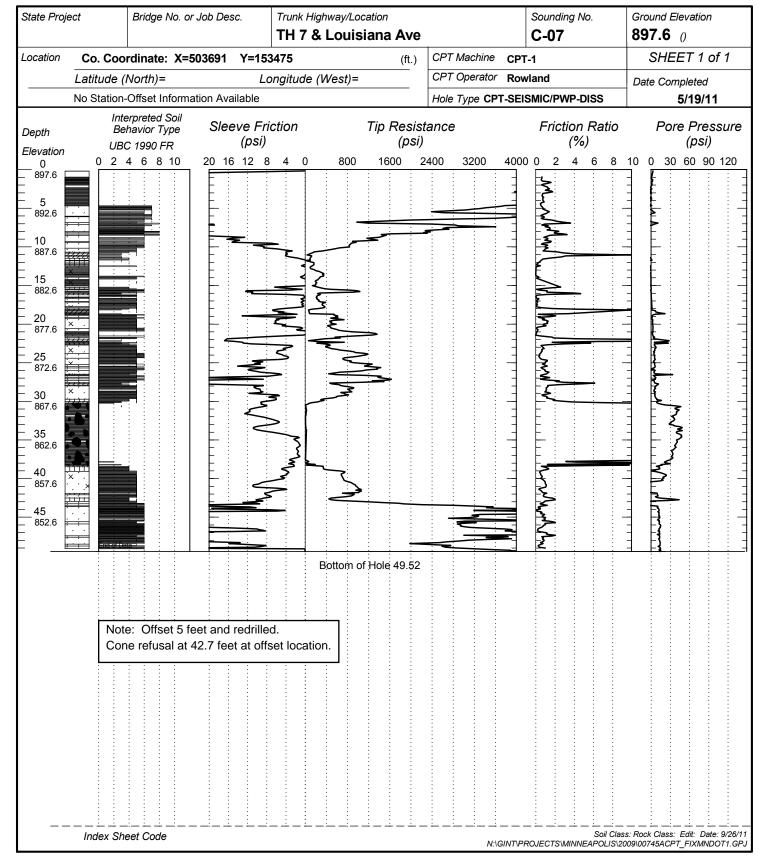


CONE PENETRATION TEST RESULTS

UNIQUE NUMBER





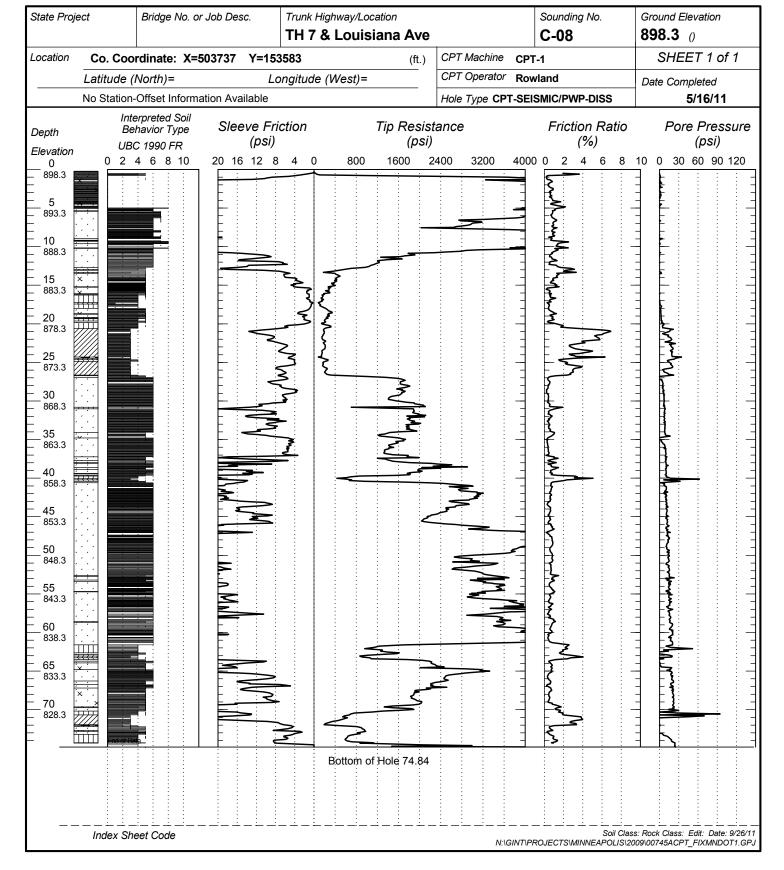




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



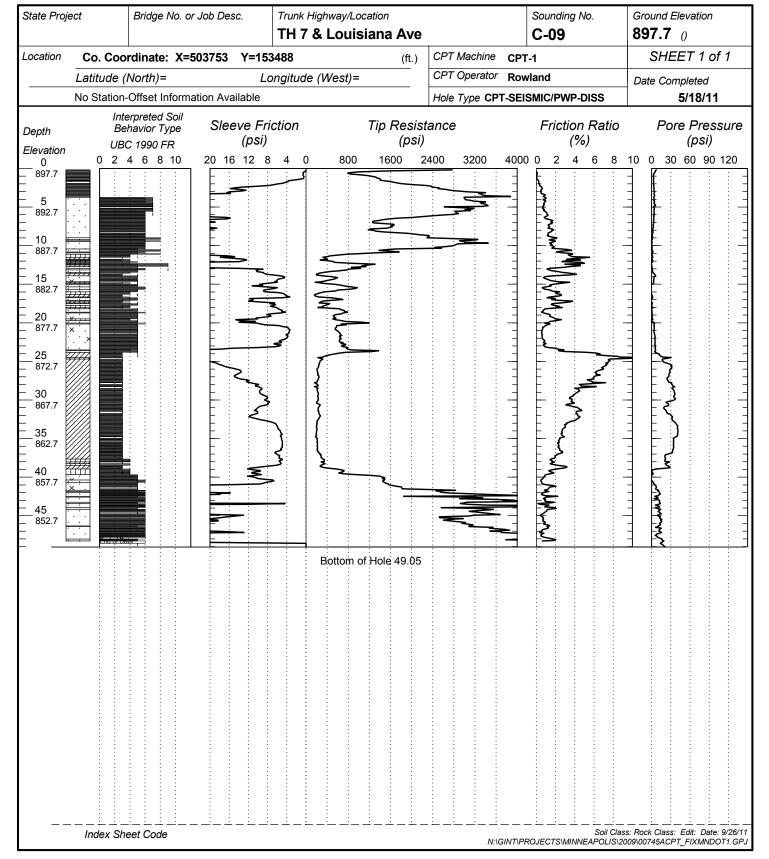




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



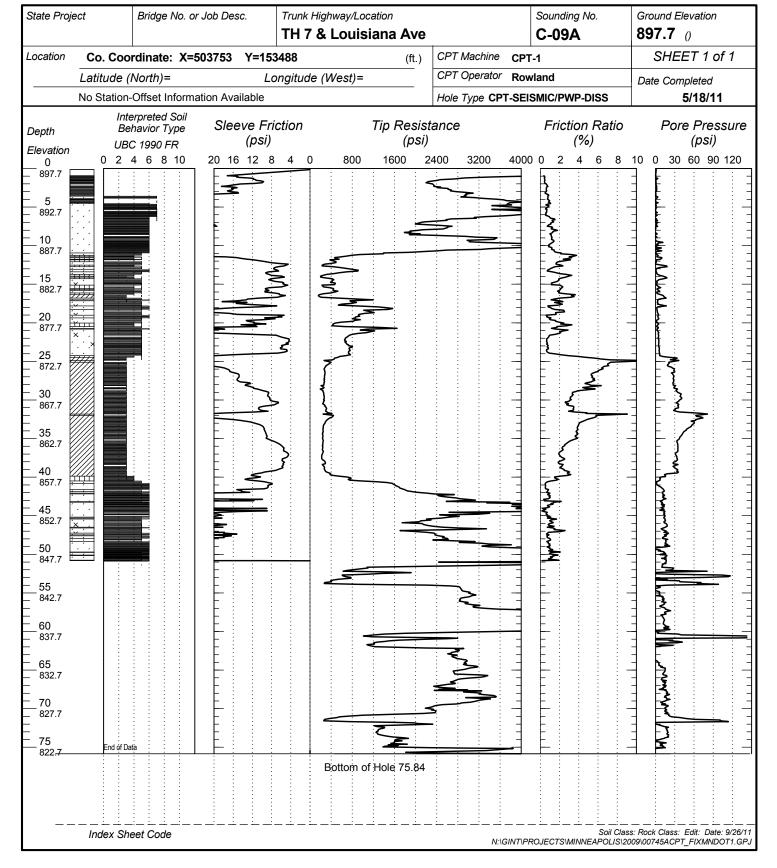




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UNIQUE NUMBER



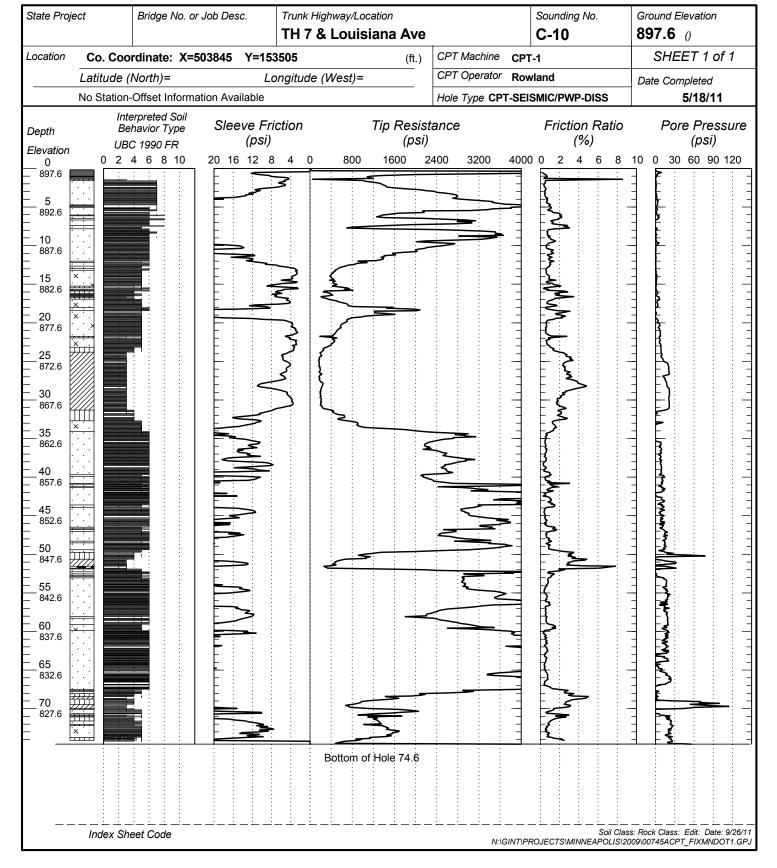




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER



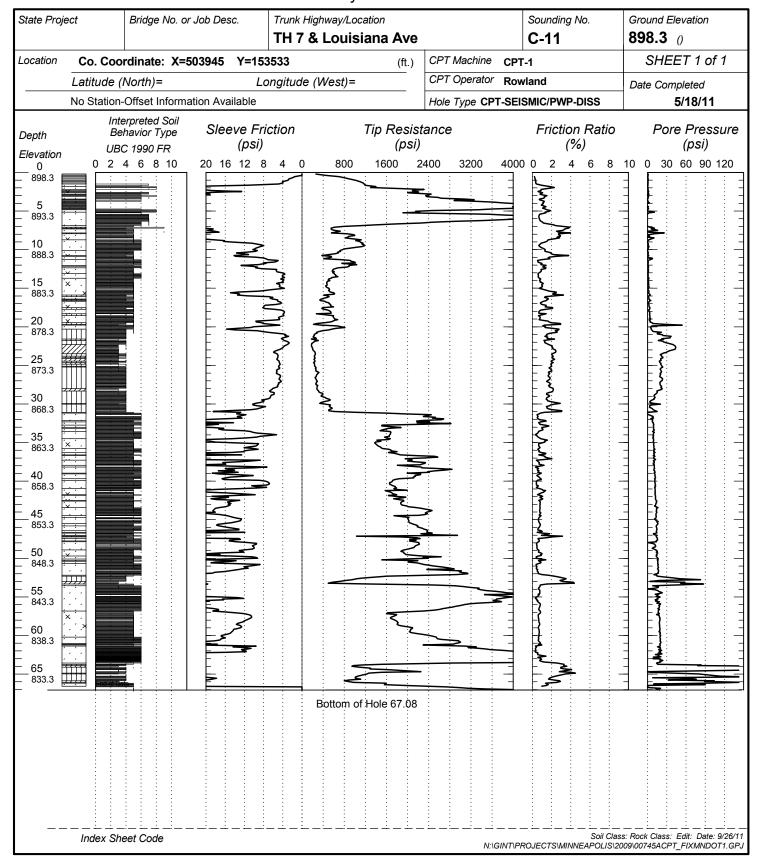




CONE PENETRATION TEST RESULTS

WINNESON DE 1841

UNIQUE NUMBER

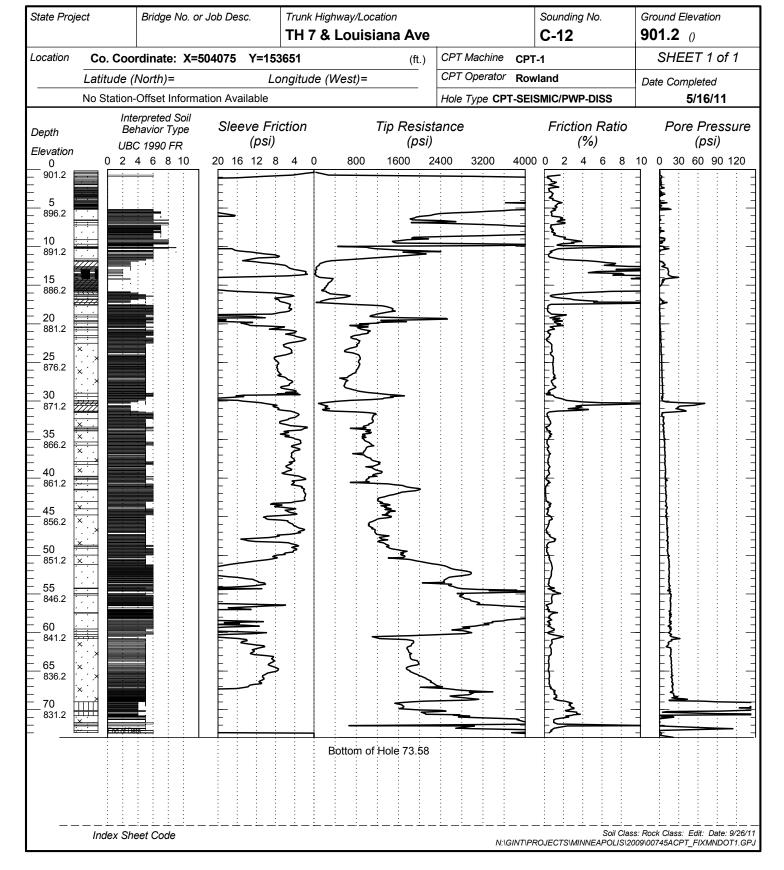




CONE PENETRATION TEST RESULTS

UNIQUE NUMBER







GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL** 7.7% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 86.1% TH 7 & Louisiana Ave Design **FINES** 6.2% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: B-1 DEPTH: 2.5'

BL-09-00745A

Braun Intertec Corporation

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1" 3/4" 1/2" 3/8" 10 20 40 60 100 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: Loamy SAND **GRAVEL** 17.3% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 70.4% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 12.3% **INTERTEC** St. Louis Park, Minnesota BORING: B-2 DEPTH: 1.0'

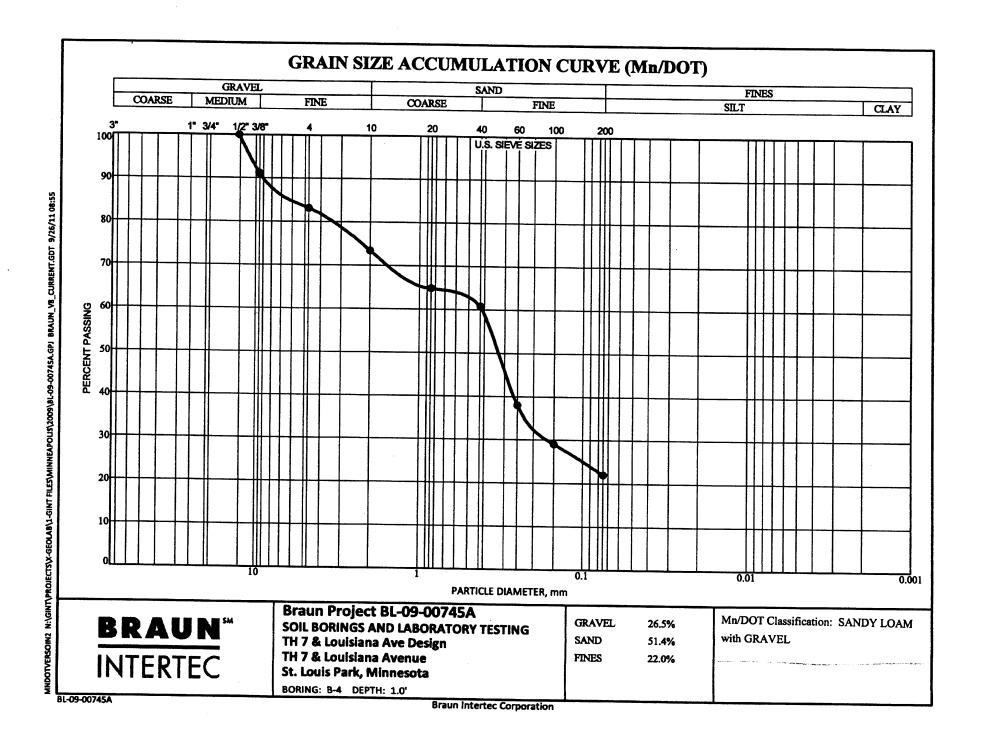
Braun Intertec Corporation

BL-09-00745A

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** MEDIUM COARSE FINE COARSE FINE SILT CLAY 3/4" 1/2" 3/8" 10 20 40 60 100 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SANDY LOAM **GRAVEL** 26.2% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 46.7% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 27.1% **INTERTEC** St. Louis Park, Minnesota BORING: B-3 DEPTH: 2.5'

Braun Intertec Corporation

BL-09-00745A



GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1/2" 3/8" 10 20 40 200 100 U.S. SIEVE SIZES MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 20 0.01 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: Loamy SAND **GRAVEL** 13.1% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 70.9% TH 7 & Louisiana Ave Design **INTERTEC TH 7 & Louisiana Avenue FINES** 16.0% St. Louis Park, Minnesota BORING: B-5 DEPTH: 1.5' BL-09-00745A

Braun Intertec Corporation

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE CLAY SILT 1" 3/4" 1/2" 3/8" 60 100 200 U.S. SIEVE SIZES PERCENT PASSING 0.001 **PARTICLE DIAMETER, mm** Braun Project BL-09-00745A Mn/DOT Classification: Loamy SAND **GRAVEL** 25.8% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 60.1% with GRAVEL TH 7 & Louisiana Ave Design TH 7 & Louisiana Avenue INTERTEC FINES 14.2% St. Louis Park, Minnesota BORING: B-8 DEPTH: 2.5' BL-09-00745A **Braun Intertec Corporation**

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) **GRAVEL** SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1" 3/4" 1/2" 3/8" 10 20 40 60 100 200 100 U.S. SIEVE SIZES MNDOTVERSOIN2 N.\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: Loamy SAND **GRAVEL** 23.1% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 63.3% TH 7 & Louisiana Ave Design **FINES** 13.6% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: B-9 DEPTH: 2.5'

Braun Intertec Corporation

BL-09-00745A

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) **GRAVEL** SAND **FINES** COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1" 3/4" 10 20 40 60 100 200 100 U.S. SIEVĖ SIZES MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: Loamy SAND **GRAVEL** 22.3% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 63.6% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue** FINES 14.2% **INTERTEC** St. Louis Park, Minnesota BORING: B-11 DEPTH: 2.5'

BL-09-00745A

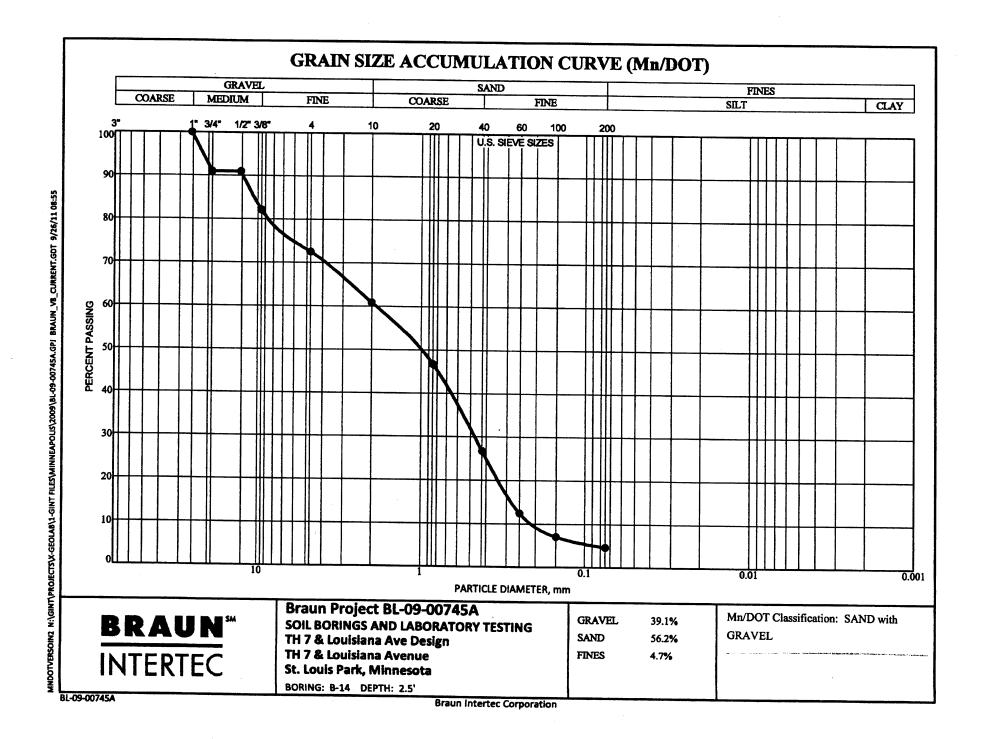
Braun Intertec Corporation

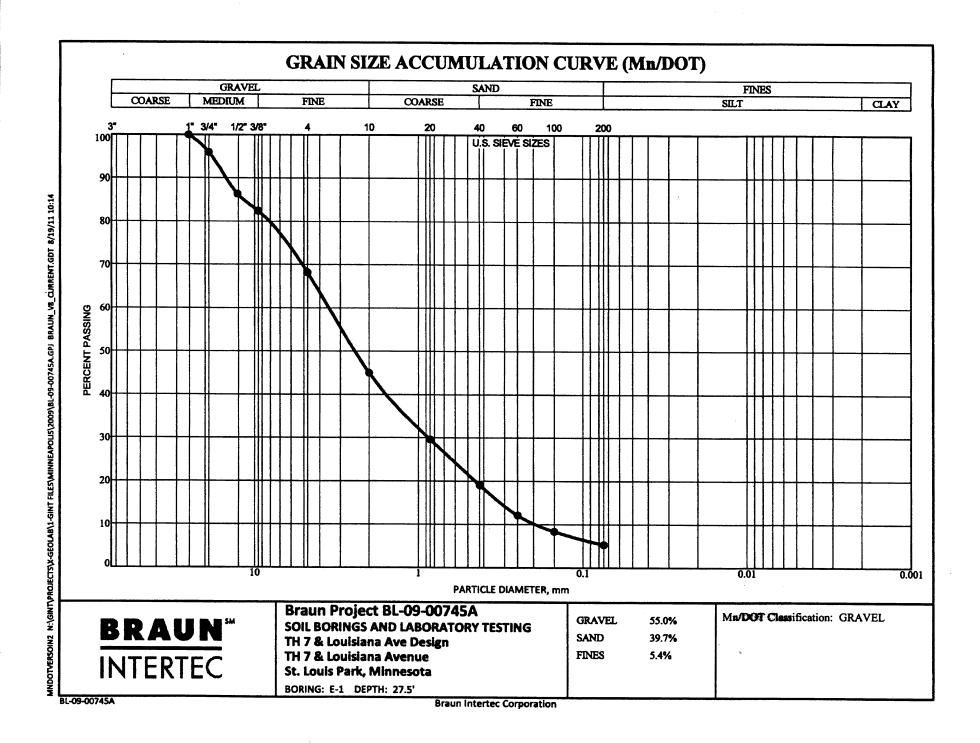
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1/2" 3/8" 10 20 60 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND GRAVEL 24.2% **BRAUN**** **SOIL BORINGS AND LABORATORY TESTING** SAND 71.1% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 4.7% **INTERTEC** St. Louis Park, Minnesota BORING: B-12 DEPTH: 2.5' BL-09-00745A **Braun Intertec Corporation**

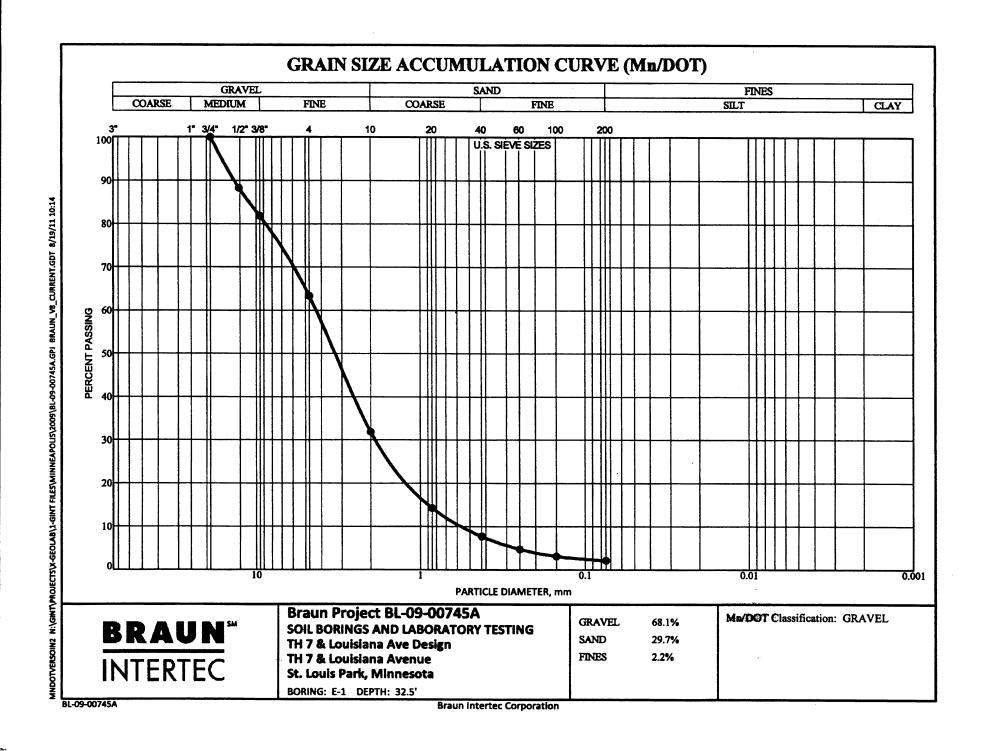
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE **MEDIUM** FINE COARSE FINE SILT CLAY 3" 1/2" 3/8" 10 20 40 60 100 200 100 U.S. SIEVE SIZES MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 30 20 0.01 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SANDY LOAM GRAVEL 23.9% **BRAUN[™] SOIL BORINGS AND LABORATORY TESTING** SAND 55.2% TH 7 & Louisiana Ave Design TH 7 & Louisiana Avenue **FINES** 20.9% **INTERTEC** St. Louis Park, Minnesota BORING: B-13 DEPTH: 2.5'

Braun Intertec Corporation

BL-09-00745A



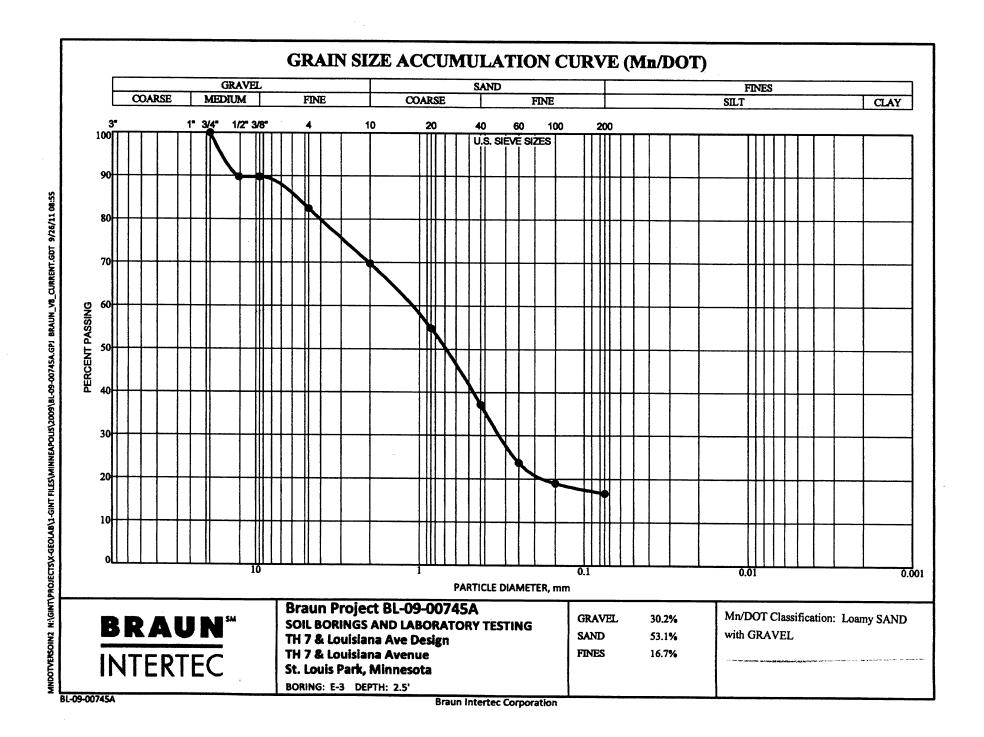


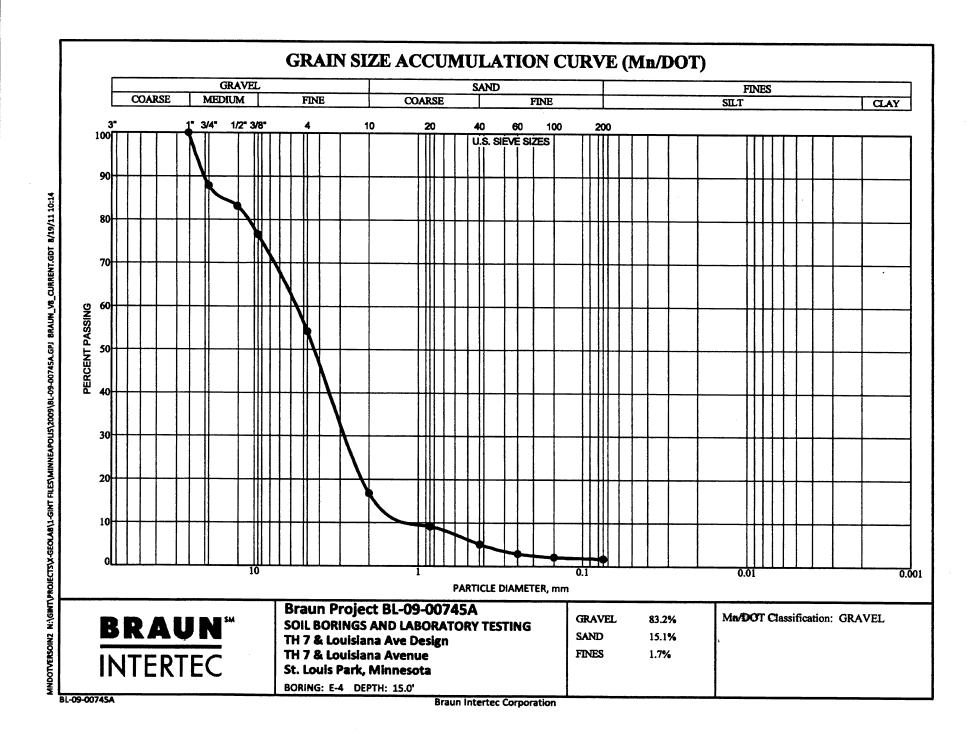


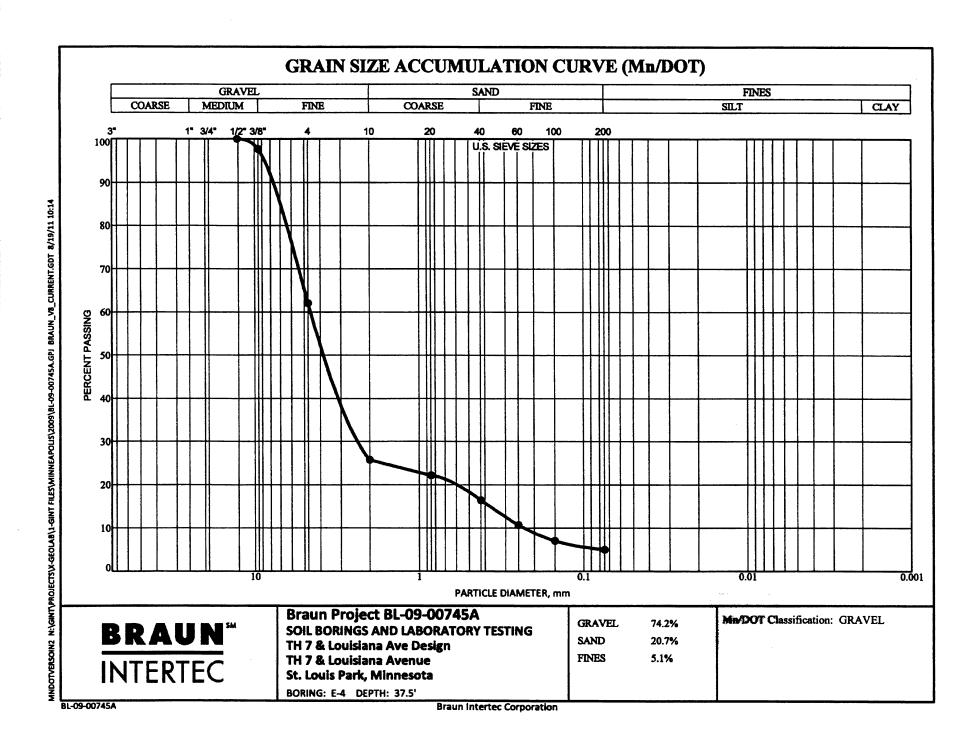
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1<u>/</u>2" 3/8" 10 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND GRAVEL 24.4% **BRAUN**[™] SOIL BORINGS AND LABORATORY TESTING SAND 75.2% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 0.4% **INTERTEC** St. Louis Park, Minnesota BORING: E-2 DEPTH: 37.5'

Braun Intertec Corporation

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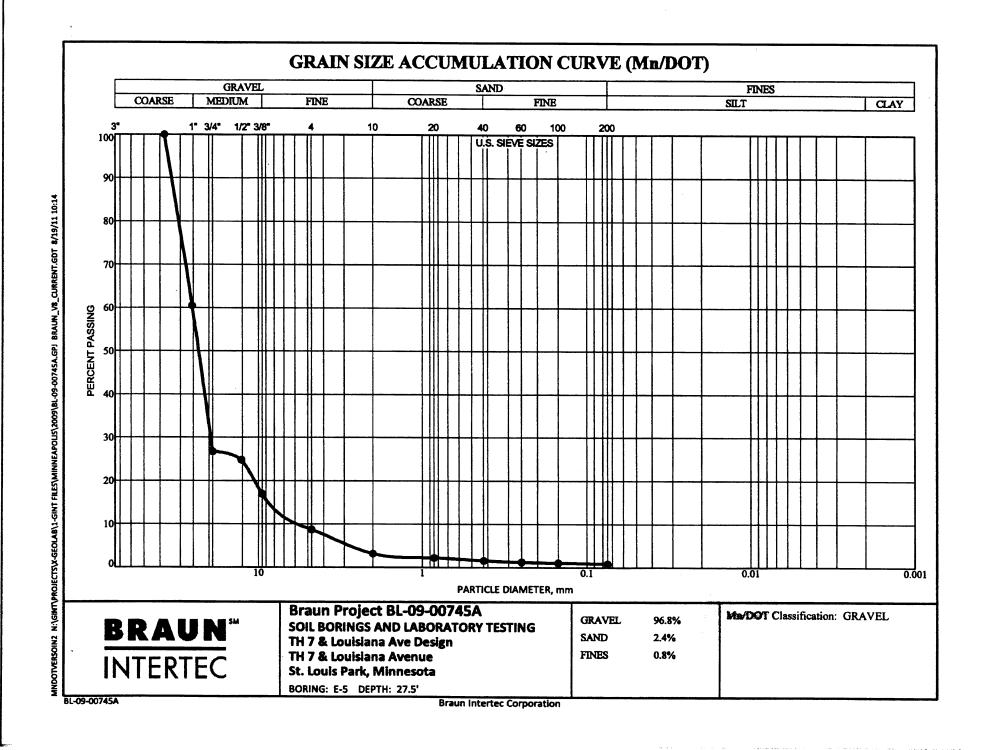






GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1/2" 3/8" 10 60 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND GRAVEL **BRAUN**[™] 21.2% **SOIL BORINGS AND LABORATORY TESTING** SAND 70.3% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 8.6% **INTERTEC** St. Louis Park, Minnesota BORING: E-5 DEPTH: 17.5'

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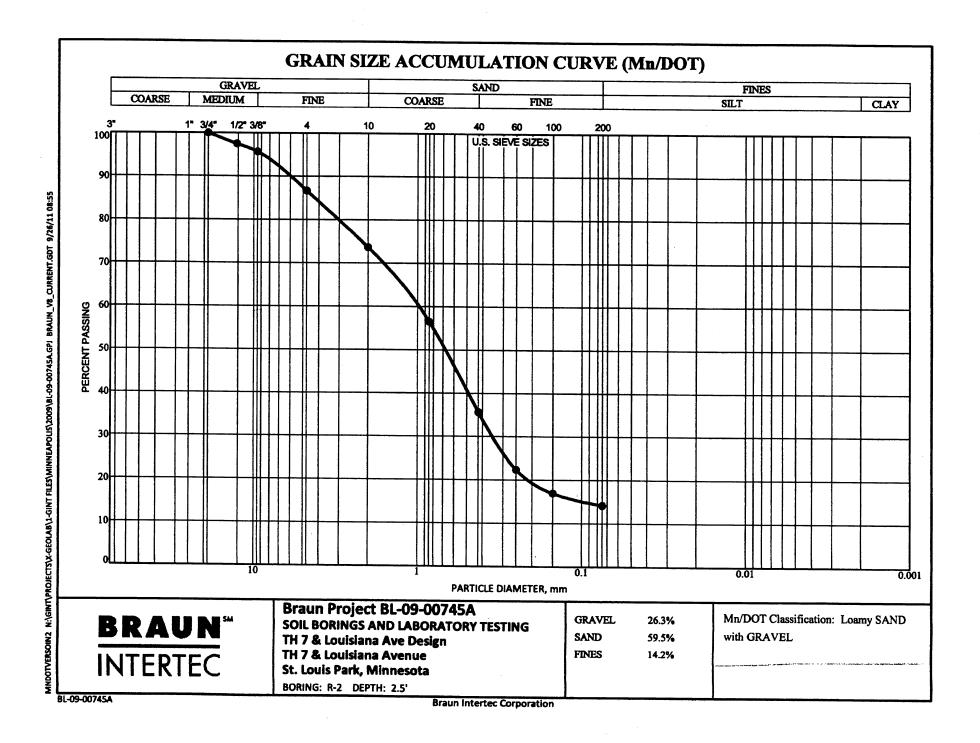
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 10 60 100 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL BRAUN**[™] 23.6% **SOIL BORINGS AND LABORATORY TESTING** SAND 75.2% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 1.1% **INTERTEC** St. Louis Park, Minnesota BORING: R-1 DEPTH: 30.0'

BL-09-00745A

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 10 60 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL** 20.6% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 77.4% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue** FINES 1.9% **INTERTEC** St. Louis Park, Minnesota BORING: R-1 DEPTH: 40.0'

BL-09-00745A

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1/2" 3/8" 10 60 100 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SANDY LOAM **BRAUN**[™] **GRAVEL** 0.7% **SOIL BORINGS AND LABORATORY TESTING** SAND 68.7% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 30.6% **INTERTEC** St. Louis Park, Minnesota BORING: R-1 DEPTH: 60.0' BL-09-00745A Braun Intertec Corporation



GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE FINE COARSE SILT CLAY 1" 3/4" 1<u>/</u>2" 3/8" 10 60 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND GRAVEL 9.0% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 89.6% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 1.4% **INTERTEC** St. Louis Park, Minnesota BORING: R-2 DEPTH: 35.0' BL-09-00745A **Braun Intertec Corporation**

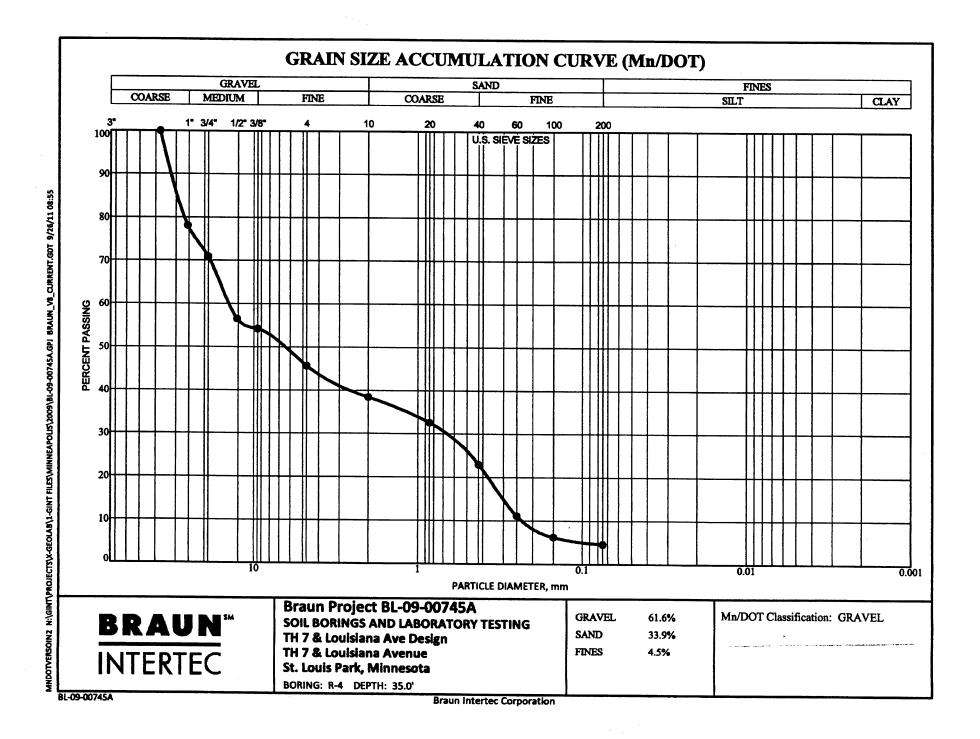
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 10 60 100 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **BRAUN**[™] **GRAVEL** 11.9% **SOIL BORINGS AND LABORATORY TESTING** SAND 82.6% TH 7 & Louisiana Ave Design FINES **TH 7 & Louisiana Avenue** 5.6% **INTERTEC** St. Louis Park, Minnesota BORING: R-2 DEPTH: 60.0' BL-09-00745A Braun Intertec Corporation

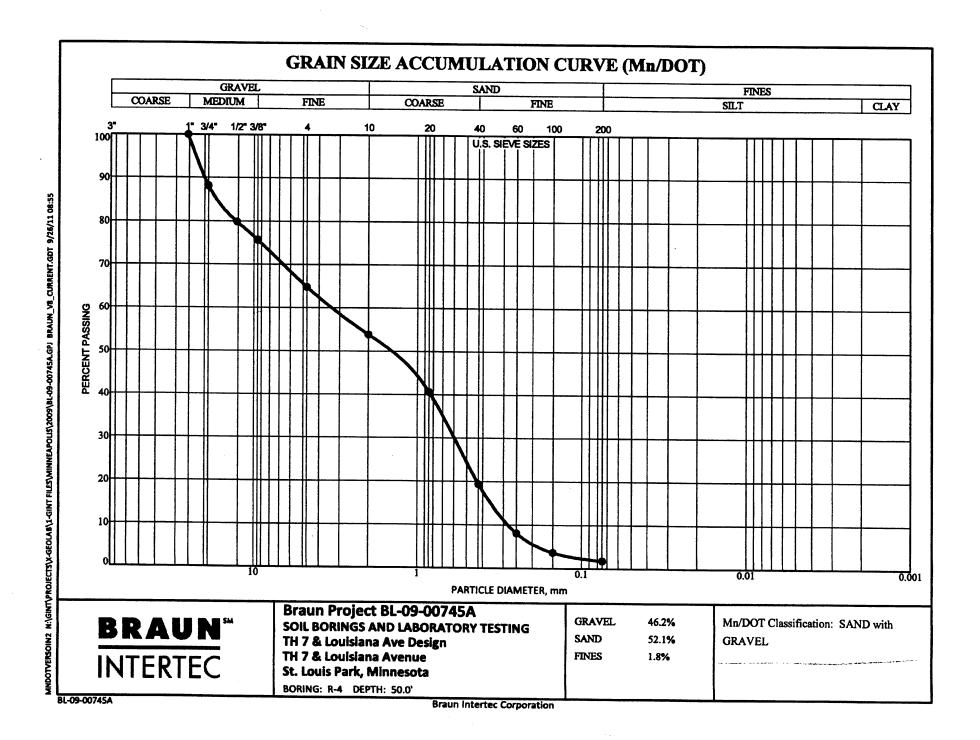
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1<u>/</u>2" 3/8" 100 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL BRAUN**[™] 8.4% **SOIL BORINGS AND LABORATORY TESTING** SAND 84.2% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 7.4% **INTERTEC** St. Louis Park, Minnesota BORING: R-2 DEPTH: 70.0' BL-09-00745A **Braun Intertec Corporation**

GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** COARSE **MEDIUM** FINE COARSE FINE SILT CLAY 1/2" 3/8" 10 100 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND **GRAVEL** 10.4% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 88.4% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 1.2% **INTERTEC** St. Louis Park, Minnesota BORING: R-3 DEPTH: 35.0'

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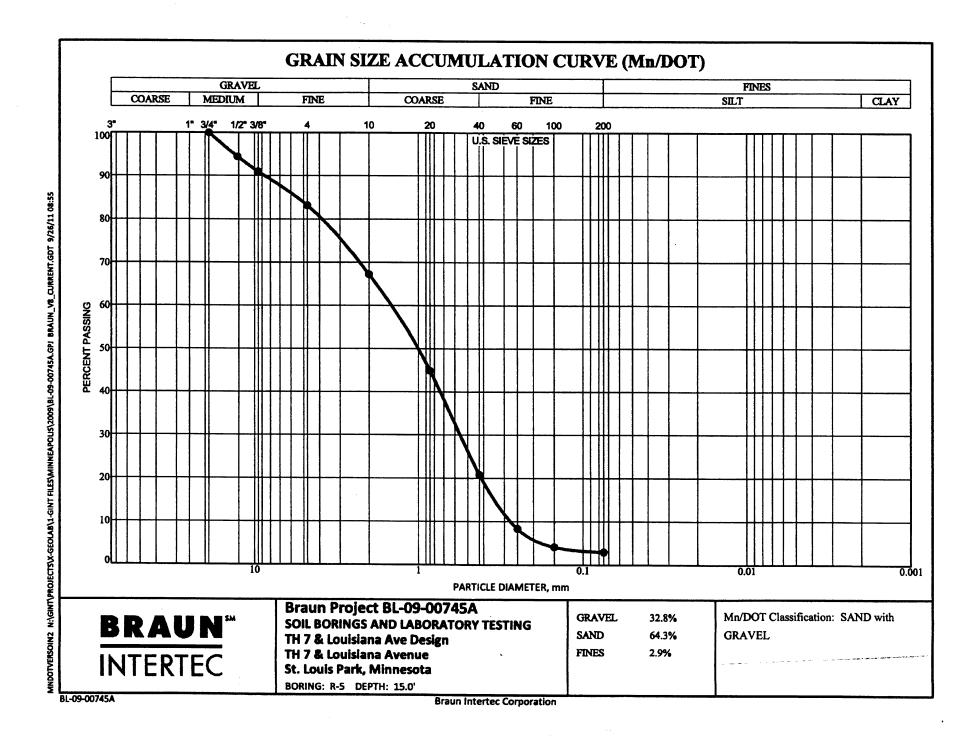
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 10 60 100 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL** 4.9% **BRAUN**[™] SOIL BORINGS AND LABORATORY TESTING SAND 89.1% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 6.0% **INTERTEC** St. Louis Park, Minnesota BORING: R-3 DEPTH: 50.0' BL-09-00745A **Braun Intertec Corporation**

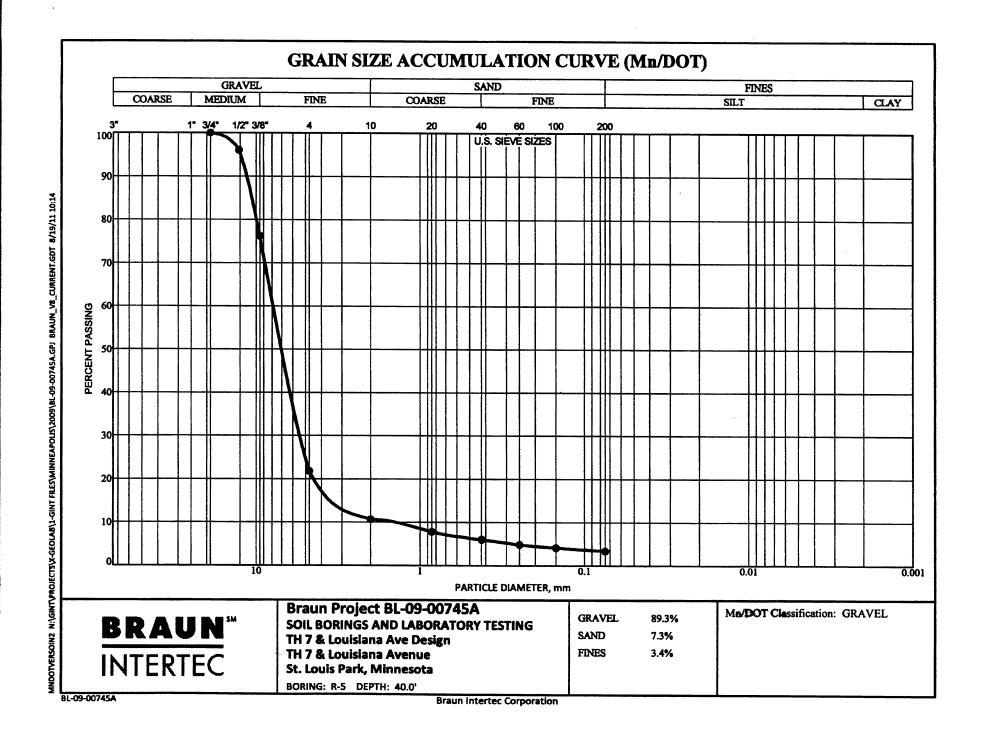


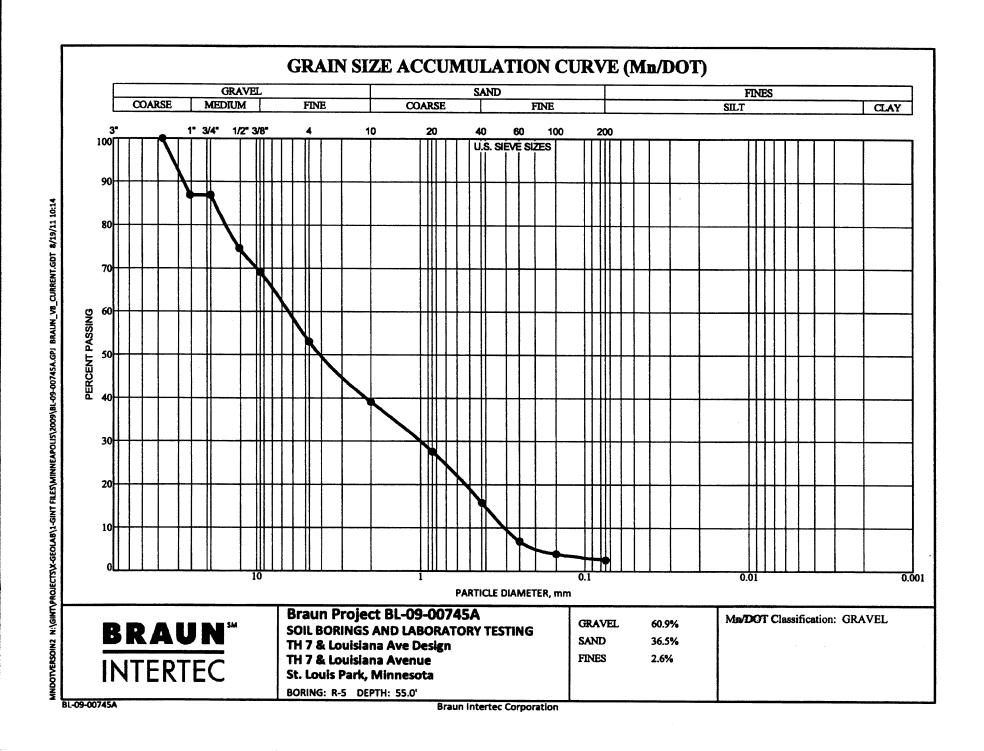


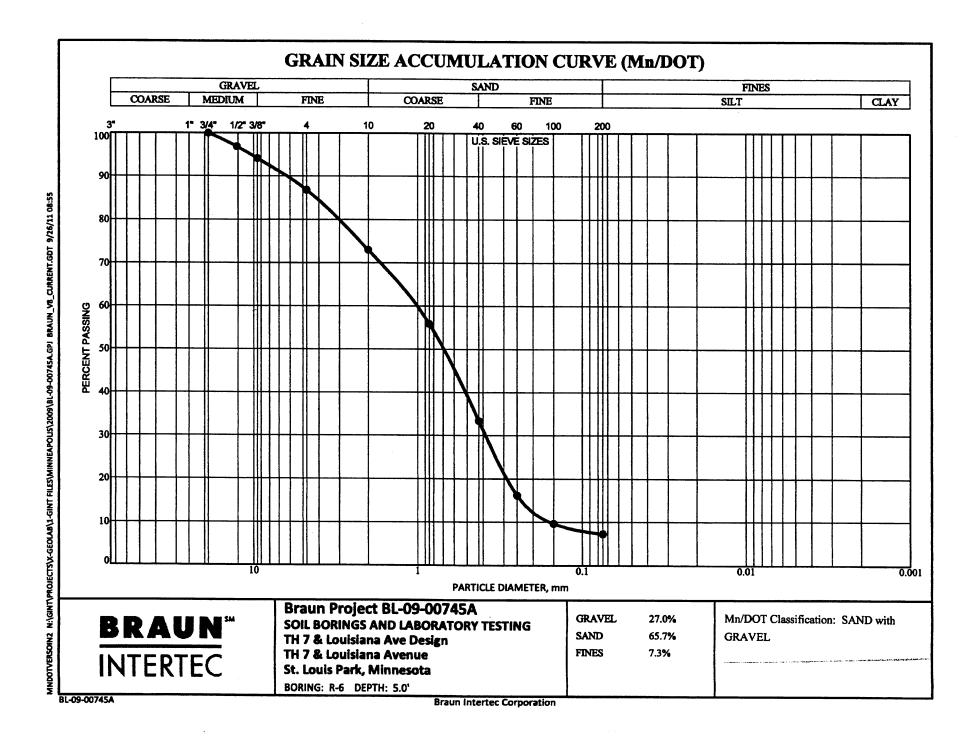
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND **FINES** COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL** 0.1% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 97.2% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 2.7% **INTERTEC** St. Louis Park, Minnesota BORING: R-4 DEPTH: 70.0'

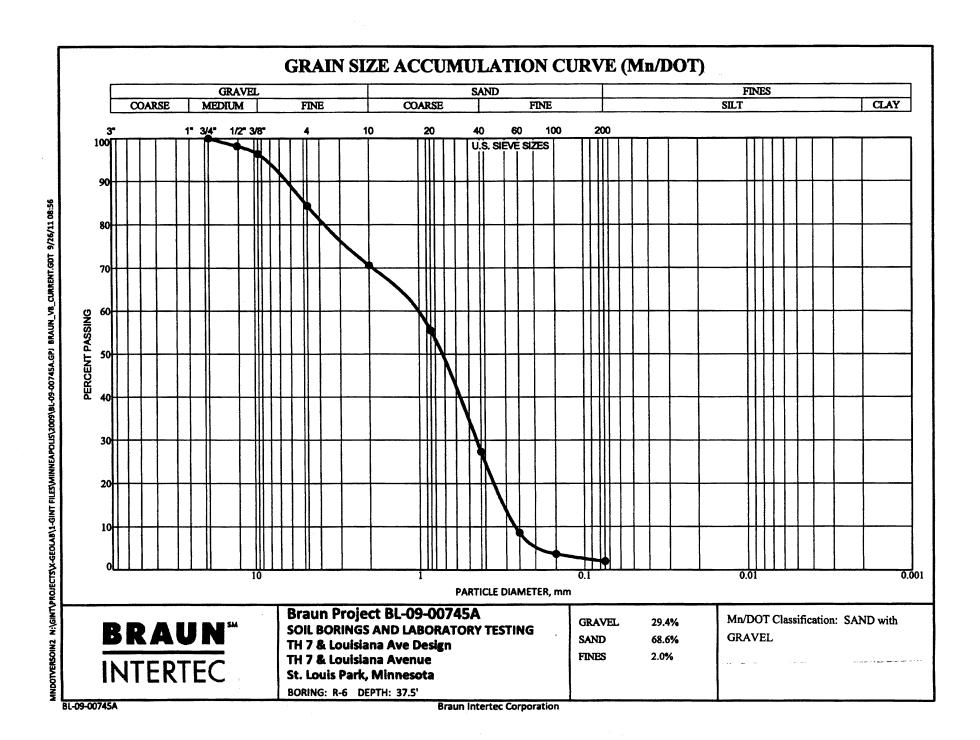
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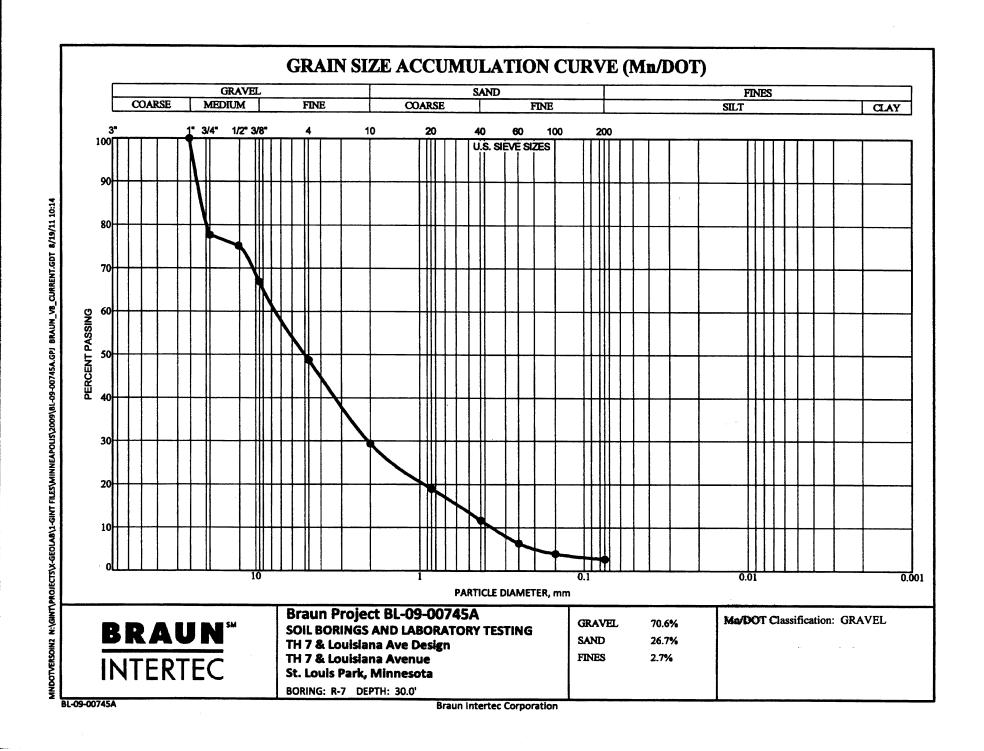
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3<u>/8</u>" 10 20 40 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND **GRAVEL** 1.0% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 96.0% TH 7 & Louisiana Ave Design **FINES** 3.0% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: R-6 DEPTH: 60.0'

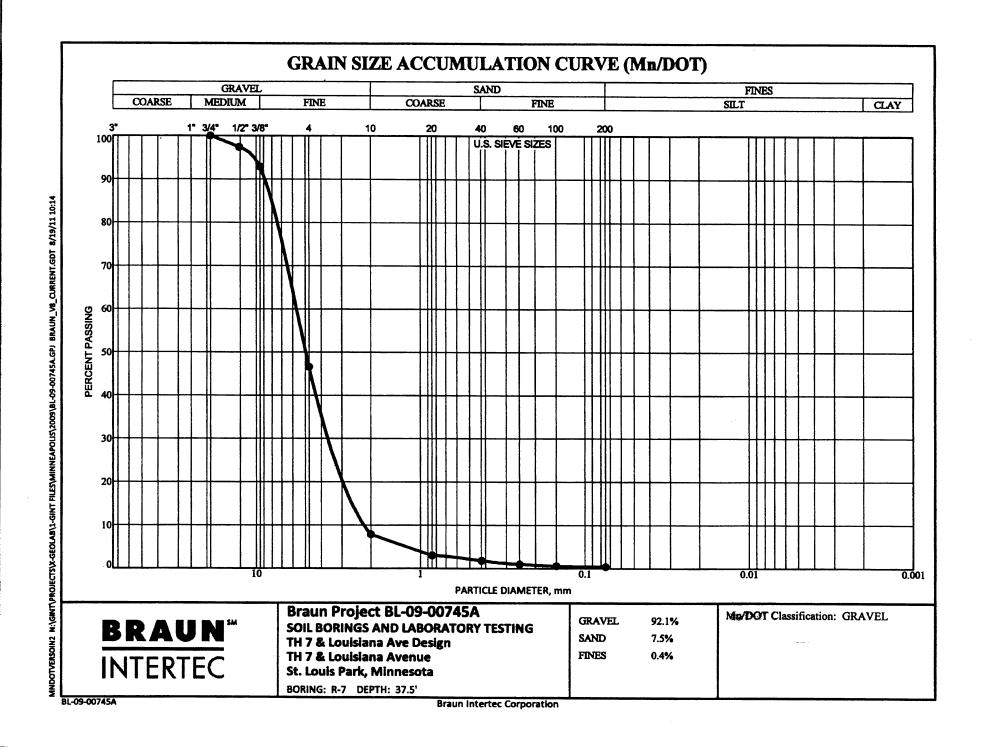
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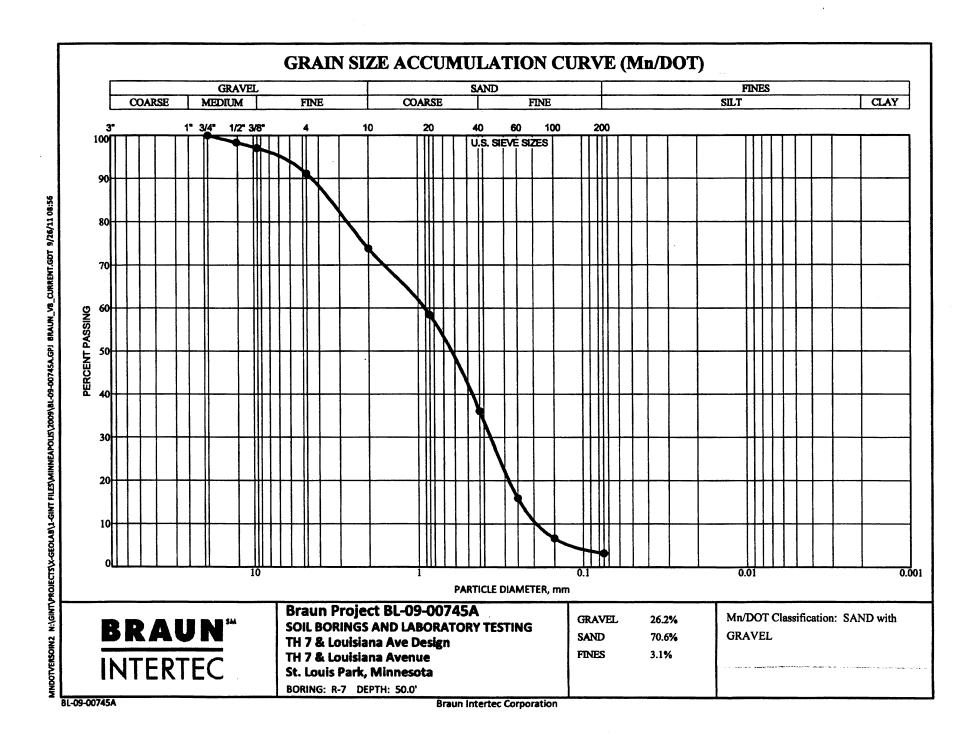
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1" 3/4" 1<u>/</u>2" 3/8" 10 20 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SANDY LOAM **GRAVEL** 14.0% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 54.0% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 31.9% **INTERTEC** St. Louis Park, Minnesota BORING: R-6 DEPTH: 70.01

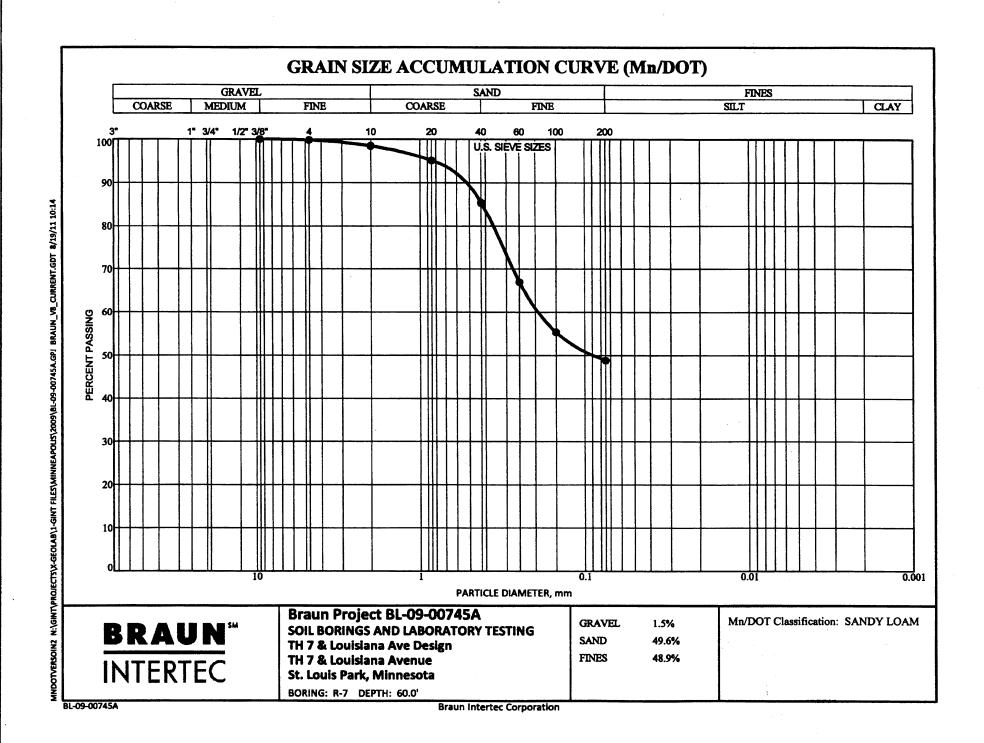
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GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 10 40 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N'\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 80 70 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: SAND **GRAVEL** 4.0% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 87.7% TH 7 & Louisiana Ave Design **FINES** 8.4% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: R-7 DEPTH: 10.0' BL-09-00745A **Braun Intertec Corporation**



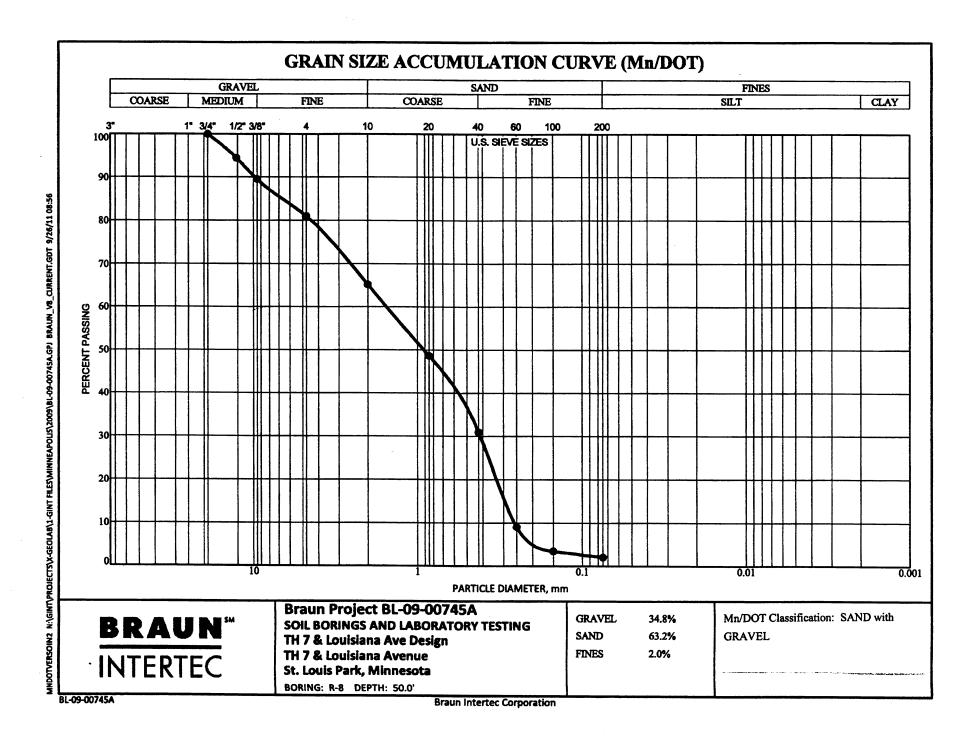






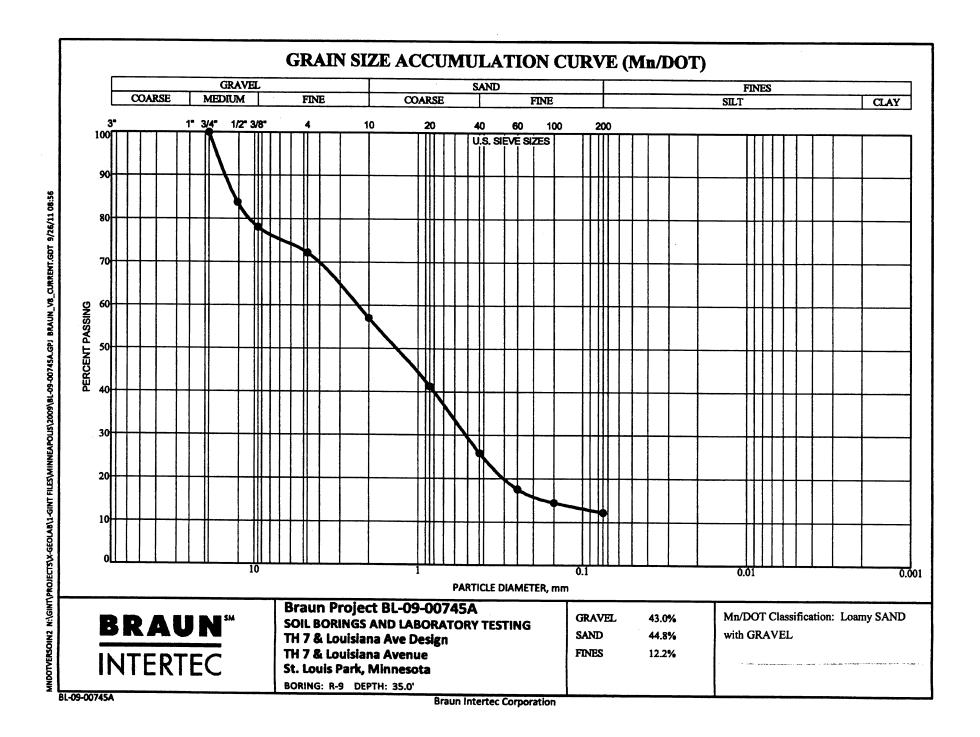
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1" 3/4" 1/2" 3/8" 10 200 100 U.S. SIEVĖ SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND **GRAVEL** 20.4% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 76.5% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 3.1% **INTERTEC** St. Louis Park, Minnesota BORING: R-8 DEPTH: 32.5'

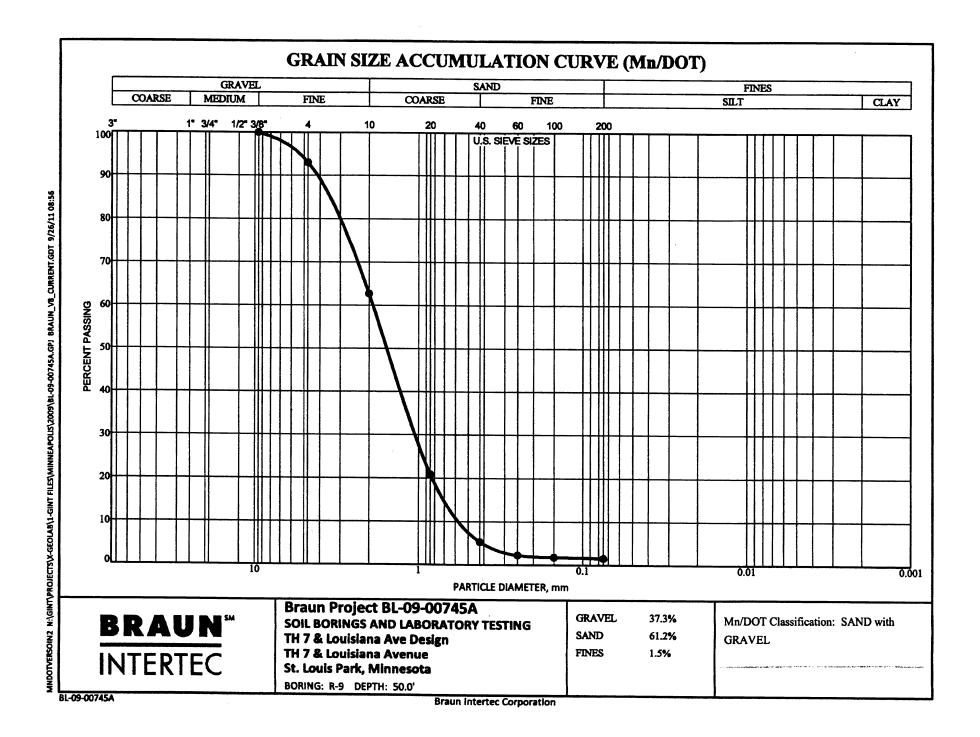
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GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 10 20 40 60 100 200 100**[** U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 PERCENT PASSING 30 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SANDY LOAM **GRAVEL** 10.8% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 59.9% TH 7 & Louisiana Ave Design TH 7 & Louisiana Avenue **FINES** 29.3% **INTERTEC** St. Louis Park, Minnesota BORING: R-8 DEPTH: 60.0'

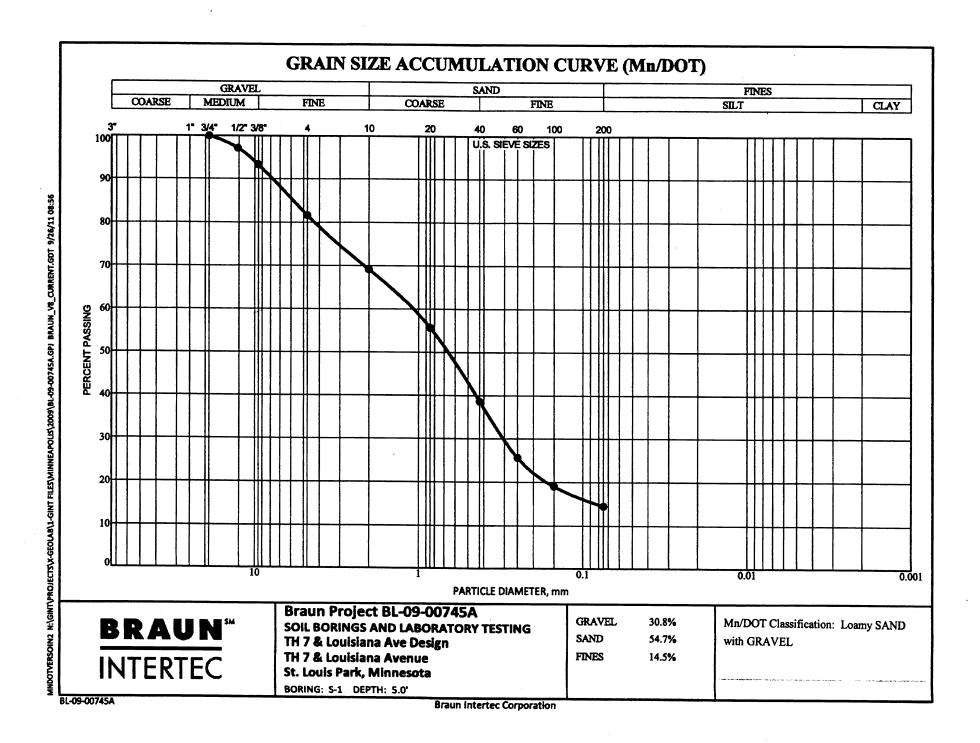
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GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 3" 1" 3/4" 1/2" 3/8" 10 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 PERCENT PASSING 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND **GRAVEL** 0.8% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 96.3% TH 7 & Louisiana Ave Design **FINES TH 7 & Louisiana Avenue** 2.9% **INTERTEC** St. Louis Park, Minnesota BORING: R-9 DEPTH: 60.0'

BL-09-00745A



GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES MEDIUM COARSE FINE COARSE FINE SILT CLAY 10 60 100 U.S. SIEVE SIZES 90 80 PERCENT PASSING MNDOTVERSOIN2 N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ 20 0.001 PARTICLE DIAMETER, mm **Braun Project BL-09-00745A** Mn/DOT Classification: Loamy SAND **GRAVEL** 18.0% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 68.8% TH 7 & Louisiana Ave Design **FINES** 13.2% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: S-12 DEPTH: 3.0

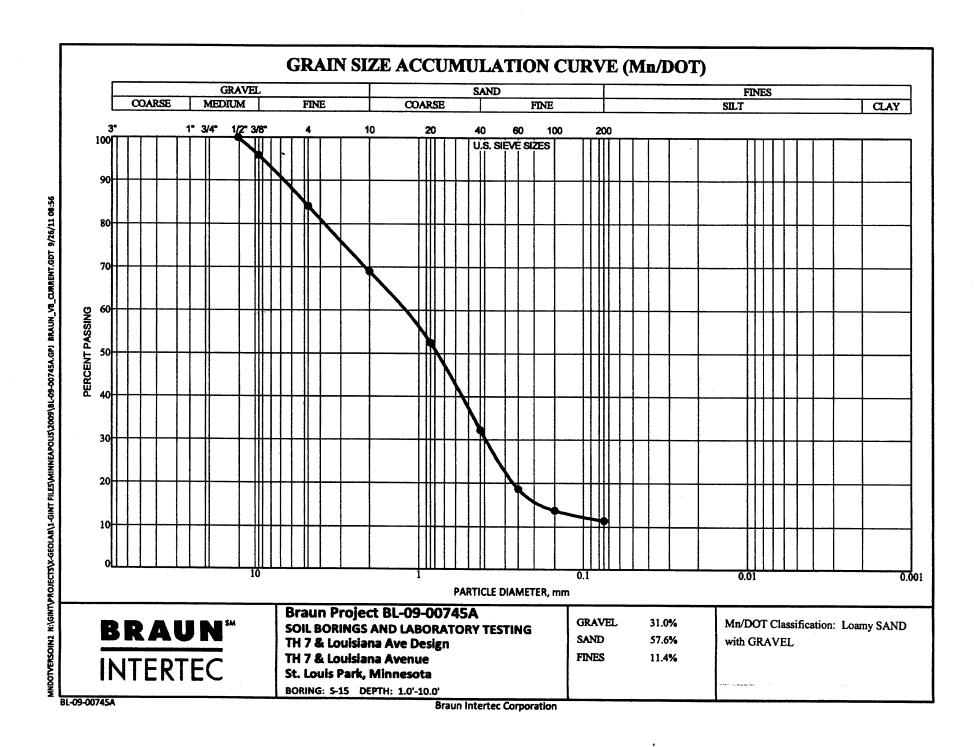
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GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1<u>/</u>2" 3/8" 10 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SANDY LOAM **GRAVEL** 19.6% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 59.7% TH 7 & Louisiana Ave Design **FINES** 20.7% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: S-13 DEPTH: 2.0'-7.0'

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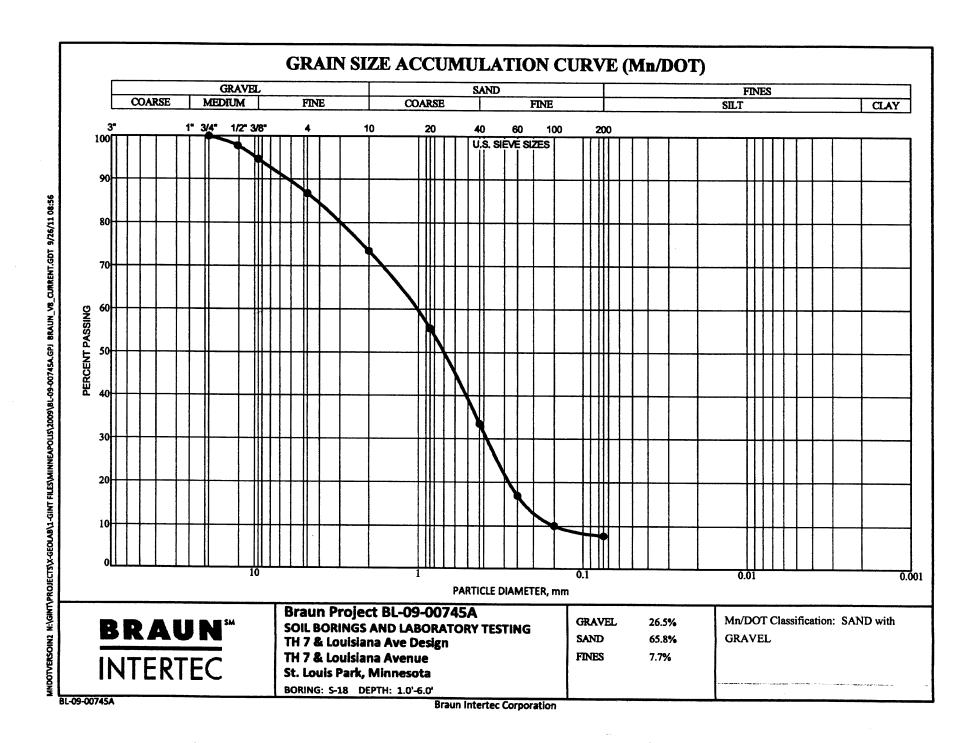
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 1" 3/4" 1/2" 3/8" 10 200 100 U.S. SIEVE SIZES 90 MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9\26/11 10:44 80 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: Loamy SAND **GRAVEL** 11.8% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 72.1% TH 7 & Louisiana Ave Design FINES 16.1% **TH 7 & Louisiana Avenue INTERTEC** St. Louis Park, Minnesota BORING: S-14 DEPTH: 3.0'

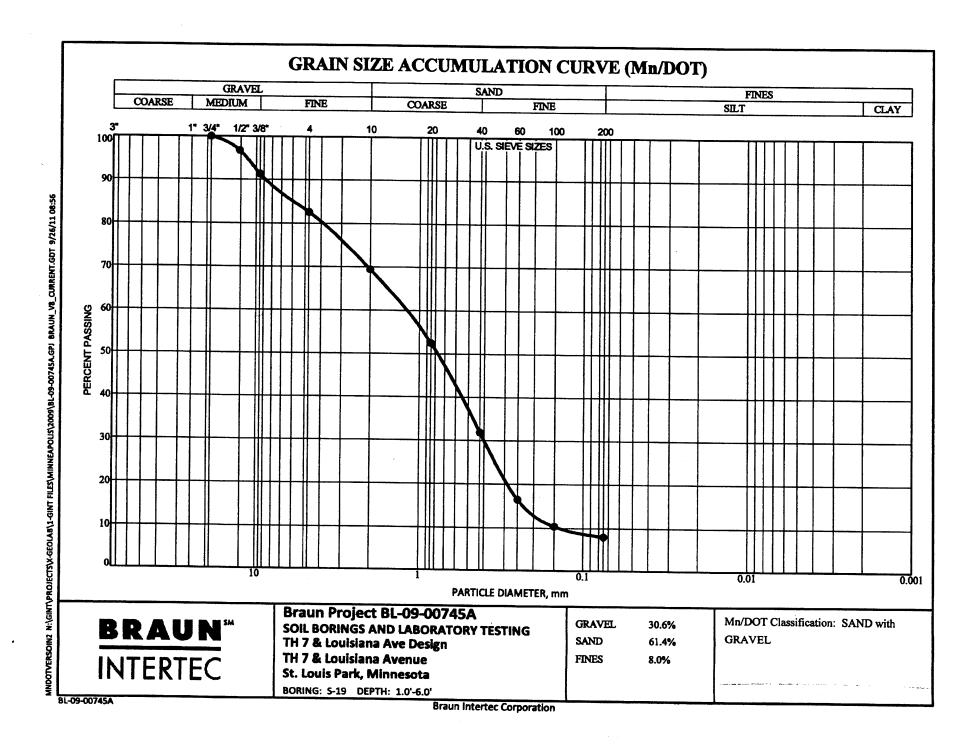
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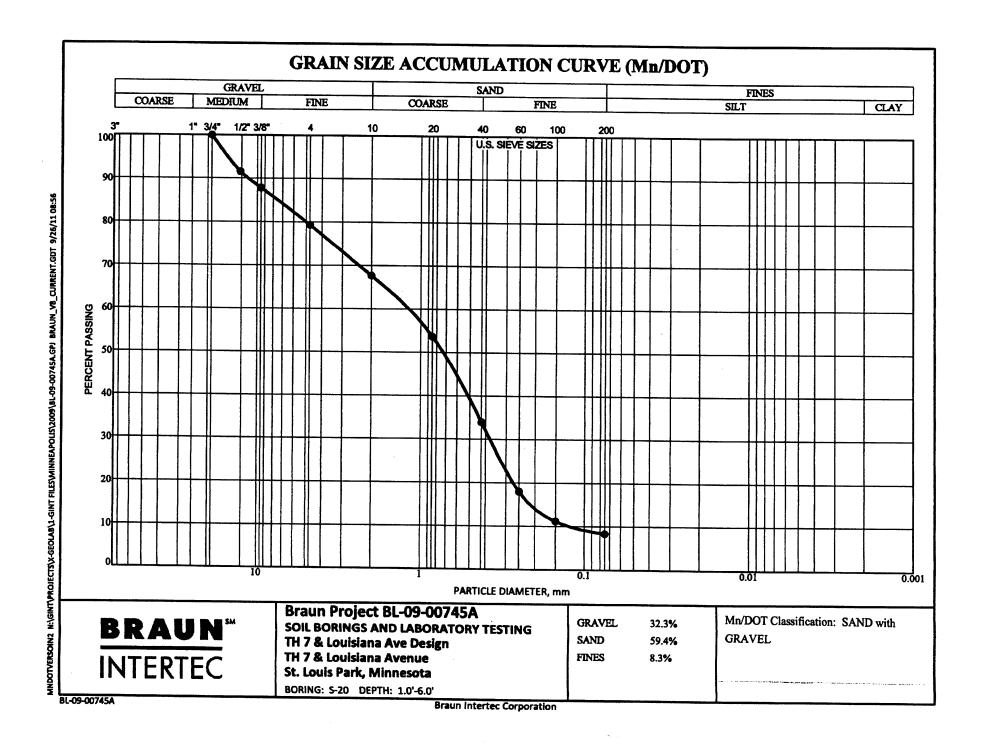


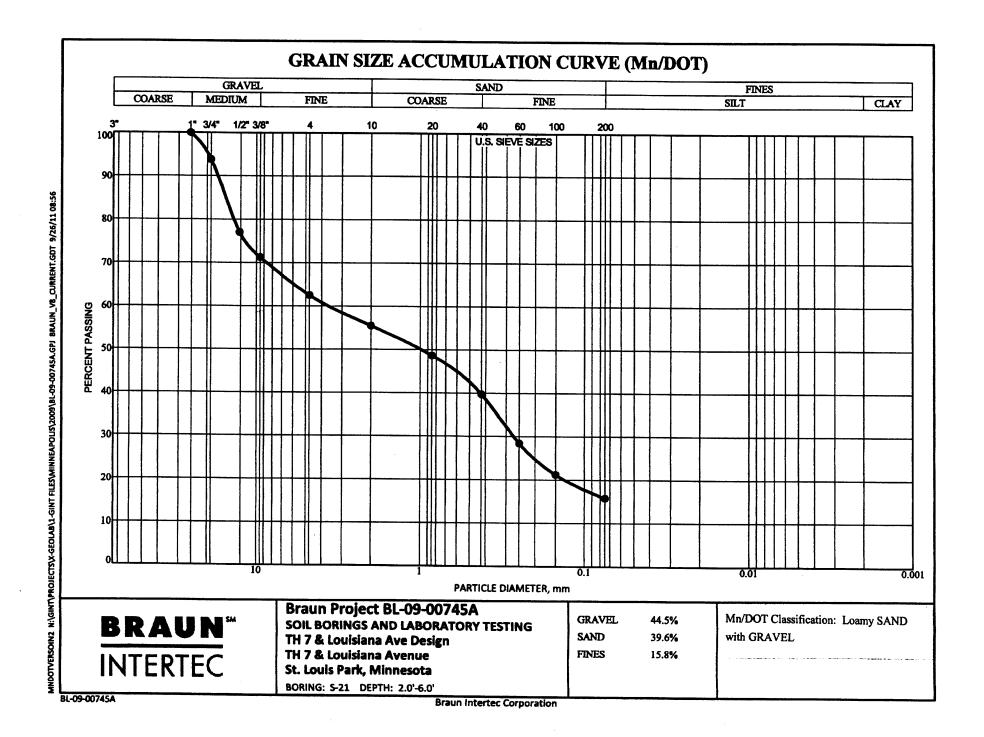
GRAIN SIZE ACCUMULATION CURVE (Mn/DOT) GRAVEL SAND FINES COARSE MEDIUM FINE COARSE FINE SILT CLAY 10 20 40 100 200 100 U.S. SIEVE SIZES MNDOTVERSOINZ N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 9/26/11 10:44 70 PERCENT PASSING 20 0.001 PARTICLE DIAMETER, mm Braun Project BL-09-00745A Mn/DOT Classification: SAND **GRAVEL** 17.4% **BRAUN**[™] **SOIL BORINGS AND LABORATORY TESTING** SAND 78.9% TH 7 & Louisiana Ave Design **TH 7 & Louisiana Avenue FINES** 3.6% **INTERTEC** St. Louis Park, Minnesota BORING: S-17 DEPTH: 3.0'-6.0'

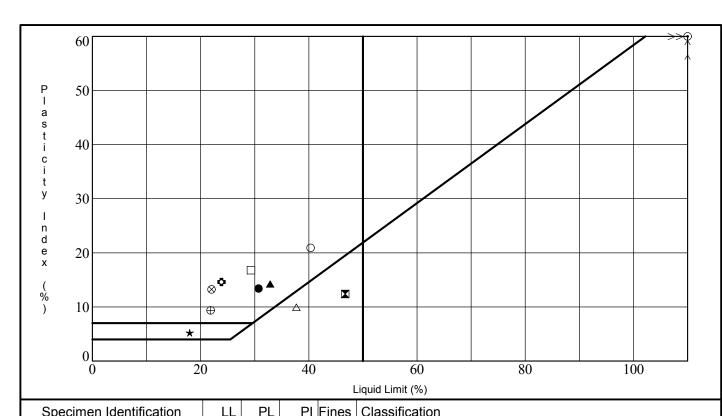
BL-09-00745A





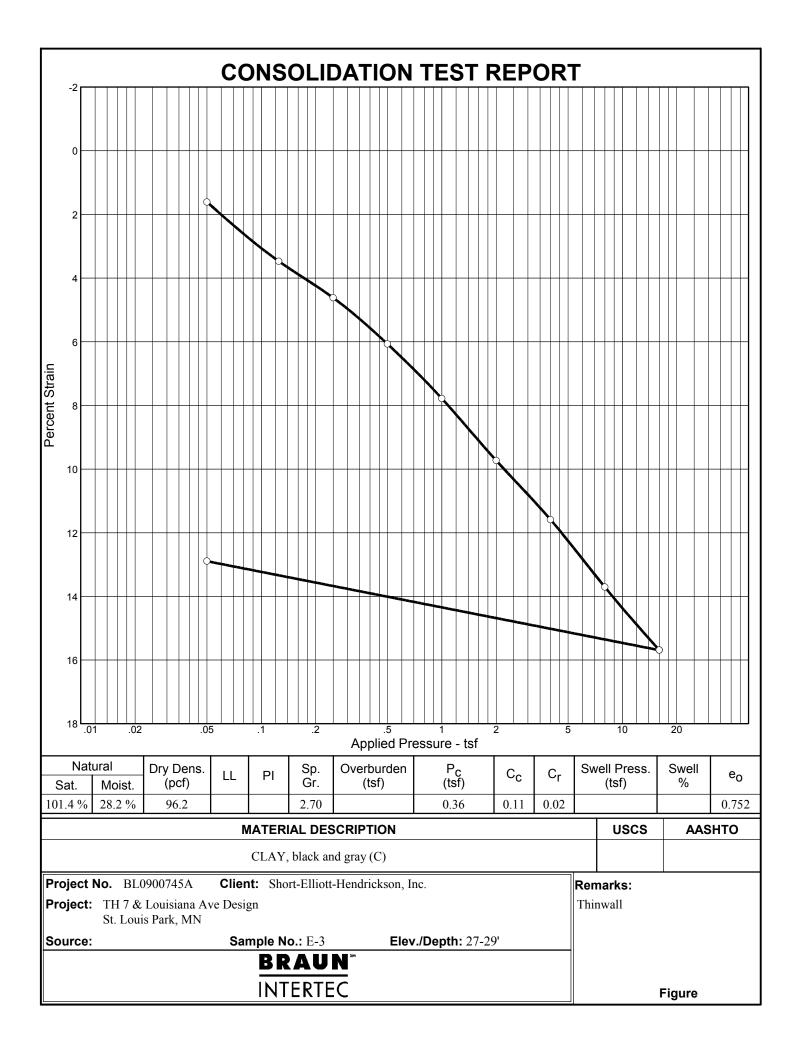






		Specimen Identification	LL	PL	Ы	Fines	Classification	
	•	E-2 10.0'	31	17	14		CLAY	
11:17	X	E-2 22.5'	47	34	13		SILTY CLAY LOAM	
19/11	▲	E-3 25.0'	33	19	14		CLAY	
DT 8/	*	E-3 35.0'	18	13	5		SILTY CLAY	
RENT.G	\odot	E-4 27.5'	264	91	173		PEAT	
_CUR	٥	R-1 55.0'	24	9	15		CLAY	
8N_N0	0	R-4 32.5'	40	19	21		SILTY CLAY LOAM	
J BRA	Δ	R-7 22.5'	38	28	10		SILTY CLAY LOAM	
15A.GP	\otimes	R-8 42.5'	22	9	13		SANDY CLAY LOAM	
9-0074	\oplus	R-9 17.5'	22	12	10		CLAY	
9\BL-0		R-9 45.0'	29	13	16		CLAY	
15\200								
EAPOL								
ΝNΝ								
FILES								
1-GINT								
)LAB								
X-GE								
DJECTS								
VT\PR(
ATTERBERG LIMITS N:\GINT\PROJECTS\X-GEOLAB\1-GINT FILES\MINNEAPOLIS\2009\BL-09-00745A.GPJ BRAUN_V8_CURRENT.GDT 8/19/11 11:17		Braun Project BL-09-00					ATTERBERG LIMITS RESULTS	
.IMITS		SOIL BORINGS AND LABORA		TESTI	NG		BRAUN	
3ERG L		rH 7 & Louisiana Ave Desig rH 7 & Louisiana Avenue	11					
\TTER		St. Louis Park, Minnesota					INTERTEC	
4	RI_00_00745A Rraun Interted						onto a Composition	





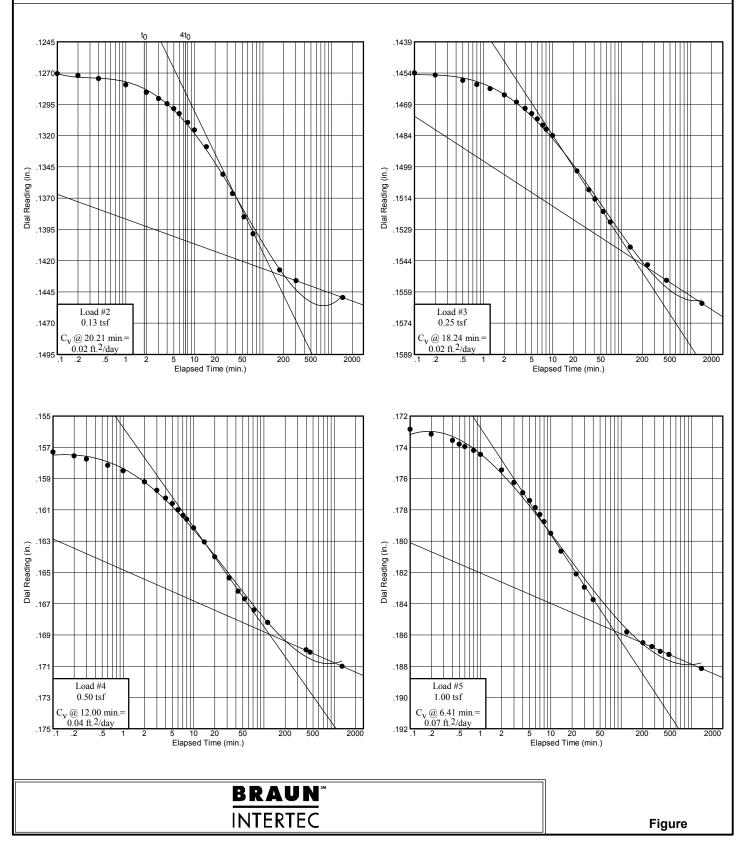
Dial Reading vs. Time

Project No.: BL0900745A

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Source: Sample No.: E-3 Elev./Depth: 27-29'



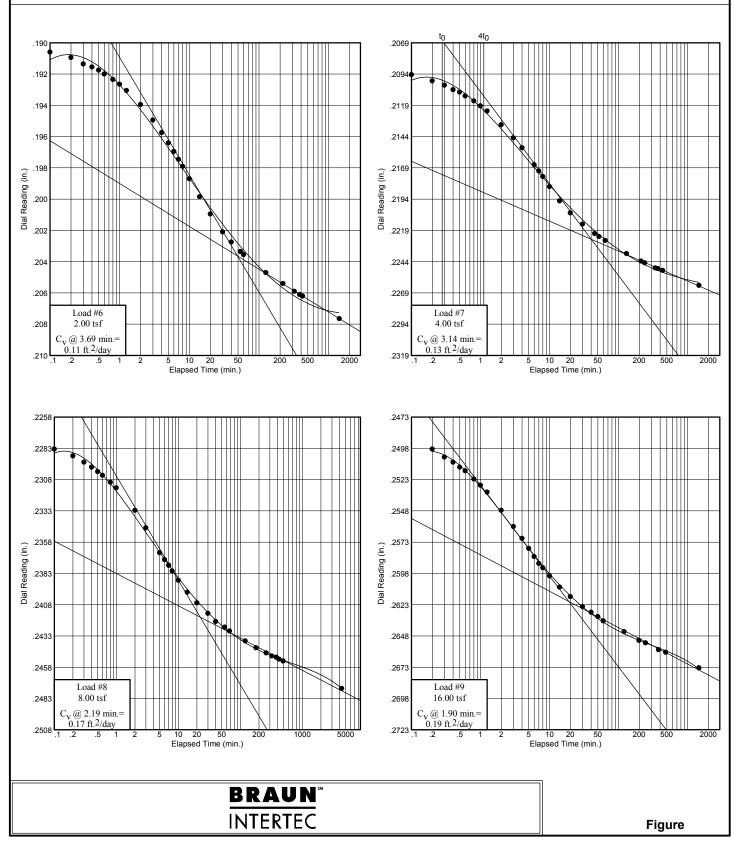
Dial Reading vs. Time

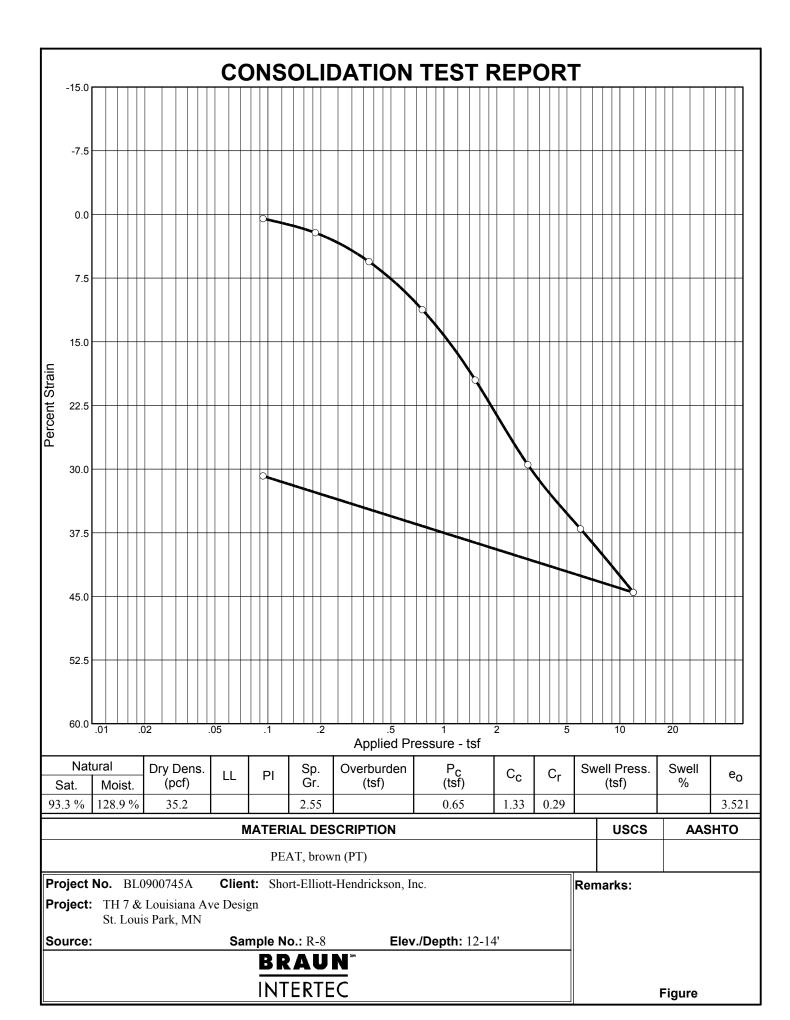
Project No.: BL0900745A

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Source: Sample No.: E-3 Elev./Depth: 27-29'





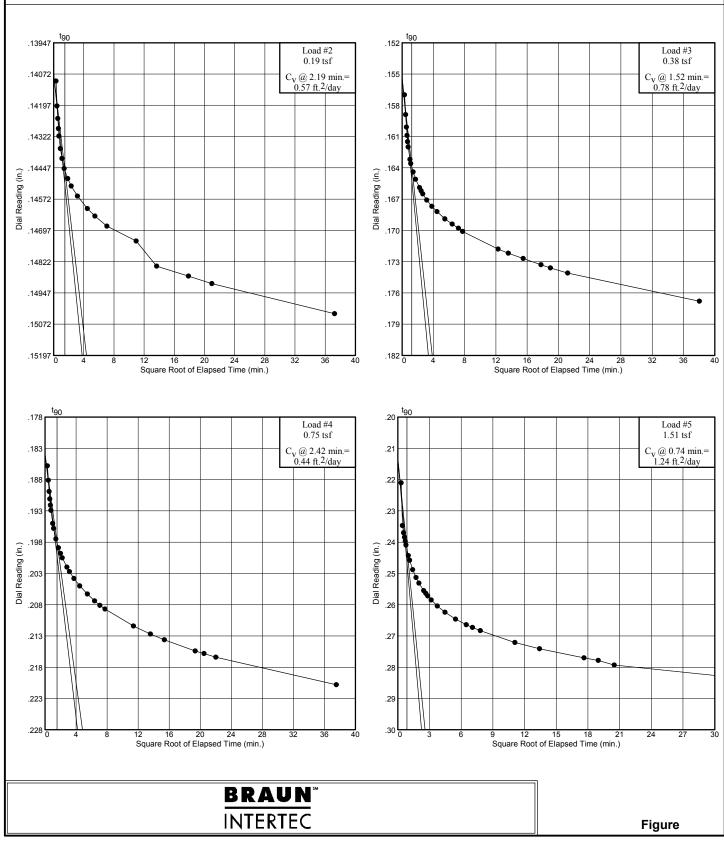


Project No.: BL0900745A

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Source: Sample No.: R-8 Elev./Depth: 12-14'



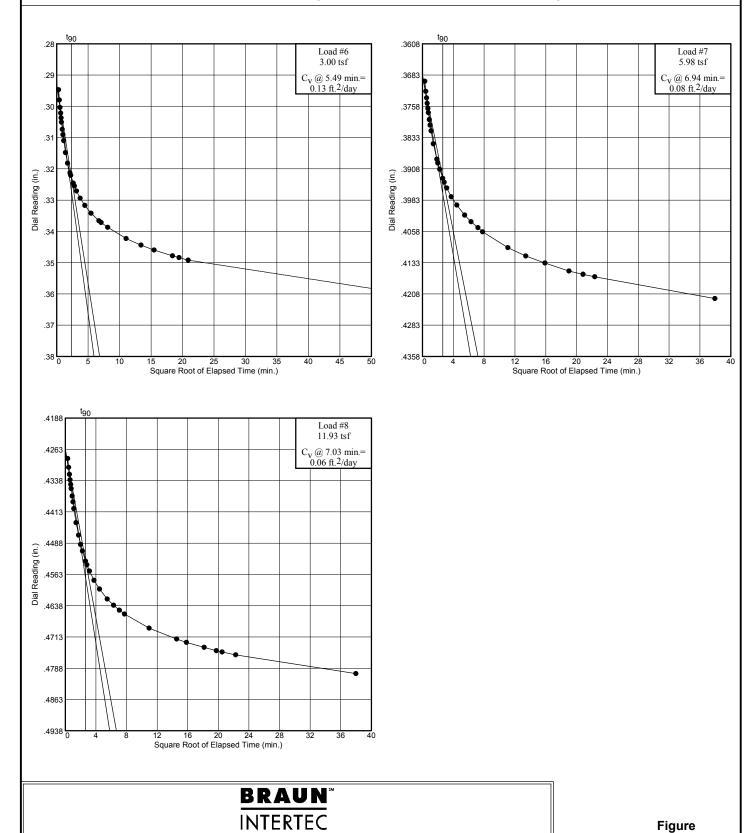
Dial Reading vs. Time

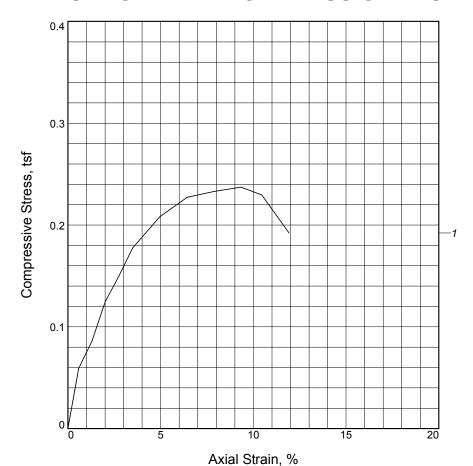
Project No.: BL0900745A

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Source: Sample No.: R-8 Elev./Depth: 12-14'





Sample No.	1				
Unconfined strength, tsf	0.237				
Undrained shear strength, tsf	0.119				
Failure strain, %	9.3				
Strain rate, %/min.	1.00				
Water content, %	16.3				
Wet density, pcf	131.0				
Dry density, pcf	112.6				
Saturation, %	88.6				
Void ratio	0.4966				
Specimen diameter, in.	2.83				
Specimen height, in.	5.58				
Height/diameter ratio	1.97				
Description: CLAY, brown (C)					

Project No.: BL0900745A

Client: Sh

Date Sampled: 5/18/11

PI =

PL =

Remarks:

LL =

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

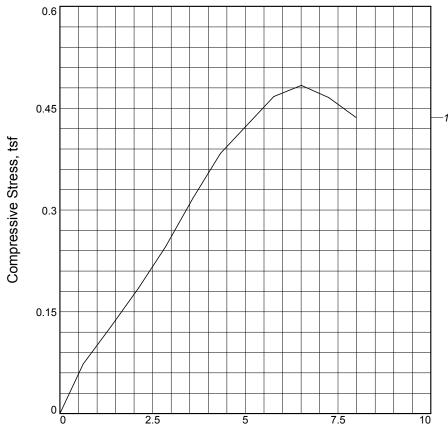
St. Louis Park, MN

GS= 2.70

Sample Number: E-1 Depth: 15'

BRAUN* INTERTEC

Type: Thinwall



Axial Strain, %

Sample No.	1	
Unconfined strength, tsf	0.484	
5 '		
Undrained shear strength, tsf	0.242	
Failure strain, %	6.5	
Strain rate, %/min.	1.00	
Water content, %	47.5	
Wet density, pcf	106.1	
Dry density, pcf	71.9	
Saturation, %	95.5	
Void ratio	1.3433	
Specimen diameter, in.	2.83	
Specimen height, in.	5.57	
Height/diameter ratio	1.97	

Description: SILTY CLAY LOAM, black (SiCL)

LL =	PL =	PI =	GS= 2.70	Type: Thinwall
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Project No.: BL0900745A Date Sampled: 5/18/11

Remarks:

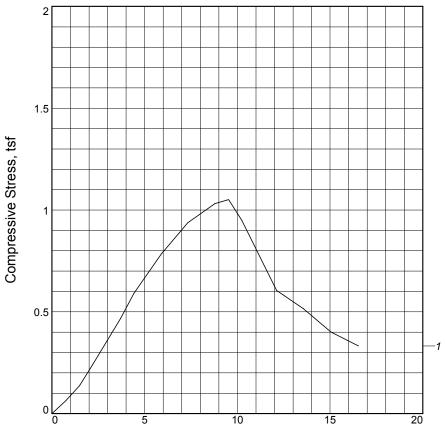
Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: E-2 Depth: 20'

BRAUN*
INTERTEC



Axial Strain, %

Sample No.	1	
Unconfined strength, tsf	1.051	
Undrained shear strength, tsf	0.526	
Failure strain, %	9.5	
Strain rate, %/min.	1.00	
Water content, %	22.7	
Wet density, pcf	129.6	
Dry density, pcf	105.6	
Saturation, %	99.8	
Void ratio	0.6258	
Specimen diameter, in.	2.82	
Specimen height, in.	5.58	
Height/diameter ratio	1.98	

Description: CLAY, brown (C)

	LL =	PL =	PI =	GS= 2.75	Type: Thinwall
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Project No.: BL0900745A Date Sampled: 5/17/11

Remarks:

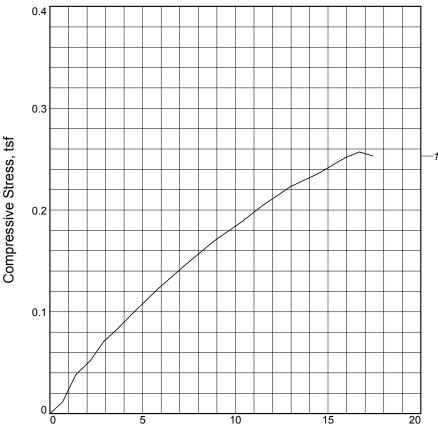
Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: E-3 Depth: 22-24'

BRAUN*
INTERTEC



Axial Strain, %

Sample No.	1	
Unconfined strength, tsf	0.257	
Undrained shear strength, tsf	0.129	
Failure strain, %	16.7	
Strain rate, %/min.	1.00	
Water content, %	26.8	
Wet density, pcf	123.8	
Dry density, pcf	97.7	
Saturation, %	99.6	
Void ratio	0.7255	
Specimen diameter, in.	2.85	
Specimen height, in.	5.51	
Height/diameter ratio	1.94	

Description: CLAY, black and gray (C)

LL =	PL =	PI =	GS= 2.7	Type: Thinwall
				J 1 -

Project No.: BL0900745A

Date Sampled: 5/17/11

Remarks:

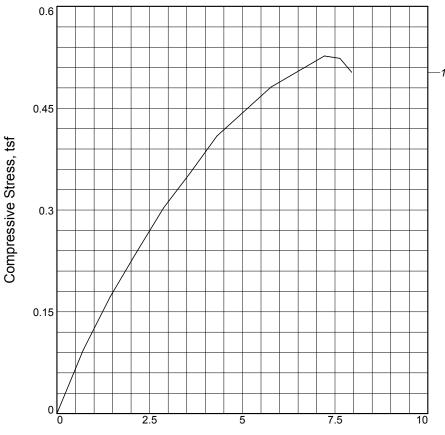
Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: E-3 Depth: 27-29'

BRAUN*
INTERTEC



Axial Strain, %

Sample No.	1	
Unconfined strength, tsf	0.527	
Undrained shear strength, tsf	0.263	
Failure strain, %	7.2	
Strain rate, %/min.	1.00	
Water content, %	225.2	
Wet density, pcf	70.1	
Dry density, pcf	21.6	
Saturation, %	89.2	
Void ratio	6.8189	
Specimen diameter, in.	2.80	
Specimen height, in.	5.60	
Height/diameter ratio	2.00	

Description: PEAT, brown (PT)

LL =	PL =	PI =	GS= 2.70	Type: Thinwall
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Project No.: BL0900745A Date Sampled: 6/3/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

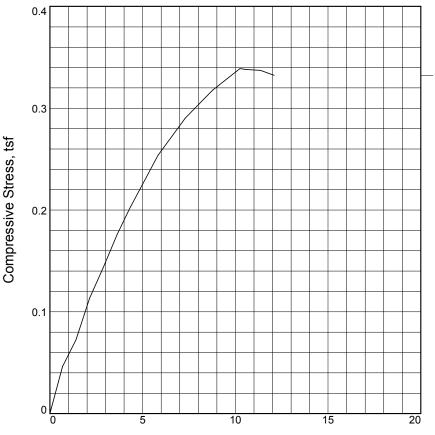
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-2 Depth: 14.5-16.5'

BRAUN*
INTERTEC

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Axial Strain, %

Sample No.	1	
Unconfined strength, tsf	0.339	
Undrained shear strength, tsf	0.169	
Failure strain, %	10.2	
Strain rate, %/min.	1.00	
Water content, %	20.1	
Wet density, pcf	131.3	
Dry density, pcf	109.3	
Saturation, %	100.0	
Void ratio	0.5419	
Specimen diameter, in.	2.83	
Specimen height, in.	5.53	
Height/diameter ratio	1.95	

Description: SILT, brown (ML)

LL = PL =	PI =	GS= 2.70	Type: Thinwall
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Project No.: BL0900745A Date Sampled: 6/3/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

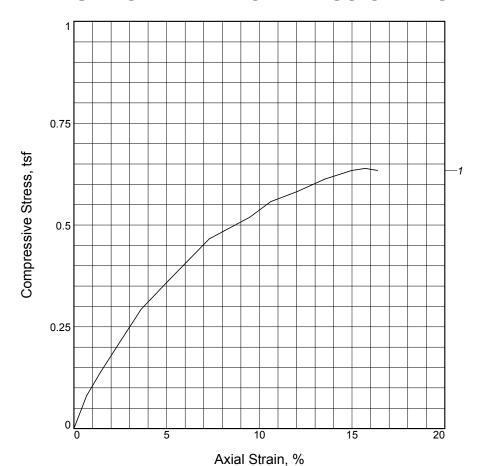
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-2 Depth: 19.5-21.5'

BRAUN**
INTERTEC

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Sample No.	1		
Unconfined strength, tsf	0.639		
Undrained shear strength, tsf	0.319		
Failure strain, %	15.7		
Strain rate, %/min.	1.00		
Water content, %	359.1		
Wet density, pcf	65.3		
Dry density, pcf	14.2		
Saturation, %	89.4		
Void ratio	10.8424		
Specimen diameter, in.	2.83		
Specimen height, in.	5.56		
Height/diameter ratio	1.96		
Description: PEAT, brown (PT)			

Project No.: BL0900745A

Client: Short-Elliott-Hendrickson, Inc.

Date Sampled: 6/8/11

PI =

Remarks:

PL =

LL =

Project: TH 7 & Louisiana Ave Design

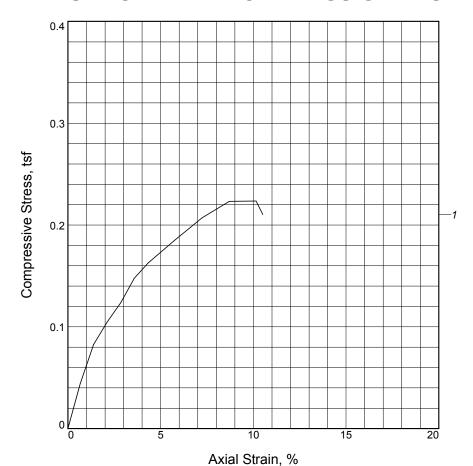
St. Louis Park, MN

GS= 2.70

Sample Number: R-3 Depth: 9.5-11.5'

BRAUN*
INTERTEC

Type: Thinwall



Sample No.	1	
Unconfined strength, tsf	0.224	
Undrained shear strength, tsf	0.112	
Failure strain, %	10.2	
Strain rate, %/min.	1.00	
Water content, %	179.0	
Wet density, pcf	72.3	
Dry density, pcf	25.9	
Saturation, %	87.8	
Void ratio	5.5037	
Specimen diameter, in.	2.78	
Specimen height, in.	5.61	
Height/diameter ratio	2.02	
Description: PEAT, brown (PT)		

Project No.: BL0900745A **Date Sampled:** 6/8/11

PL =

PI =

Remarks:

LL =

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

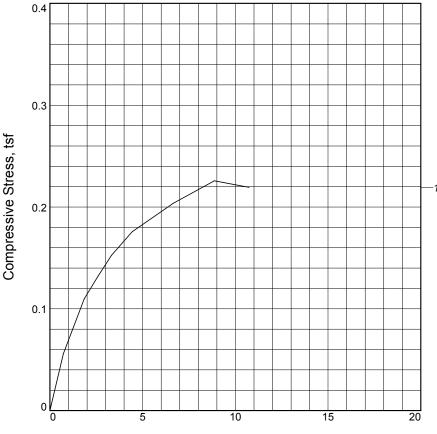
St. Louis Park, MN

GS= 2.70

Sample Number: R-3 Depth: 14.5-16.5'

BRAUN*
INTERTEC

Type: Thinwall



Axial Strain, %

Sample No.	1		
Unconfined strength, tsf	0.226		
Undrained shear strength, tsf	0.113		
Failure strain, %	8.9		
Strain rate, %/min.	1.00		
Water content, %	84.1		
Wet density, pcf	92.2		
Dry density, pcf	50.1		
Saturation, %	95.9		
Void ratio	2.3676		
Specimen diameter, in.	2.80		
Specimen height, in.	5.53		
Height/diameter ratio	1.97		

Description: SILTY CLAY LOAM, gray (SiCL)

LL =	PL =	PI =	GS= 2.70	Type: Thinwall
	• =	• •		- 7 6 6

Project No.: BL0900745A Date Sampled: 6/8/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

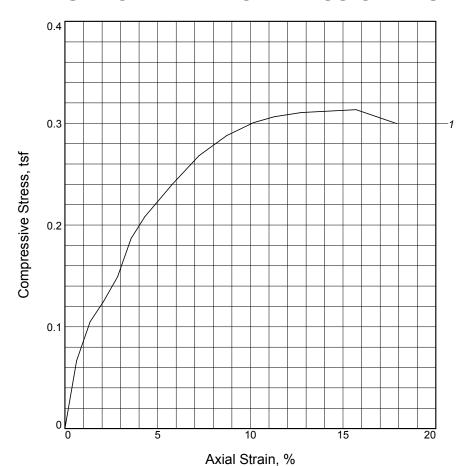
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-3 Depth: 19.5-21.5'

BRAUN*
INTERTEC

Fig	ure	



			_	
Sample No.	1			
Unconfined strength, tsf	0.313			
Undrained shear strength, tsf	0.157			
Failure strain, %	15.7			
Strain rate, %/min.	1.00			
Water content, %	79.0			
Wet density, pcf	93.0			
Dry density, pcf	51.9			
Saturation, %	95.0			
Void ratio	2.2455			
Specimen diameter, in.	2.79			
Specimen height, in.	5.58			
Height/diameter ratio	2.00			
Description: SILTY CLAY LOAM, gray (SiCL)				

Project No.: BL0900745A Client: Short-Elliott-Hendrickson, Inc. Date Sampled: 6/13/11

PI =

PL =

Remarks:

LL =

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

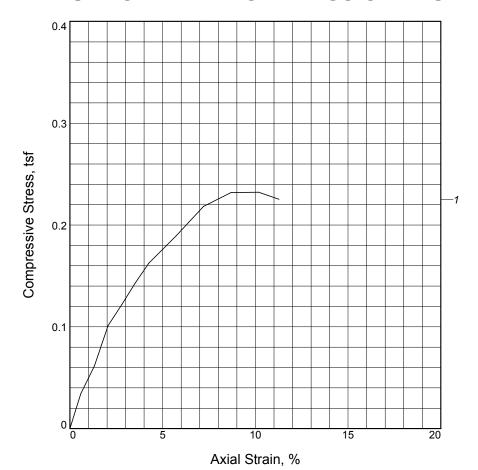
GS= 2.70

Sample Number: R-4 **Depth:** 29.5-31.5'

> **BRAUN**** INTERTEC

Type: Thinwall

Figure _



1				
0.232				
0.116				
10.2				
1.00				
144.1				
81.2				
33.3				
95.7				
4.0682				
2.84				
5.53				
1.95				
Description: CLAY, gray (C)				
	0.116 10.2 1.00 144.1 81.2 33.3 95.7 4.0682 2.84 5.53	0.116 10.2 1.00 144.1 81.2 33.3 95.7 4.0682 2.84 5.53	0.116 10.2 1.00 144.1 81.2 33.3 95.7 4.0682 2.84 5.53	

Project No.: BL0900745A

Client: S

Date Sampled: 6/13/11

PI =

PL =

Remarks:

LL =

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

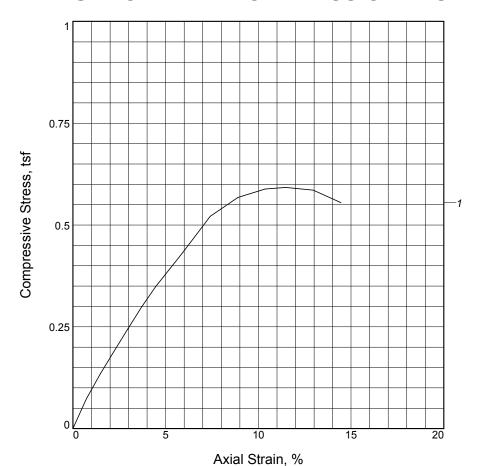
St. Louis Park, MN

GS= 2.70

Sample Number: R-6 Depth: 19.5-21.5'

BRAUN*
INTERTEC

Type: Thinwall



1			
0.592			
0.296			
11.5			
1.00			
22.2			
130.3			
106.7			
100.0			
0.6096			
2.82			
5.55			
1.97			
	0.296 11.5 1.00 22.2 130.3 106.7 100.0 0.6096 2.82 5.55	0.296 11.5 1.00 22.2 130.3 106.7 100.0 0.6096 2.82 5.55	0.296 11.5 1.00 22.2 130.3 106.7 100.0 0.6096 2.82 5.55

Description: CLAY, gray (C)

LL =	PL =	PI =	GS= 2.75	Type: Thinwall
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Project No.: BL0900745A Date Sampled: 6/13/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

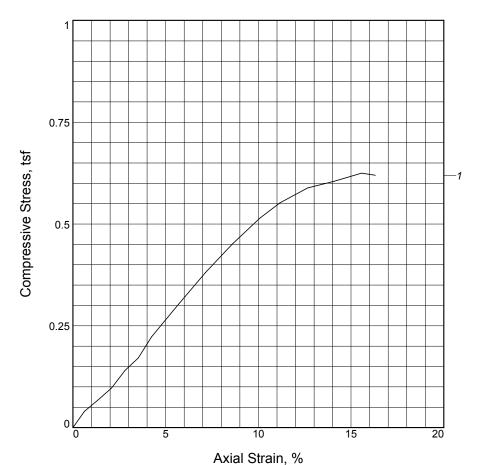
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-6 Depth: 24.5-26.5'

BRAUN*
INTERTEC

F	ig	ure	-



Sample No.	1		
Unconfined strength, tsf	0.625		
Undrained shear strength, tsf	0.312		
Failure strain, %	15.6		
Strain rate, %/min.	1.00		
Water content, %	24.7		
Wet density, pcf	124.0		
Dry density, pcf	99.5		
Saturation, %	96.0		
Void ratio	0.6948		
Specimen diameter, in.	2.83		
Specimen height, in.	5.62		
Height/diameter ratio	1.98		

Description: SILTY CLAY LOAM, brown (SiCL)

LL =	PL =	PI =	GS= 2.7	Type: Thinwall
				J 1 -

Project No.: BL0900745A Date Sampled: 5/10/11

Remarks:

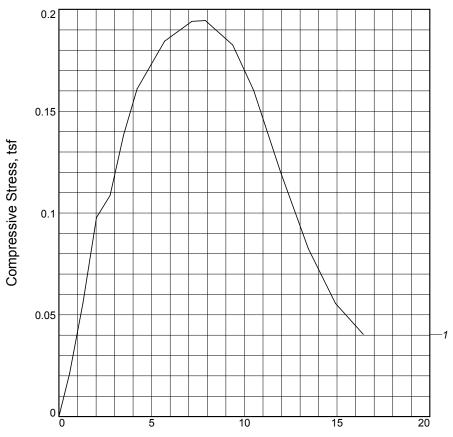
Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-7 Depth: 19-21'

BRAUN*
INTERTEC



Axial Strain, %

Sample No.	1	
Unconfined strength, tsf	0.195	
Undrained shear strength, tsf	0.097	
Failure strain, %	7.9	
Strain rate, %/min.	1.00	
Water content, %	36.3	
Wet density, pcf	113.6	
Dry density, pcf	83.4	
Saturation, %	95.8	
Void ratio	1.0213	
Specimen diameter, in.	2.83	
Specimen height, in.	5.56	
Height/diameter ratio	1.97	

Description: SILTY CLAY LOAM, gray (SiCL)

LL = PL = PI = GS = 2.70 Type: Thinwall
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Project No.: BL0900745A Date Sampled: 5/10/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

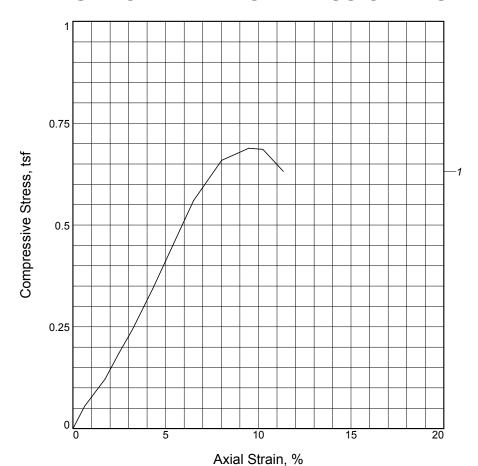
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-7 Depth: 24-26'

BRAUN*
INTERTEC

Fig	ure	



Sample No.	1
Unconfined strength, tsf	0.688

Undrained shear strength, tsf 0.344 Failure strain, % 9.5 Strain rate, %/min. 1.00 Water content, % 27.0 Wet density, pcf 124.9 Dry density, pcf 98.4 Saturation, % 99.6 Void ratio 0.7447 Specimen diameter, in. 2.82 Specimen height, in. 5.52

Description: SILTY CLAY LOAM, brown (SiCL)

	,	, ()		
LL =	PL =	PI =	GS= 2.75	Type: Thinwall

Project No.: BL0900745A **Date Sampled:** 6/9/11

Height/diameter ratio

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

1.96

Project: TH 7 & Louisiana Ave Design

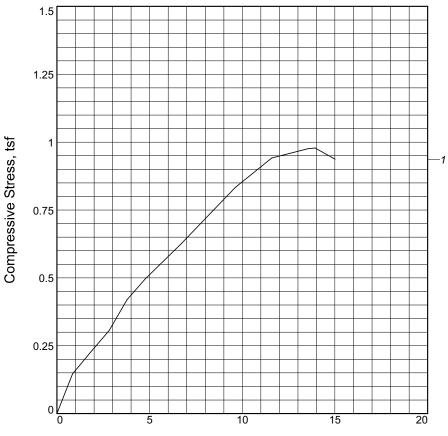
St. Louis Park, MN

Sample Number: R-8 Depth: 22-24'

BRAUN*
INTERTEC

Figure $_$	
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UNCONSOLIDATED UNDRAINED TEST



Axial Strain, %

1		
0.979		
0.937		
1.100		
1.00		
52.9		
103.5		
67.7		
95.9		
1.4899		
1.42		
2.80		
1.98		
	0.937 1.100 1.00 52.9 103.5 67.7 95.9 1.4899 1.42 2.80	0.937 1.100 1.00 52.9 103.5 67.7 95.9 1.4899 1.42 2.80

Description: SILTY CLAY LOAM, black (SiCL)

LL = PL = PI = GS = 2.70 Type: Thinwall

Project No.: BL0900745A

Date Sampled: 5/18/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

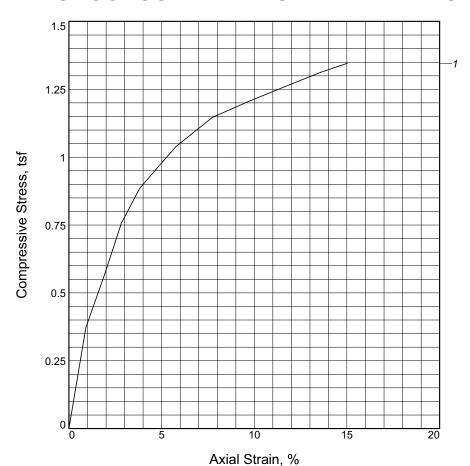
St. Louis Park, MN

Sample Number: E-2 Depth: 20'

BRAUN*
INTERTEC

Figure UU Triax ASTM D 2850

UNCONSOLIDATED UNDRAINED TEST



Sample No.	1		
Peak Stress, tsf	1.346		
Ult. Stress, tsf	1.346		
Cell pressure, tsf	1.500		
Strain rate, %/min.	1.00		
Water content, %	25.2		
Wet density, pcf	126.6		
Dry density, pcf	101.1		
Saturation, %	99.4		
Void ratio	0.6988		
Specimen diameter, in.	1.41		
Specimen height, in.	2.80		
Height/diameter ratio	1.99		

Description: CLAY, black and gray (C)

LL = PL = PI = GS = 2.75 Type: Thinwall

Project No.: BL0900745A

Date Sampled: 5/17/11

Date Sampled. 3/1//11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

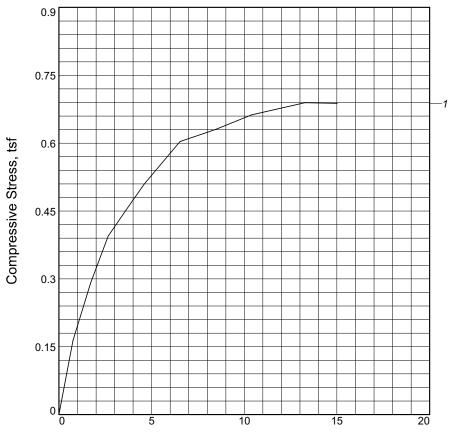
St. Louis Park, MN

Sample Number: E-3 Depth: 22-24'

BRAUN*
INTERTEC

Figure UU Triax ASTM D 2850

UNCONSOLIDATED UNDRAINED TEST



Axial	Strain,	%
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Sample No.	1		
Peak Stress, tsf	0.689		
Ult. Stress, tsf	0.688		
Cell pressure, tsf	0.650		
Strain rate, %/min.	1.00		
Water content, %	47.2		
Wet density, pcf	100.8		
Dry density, pcf	68.5		
Saturation, %	87.1		
Void ratio	1.4610		
Specimen diameter, in.	1.40	 	
Specimen height, in.	2.81		
Height/diameter ratio	2.00		

Description: PEAT, brown (PT)

Type: Thinwall LL = PL = PI = **GS=** 2.70

Project No.: BL0900745A Date Sampled: 6/3/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

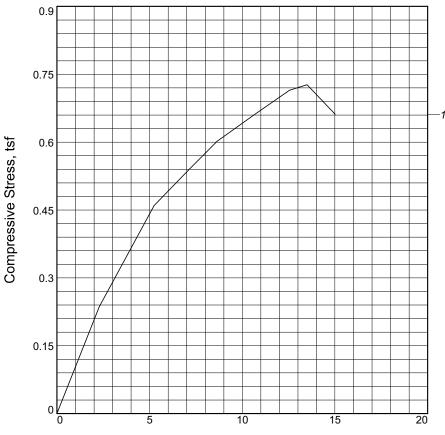
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-2 **Depth:** 9.5-11.5'

> **BRAUN**^{ss} INTERTEC

Figure UU Triax ASTM D 2850



Axial Strain, %

Sample No.	1	
Peak Stress, tsf	0.727	
Ult. Stress, tsf	0.661	
Cell pressure, tsf	0.400	
Strain rate, %/min.	1.00	
Water content, %	393.0	
Wet density, pcf	66.7	
Dry density, pcf	13.5	
Saturation, %	92.6	
Void ratio	11.4593	
Specimen diameter, in.	1.41	
Specimen height, in.	2.79	
Height/diameter ratio	1.98	·

Description: PEAT, brown (PT)

LL = PL = PI = GS = 2.70 Type: Thinwall

Project No.: BL0900745A

Date Sampled: 6/8/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

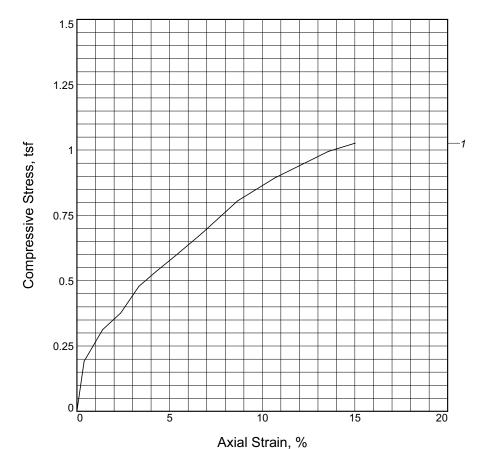
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-3 Depth: 9.5-11.5'

BRAUN*
INTERTEC

Figure UU Triax ASTMD 2850



Sample No.	1	
Peak Stress, tsf	1.026	
Ult. Stress, tsf	1.026	
Cell pressure, tsf	1.250	
Strain rate, %/min.	1.00	
Water content, %	59.0	
Wet density, pcf	103.2	
Dry density, pcf	64.9	
Saturation, %	99.8	
Void ratio	1.5953	
Specimen diameter, in.	1.38	
Specimen height, in.	2.80	
Height/diameter ratio	2.02	

Description: SILTY CLAY LOAM, gray (SiCL)

LL =	PL =	PI =	GS= 2.70	Type: Thinwall
------	------	------	-----------------	----------------

Project No.: BL0900745A Date Sampled: 6/13/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

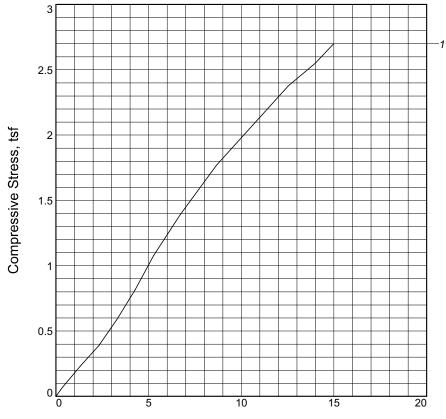
St. Louis Park, MN

Sample Number: R-4 Depth: 29.5-31.5'

BRAUN*
INTERTEC

Figure UU Triax ASTM D 2850

Tested By: jk Checked By: jrs



Axial Strain, %

Sample No.	1		
Peak Stress, tsf	2.700		·
Ult. Stress, tsf	2.700		
Cell pressure, tsf	1.000		
Strain rate, %/min.	1.00		
Water content, %	18.7		
Wet density, pcf	135.2		
Dry density, pcf	113.9		
Saturation, %	99.4		
Void ratio	0.5237		
Specimen diameter, in.	1.39		
Specimen height, in.	2.80		
Height/diameter ratio	2.02		
	·	·	

Description: SILTY CLAY LOAM, gray (SiCL)

LL =	PL =	PI =	GS= 2.78	Type: Thinwall
------	------	------	-----------------	----------------

Project No.: BL0900745A **Date Sampled:** 5/10/11

2 at 3 ampioa. 27 107 11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

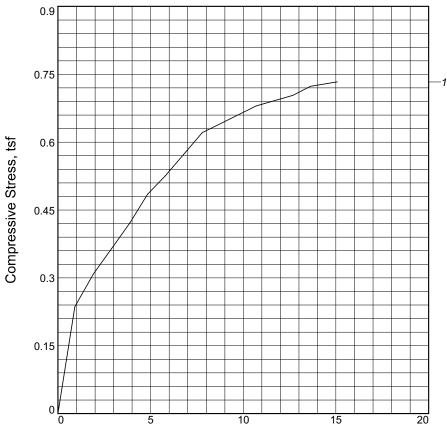
St. Louis Park, MN

Sample Number: R-7 Depth: 19-21'

BRAUN**
INTERTEC

Figure UU Triax ASTM D 2850

Tested By: jk Checked By: jrs



Axial Strain, %

Sample No.	1	
Peak Stress, tsf	0.733	
Ult. Stress, tsf	0.733	
Cell pressure, tsf	1.000	
Strain rate, %/min.	1.00	
Water content, %	31.5	
Wet density, pcf	118.3	
Dry density, pcf	89.9	
Saturation, %	97.4	
Void ratio	0.8744	
Specimen diameter, in.	1.39	
Specimen height, in.	2.81	
Height/diameter ratio	2.03	

Description: SILTY CLAY LOAM, gray (SiCL)

LL = PL = PI = GS = 2.7 Type: Thinwall

Project No.: BL0900745A

Date Sampled: 5/10/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

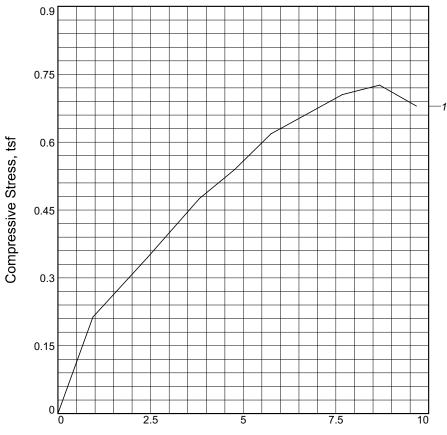
Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-7 Depth: 24-26'

BRAUN**
INTERTEC

Figure UU Triax ASTMD 2850



Axial Strain, %

Sample No.	1	
Peak Stress, tsf	0.726	
Ult. Stress, tsf	0.680	
Cell pressure, tsf	1.000	
Strain rate, %/min.	1.00	
Water content, %	264.4	
Wet density, pcf	65.4	
Dry density, pcf	18.0	
Saturation, %	85.1	
Void ratio	8.3870	
Specimen diameter, in.	1.40	
Specimen height, in.	2.78	
Height/diameter ratio	1.98	

Description: PEAT, brown (PT)

LL = PL = PI = GS = 2.70 Type: Thinwall

Project No.: BL0900745A

Date Sampled: 5/25/11

Date Sampled. 3/23/11

Remarks:

Client: Short-Elliott-Hendrickson, Inc.

Project: TH 7 & Louisiana Ave Design

St. Louis Park, MN

Sample Number: R-9 Depth: 14.5-16.5'

BRAUN**
INTERTEC

Figure UU Triax ASTM D 2850



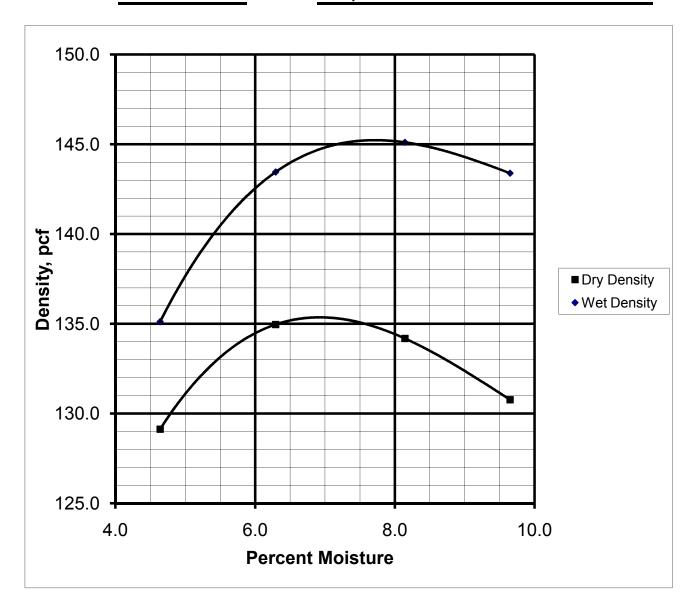
Client: Shot-Elliott-Hendrickson, Incorporated Project No.: BL-09-00745A

Location: TH 7 & Louisiana Ave St. Louis Park, MN

Moisture-Density Relationship

 SP No:
 Date:
 7/8/2011
 Tester:
 13733

 Curve No:
 P-01
 Soil Class:
 Loamy Sand



Optimum Moisture: 6.9 % Maximum Density: 135.4 pcf
Sample Location: Boring B-13, Boring B-13, 1-3ft



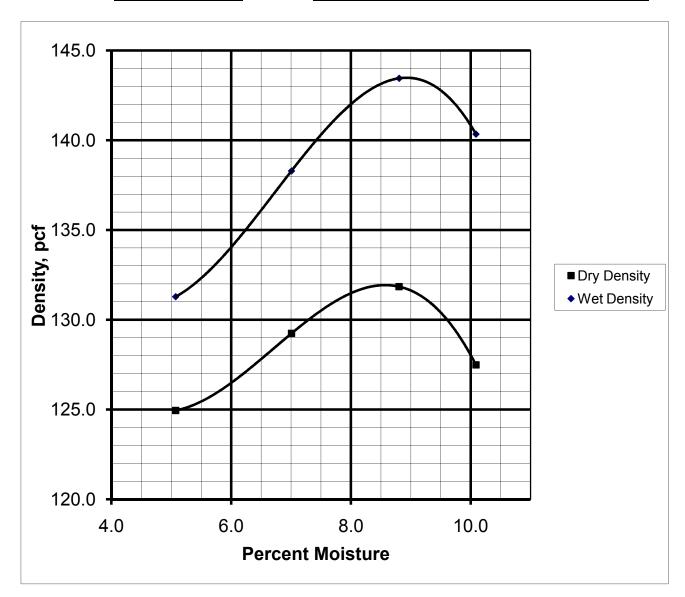
Client: Shot-Elliott-Hendrickson, Incorporate Project No.: BL-09-00745A

Location: TH 7 & Louisiana Ave St. Louis Park, MN

Moisture-Density Relationship

 SP No:
 Date:
 7/8/2011
 Tester:
 13733

 Curve No:
 P-02
 Soil Class:
 Sandy Loam



Optimum Moisture: 8.6 % Maximum Density: 131.9 pcf
Sample Location: Boring B-3, Boring B-3, 1-5ft



Minneapolis Laboratory **Braun Intertec Corporation**

Phone: 952-995-2000

Material Test Report

Client: **Brent Theroux**

Short-Elliott-Hendrickson, Incorporated

3535 Vadnais Center Dr

Saint Paul, MN, 55110-5196

Project: BL-09-00745A

TH 7 & Louisiana Ave Design TH 7 & Louisiana Avenue St. Louis Park, MN, 55426

PM: Josh J VanAbel, jvanabel@BraunIntertec.com Report No: MAT:W11-001210-S2

Alla O.M.

Issue No: 1

Dallas Miner Laboratory Supervisor

Date of Issue: 7/13/2011

Sample Details

Sample ID: W11-001210-S2

Alternate Sample ID:

Sampled By: Scott Mclean Sampling Method: Soil Boring Auger

Date Sampled: 5/18/2011 Date Submitted: 7/7/2011

Specification:

Source: Boring B-3, 1-5 ft Material Type: Sandy Loam Sample Location: Boring B-3

Test Results

Description	Method	Result Lir	mits
R Value	MnDOT 1307 - 95	28	
Date Tested		7/12/2011	
Certification #s		15600	
Date Tested		7/12/2011	

Comments



Minneapolis Laboratory **Braun Intertec Corporation**

Phone: 952-995-2000

Material Test Report

Client: **Brent Theroux**

Short-Elliott-Hendrickson, Incorporated

3535 Vadnais Center Dr

Saint Paul, MN, 55110-5196

Project: BL-09-00745A

TH 7 & Louisiana Ave Design TH 7 & Louisiana Avenue St. Louis Park, MN, 55426

PM: Josh J VanAbel, jvanabel@BraunIntertec.com Report No: MAT:W11-001210-S1

Alla O.M.

Issue No: 1

Dallas Miner Laboratory Supervisor

Date of Issue: 7/13/2011

Sample Details

Sample ID: W11-001210-S1

Alternate Sample ID: P-01

Sampled By: Scott Mclean Sampling Method: Soil Boring Auger Date Sampled: 5/20/2011

Date Submitted: 7/7/2011

Specification:

Source: Boring B-13, 1-3 ft Material Type: Sandy Loam Sample Location: Boring B-13

Test Results

Description	Method	Result	Limits
R Value	MnDOT 1307 - 95	71	
Date Tested		7/12/2011	
Certification #s		15600	
Date Tested		7/12/2011	

Comments



Minnesota Department of Transportation Geotechnical Section

Boring Log Descriptive Terminology (English Units)



USER NOTES, ABBREVIATIONS AND DEFINITIONS - Additional information available in Geotechnical Manual.

This boring was made by ordinary and conventional methods and with care deemed adequate for the Department's design purposes. Since this boring was not taken to gather information relating to the construction of the project, the data noted in the field and recorded may not necessarily be the same as that which a contractor would desire. While the Department believes that the information as to the conditions and materials reported is accurate, it does not warrant that the information is necessarily complete. This information has been edited or abridged and may not reveal all the information which might be useful or of interest to the contractor. Consequently, the Department will make available at its offices, the field logs relating to this boring.

Since subsurface conditions outside each borehole are unknown, and soil, rock and water conditions cannot be relied upon to be consistent or uniform, no warrant is made that conditions adjacent to this boring will necessarily be the same as or similar to those shown on this log. Furthermore, the Department will not be responsible for any interpretations, assumptions, projections or interpolations made by contractors, or other users of this log.

Water levels recorded on this log should be used with discretion since the use of drilling fluids in borings may seriously distort the true field conditions. Also, water levels in cohesive soils often take extended periods of time to reach equilibrium and thus reflect their true field level. Water levels can be expected to vary both seasonally and yearly. The absence of notations on this log regarding water does not necessarily mean that this boring was dry or that the contractor will not encounter subsurface water during the course of construction.

WATER MEASUREMENT

AB	After Bailing
AC	After Completion
AF	After Flushing
w/C	with Casing
w/M	with Mud
WSD	While Sampling/Drilling

w/AUGwith Hollow Stem Auger

MISCELLANEOUS

MICCELLAILE	000
NA	Not Applicable
w/	with
w/o	with out
sat	saturated

DRILLING OPERATIONS

DRILLI	NG OPERATIONS
AUG	Augered
CD	Core Drilled
DBD	Disturbed by Drilling
DBJ	Disturbed by Jetting
PD	Plug Drilled
ST Index Sh	

TW	Thinwall (Shelby Tube)
WS	Wash Sample
NSR	No Sample Retrieved
WH	Weight of Hammer
WR	Weight of Rod
Mud	Drilling Fluids in Sample
CS	Continuous Sample

SOIL/CORE TESTS

SPT N₆₀.......ASTM D1586 Modified Blows per foot with 140 lb. hammer and a standard energy of 210 ft-lbs. This energy represents 60% of the potential energy of the system and is the average energy provided by a Rope & Cathead system.

MC	.Moisture Content
COH	.Cohesion
?	.Sample Density
LL	Liquid Limit
PI	.Plasticity Index
F	.Phi Angle
	.Percent Core Recovered
RQD	.Rock Quality Description
(Percent of total	core interval consisting of
unbroken pieces	4 inches or longer)
ACL	Average Core Length
(Average length	of core that is greater than 4
inches Iona)	· ·

Core BreaksNumber of natural core breaks per 2-foot interval.

DISCONTINUITY SPACING

Fractures	Distance	Bedding
Very Close	<2 inches	Very Thin
Close	2-12 inches	Thin
Mod. Close	12-36 inches	Medium
Wide	>36 inches	Thick

Vane Shear Test

PRILLING SYMBOLS
Washed Sample
(Collected during plug drilling)

Augered

Plug Drilled

Split Tube Sample (SPT N₅₀ 2 in. spilt tube with liners)

Thin Wall Sample (3 in. Shelby Tube)

Core Drilled (NV Core Barrel unless otherwise noted)

Continuous Soil
Sample
Augered & Jetted

et Jetted

VP Augered & Plug Drilled

RELATIVE DENSITY

Compactness - Granular Solls	BPF
very loose	0-4
loose	5-10
medium dense	11-24
dense	25-50
very dense	>50

Consistency - Cohesive Soils	<u>BPF</u>
very soft	0-1
soft	2-4
firm	5-8
stiff	9-15
very stiff	16-30
hard	31-60
very hard	> 60

COLOR

blk	Black	wht	White
grn	Green	brn	Brown
orng	Orange	yel	Yellov
dk	Dark	lt	Light
IOS	Iron Oxid	e Stained	_

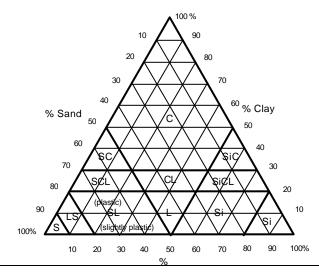
GRAIN SIZE /PLASTICITY

VF	Very Fine	pl Plastic
F	Fine	slplSlightly
Cr	Coarse	Plastic

SOIL/ROCK TERMS

SOIL/ROC	K IEKIVIS		
C	Clay	Lmst	.Limestone
L	Loam	Sst	.Sandstone
S	Sand	Dolo	.Dolostone
Si	Silt	w x	.weathered
G	Gravel (No. 10	Sieve to 3	inches)
Bldr	Boulder (over 3	3 inches)	
T	till (unsorted, i	nonstratifie	ed glacial
deposits)			

Mn/DOT Triangular Textural Soil Classification System



Ap	p	er	d	İΧ	C

SEH Phase II Investigation (Submitted under Separate Cover)

Appendix D

Braun Soil Boring Report, 2009

Results of Soil Borings and Laboratory Testing

Soil Borings and Laboratory Testing Preliminary Design - State Highway 7 and Louisiana Avenue Intersection Reconstruction St. Louis Park, Minnesota

Prepared for

Short Elliott Hendrickson, Inc.

Project BL-09-00745 July 16, 2009

Braun Intertec Corporation





Braun Intertec Corporation 11001 Hampshire Avenue S Minneopolis, MN 55438

Phone: 932,995,2000 Fax: 952 995,2020 - Web: - brounintered com

July 16, 2009

Project BL-09-00745

AJ Schwidder, PE Short Elliott Hendrickson, Inc. 3535 Vadnais Center Drive St. Paul, MN 55110

Re:

Soil Borings and Laboratory Testing

Preliminary Design - State Highway 7 and Louisiana Avenue

Intersection Reconstruction St. Louis Park, Minnesota

Dear Mr. Schwidder:

We have completed the soil borings and laboratory testing requested by Short Elliott Hendrickson, Inc. (SEH) for the preliminary design of the Intersection State Highway 7 and Louisiana Avenue in St. Louis Park, Minnesota.

Scope of Services

Our work was completed in general accordance with our authorized Proposal for Soil Borings and Laboratory Testing, dated February 26, 2009.

For the project, our scope of services included performing a total of 12 standard penetration test soil borings to nominal depths of 20 to 30 feet below grade (one boring was extended to 35 feet due to poor soil conditions). Our services also included clearance of public utilities, traffic control, acquiring MnDOT right of way permits, laboratory testing as requested by SEH and preparation of a factual soil boring report.

Documents Provided

SEH provided us with a Preliminary Boring Plan for TH 7 – Louisiana Ave, which included the requested boring locations. The plan was prepared by SEH and was dated January 29, 2009.

Boring Locations and Elevations

We performed a total of 12 standard penetration test soil borings for the project. The soil borings were denoted as ST-1 to ST-12 and were performed at the approximate locations shown on the attached Soil Boring Location Sketch. SEH provided us with the surveyed boring coordinates, which were used to create a Soil Boring Location Sketch utilizing an aerial map from Google Earth®.

The boring locations were selected and staked by SEH. Ground surface elevations at the boring locations were also provided by SEH.

Short Elliott Hendrickson, Inc. Project BL-09-00745 July 16, 2009 Page 2

Drilling and Sampling

The penetration test borings were drilled with a truck-mounted core and auger drill equipped with hollow-stem auger. The borings were performed in accordance with ASTM D 1586. Penetration test samples were taken at 2 1/2 and 5-foot intervals. Actual sample intervals and corresponding depths are shown on the boring logs. Additional thinwall samples (TW) were taken in zones of organic soils.

Log of Boring Sheets

Log of Boring sheets for our penetration test borings are attached to this report. The logs identify and describe the geologic materials that were penetrated, present the results of penetration resistance tests, laboratory tests performed on penetration test samples retrieved from them, and groundwater measurements.

Strata boundaries were inferred from changes in the penetration test samples and the auger cuttings. Because sampling was not performed continuously, the strata boundary depths are only approximate. The boundary depths likely vary away from the boring locations, and the boundaries themselves may also occur as gradual rather than abrupt transitions.

Soil Classification

The geologic materials encountered were visually and manually classified in accordance with ASTM Test Method D 2488. A chart explaining the classification system is attached. Samples were sealed in jars or bags and returned to our facility for review by a geotechnical engineer and storage.

Laboratory Testing

We performed moisture content, dry density and Atterberg limits tests on jar and thinwall samples recovered from the soil borings in accordance with ASTM methods. The test results are shown or noted on the right side of the Log of Boring Sheets, across from the associated sample. The Atterberg limits test results are also shown on separate sheets attached to this report.

Groundwater Observations

The drillers checked for groundwater as the borings were advanced, and again after auger withdrawal. The boreholes were then backfilled with bentonite grout.

Groundwater Fluctuations

Groundwater measurements were made under the conditions reported herein and shown on the exploration logs, and interpreted in the text of this report. It should be noted that the observation period was relatively short, and groundwater can be expected to fluctuate in response to rainfall, flooding, irrigation, seasonal freezing and thawing, surface drainage modifications and other seasonal and annual factors.



Short Elliott Hendrickson, Inc. Project BL-09-00745 July 16, 2009 Page 3

Level of Care

In performing our services, Braun Intertec has used that degree of care and skill ordinarily exercised under similar circumstances by reputable members of our profession currently practicing in the same locality. No warranty, express or implied, is made.

General

Please refer to the attached report for a detailed summary of our procedures and results. We appreciate the opportunity to be of service to you on this project. If you have any questions regarding this report, please contact Josh Van Abel at 952.995.2310 or Matt Ruble at 952.995.2224.

Sincerely,

BRAUN INTERTEC CORPORATION

Joshua J. Van Abel, PE Project Engineer

7 Val

Matthew P. Ruble, PE Principal Engineer

Attachments:

Soil Boring Location Sketch Log of Boring Sheets ST-1 to ST-12 Atterberg Limits Results (1 Sheet) Descriptive Terminology of Soil

Rpt Hwy 7 and Louisiana Avenue





11001 Hampshire Avenue So. Minneapolis, MN 55438 PH. (952) 995-2000 FAX (952) 995-2020

Base Dwg Provided By:

Google.

PRELIMINARY DESIGN TRUNK HIGHWAY 7 AND LOUISIANA A SAINT LOUIS PARK, MINNESOTA

Project No: BL0900745

Drawing No: BL0900745

Scale:	1" = 150'
Drawn By:	BJB
Date Drawn:	5/27/09
Checked By:	JJV
Last Modified:	5/18/09

Sheet: Fig:



Braun P					BORING			ST-1
	ry D on R	esign-S leconst	tate ruct		LOCATIO	DN: Se	e att	ached sketch.
DRILLER:	М.	Takada		METHOD: 3 1/4" HSA, Autohammer	DATE:	3/20	6/09	SCALE: 1" = 4'
	epth eet 0.0	ASTM Symbo	1	Description of Materials (ASTM D2488 or D2487)		BPF	WL	Tests or Notes
feet 889.1 888.1	et	FILL FILL PT		·	with —	BPF 10 10 2 2 WH* 1 3	₩L	Benchmark: Ground surface elevations provided by SEH, Inc. Note: Possible chemical odd detected in most soil sample below 5 to 7 feet at all boring locations. An open triangle in the water level (WL) column indicates the depth at which groundwater was observed while drilling. Groundwater levels fluctuate. *Weight of hammer. *Weight of hammer. *Weight of hollow-stem auger in the ground. Water observed at 15 feet with 24 1/2 feet of hollow-stem auger in the ground. Water not observed to
-				END OF BORING.*	- - -			cave-in depth of 12 feet immediately after withdrawa of auger. Boring immediately backfills with bentonite grout.
BL-09-00745	, adajupajo comzecca			Braun Intertec Corporation				ST-1 page



	ect BL-0					BORING:			ST-2		
SOIL BORING Preliminary D Intersection I St. Louis Park	esign-Sta Reconstru	ite Higi iction		NG ouisiana Avenue		LOCATIO	N: Se	N: See attached sketch.			
DRILLER: C.	Powers		METHOD:	3 1/4" HSA, Autohamm	er	DATE:	3/27	7/09	SCALE: 1" = 4'		
Elev. Depth feet feet 891.1 0.0	t ASTM Description of Materials						BPF	WL	Tests or Notes		
- 889.1 2.0 	FILL	of Gramoist FILL: Organ	avel, non- to t. Silty Sand,	fine- to medium-graine slightly organic, black fine- to medium-graine Peat, with a trace of G vet.	and br	own, _ ed with	V 6				
884.1 7.0 - - 881.1 10.0	PT 44	browi	T, with Sand : n, wet.	seams, fibrous, black a	ind da	rk –	2	立			
	SP	with a	a trace of Gra	D SAND, fine- to coars ivel, gray, waterbearing (Alluvium) at 15 feet.			TW*		*Thinwall sample.		
870.1 21.0		Wate auge Wate hollow	r in the groun er observed a w-stem auger er not observe	t 9 feet with 9 1/2 feet ad. t 12 feet with 19 1/2 fer in the ground. ed to cave-in depth of 7 withdrawal of auger.	et of	ow-stem	13				



Braun Proje			BORING:			S	ST-3	
	esign-Stat Reconstruc		LOCATIO	N: Se	e atta	ache	d sketch.	
DRILLER: C.	Powers	METHOD: 3 1/4" HSA, Autohammer	DATE:	3/27	7/09		SCALE:	1" = 4'
Elev. Depth feet feet 892.1 0.0	ASTM Symbol	Description of Materials (ASTM D2488 or D2487)		BPF	WL	qu tsf	Tests o	or Notes
	CL	FILL: Silty Sand, fine- to medium-grained, non-slightly organic, black, moist. (Topsoil/Fill) FILL: Silty Sand, fine- to coarse-grained, with a Gravel, brown, moist. LEAN CLAY, slightly organic, with a trace of fibblack, wet, rather soft. (Alluvium) LEAN CLAY, with a trace of fibers, light gray, we rather soft to medium. (Alluvium) POORLY GRADED SAND, fine- to coarse-grain with a trace of Gravel, brown to gray, moist to waterbearing, loose. (Alluvium) END OF BORING. Water observed at 12 feet with 12 feet of hollowauger in the ground. Water observed at 16 feet with 19 1/2 feet of hollow-stem auger in the ground. Water not observed to cave-in depth of 4 feet immediately after withdrawal of auger. Boring immediately backfilled.	ers, vet, ned,	12 4 4 8 7 9	文	1		ST-3 page 1 of



Braun Proje			BORING:			ST-4	
	esign-State Hig econstruction	ATORY TESTING ghway 7 & Louisiana Avenue	LOCATIO	N: Se	e attach	ned sketch.	
DRILLER: C. P	Powers	METHOD: 3 1/4" HSA, Autohammer	DATE:	3/2	7/09	SCALE:	1" = 4'
Elev. Depth feet feet 895.7 0.0	ASTM Symbol	Description of Materials (ASTM D2488 or D2487)		BPF	WL	Tests or I	Notes
895.0 0.7 - - - - - - - - - - - - -	FILL trace wet. FILL Graved ark SP-SM POC coar loos SP POC with 1/2 1 Wat hollo Wat hollo Wat with with thollo Wat wit	(Topsoil/Fill) : Clayey Sand, fine- to medium-grained, well and wood, with Silty Sand layers, brown to brown, moist to wet. ORLY GRADED SAND with SILT, fine- to rse-grained, with a trace of Gravel, brown, response to the same of the	moist,		▽		



Braun Projec			BORING:			S	ST-5	
	esign-State I econstruction	RATORY TESTING Highway 7 & Louisiana Avenue on	LOCATIC	N: Se	e atta	ache	d sketch.	
DRILLER: C. P.	owers	METHOD: 3 1/4" HSA, Autohammer	DATE:	3/2	7/09		SCALE:	1" = 4'
	ASTM Symbol	Description of Materials (ASTM D2488 or D2487)		BPF	WL	qu tsf	Tests	or Notes
- 889.8 7.0	FILL Signal Sign	ILL: Silty Sand, fine- to medium-grained, non ightly organic, black, moist. (Topsoil/Fill) ILL: Poorly Graded Sand with Silt, fine- to barse-grained, with a trace of Gravel, with Silt beams, brown and dark brown, moist. ILL: Clayey Sand, fine- to medium-grained, vand layers, with a trace of Gravel, dark brown rown, moist to wet. ILL: Poorly Graded Sand with Silt, fine- to barse-grained, with a trace of Gravel, brown, compared to barse-grained, with a trace of Gravel, black (Swamp Deposit) EAN CLAY with SAND, gray, wet, medium. (Alluvium) OORLY GRADED SAND with SILT, fine- to barse-grained, gray, moist, loose. (Alluvium) ND OF BORING. Vater not observed with 19 1/2 feet of hollow-suger in the ground. Vater not observed to cave-in depth of 10 feet namediately after withdrawal of auger. oring immediately backfilled.	vith Silty and, wet	28 21 14 8 7 7		1 1/2		ST-5 page 1



	n Proje							ВС	RING:			S	T-6		
Prelin Inters		esign Recons	-Star	te Hig ction	TORY TESTI ghway 7 & L		Avenue	LO	CATIO	N: Se	e att	achec	l sketch.		
DRILLE	R: C.	Powers	6		METHOD:	3 1/4" HSA	A, Autohammer	DA	TE:	3/27	7/09		SCALE:	1" = 4'	
Elev. feet 892.2	Depth feet 0.0	AST Sym	bol	8 inc	(A		of Materials 3 or D2487) 22 inches of agg	regate		BPF	WL		Tests o	or Notes	
_ 889.7	2.5			base	€.										
_ 888.2	4.0	FILL		of G	ravel, dark br	own, moist.		h a tra	ce _	23					
		FILL		coar	.: Poorly Grad rse-grained, w d seams, brov	rith a trace o	vith Silt, fine- to of Gravel, with C	Clayey		13					
885.2 -	7.0	FILL		FILL of G	.: Silty Sand, ravel, dark br	fine- to me own, moist.	dium-grained, w	ith a tr	ace	4*		*Littl	e sample	recovery.	
883.2	9.0	PT	× 44	PEA	λΤ, semi-fibroι	us, black to (Swamp [dark brown, we Deposit)	t.		3		To the state of th			
 880.2	12.0		<u> </u>						_						
 		SP					ine- to coarse-g waterbearing, lo ium)			TW*	∇	*Thir	nwall sam	ple.	
 871.2	21.0									6		Action of the Control			
- -				Wat holld Wat holld	ow-stem auge	at 14 feet wi r in the gro at 17 feet wi r in the gro	ith 19 1/2 feet of und.								
- - -					3										
 BL-09-0074	15					Brau	n Intertec Corporation	n	_					ST-6 page	e 1



Braun Pro							ВОР	RING:			S	T-7		
SOIL BORIN Preliminary Intersection St. Louis Pa	/ Desig n Reco	n-Sta nstru	te Hig ction			a Avenue	LOC	CATIO	N: Se	e att	ache	d sket	ch.	
DRILLER:	M. Taka	da		METHOD:	3 1/4" H	SA, Autohammer	DAT	E:	3/20	6/09		SCA	LE:	1" = 4'
Elev. Dep feet fee 893.4	t AS	STM mbol				n of Materials 188 or D2487)			BPF	WL	qu tsf	MC %	Tes	ts or Notes
893.4 (0 892.8 (0).0 Sy	mbol L S S S S S S S S S S S S S S S S S S	SILT fiber PEA	: Clayey Sai titly organic, v : Silt (possib TY SAND, fin rs, slightly organics, slightly organics, slightly organics)	aSTM D24 nd, fine- to vith a trace (Tops ole fly ash e- to med ganic, blace (Allu ark brown (Swamp SAND, g (Allu ED SAND vith a trace	ium-grained, with waterbearing.	a trace o	vet	5 2 4 6 TW*	Ϋ́		1		wall sample
872.4 2 ⁻	1.0		Wate Hollo Wate imme	erbearing, loc OF BORING er observed a ow-stem auge er not observediately after	(Allu G. at 19 feet er in the g red to cav	with 19 1/2 feet or round. e-in depth of 14 f	of feet		7					



1	_			0-00745	BORING	:		ST-8
Prelim Interse		esign Recon	-Stat		LOCATIO	DN: S€	e att	tached sketch.
DRILLE	R: J.	Cherma	ak	METHOD: 3 1/4" HSA, Autohammer	DATE:	3/2	5/09	SCALE: 1" = 4'
Elev. feet 893.9	Depth feet 0.0	AST Sym	bol	Description of Materials (ASTM D2488 or D2487)		BPF	WL	Tests or Notes
892.4	7.0	FILL SP		6 inches of bituminous over 12 inches of aggrebase. FILL: Silty Sand, fine- to coarse-grained, with concrete fragments and bituminous fragments brown, moist. FILL: Peat, black, wet. FILL: Lean Clay, non- to slightly organic, with Sand seams, black and gray, wet. POORLY GRADED SAND, fine- to coarse-grawith Gravel, gray to brown, waterbearing, med dense. (Alluvium) END OF BORING. Water observed at 12 feet with 12 feet of hollowager in the ground. Water observed at 17 feet with 19 1/2 feet of hollow-stem auger in the ground. Water not observed to cave-in depth of 8 feet immediately after withdrawal of auger. Boring immediately backfilled with bentonite ground.	Gravel,	14 8 8 6 8 20 27*	Ţ	*Encountered Gravel. No sample recovery.
BL-09-0074	5	deserve		Braun Intertec Corporation				ST-8 page 1 c



	-			0-00745	BORING	:		ST-9
Prelim Interse		esign lecon	-Stat		LOCATIO	ON: Se	e att	ached sketch.
DRILLE	:R: J. (Cherma	ak	METHOD: 3 1/4" HSA, Autohammer	DATE:	3/2	5/09	SCALE: 1" = 4'
Elev. feet 890.7	Depth feet 0.0		bol	Description of Materials (ASTM D2488 or D2487)		BPF	WL	Tests or Notes
889.3	1.4	PAV		6 inches of bituminous over 10 inches of aggrebase.	egate -			
		FILL		FILL: Silty Sand, fine- to coarse-grained, with dark brown, moist.	Gravel, _	28		
886.7	4.0	FILL		FILL: Poorly Graded Sand with Silt, fine- to coarse-grained, with a trace of Gravel, brown,	moist	16	立	
883.2	7.5	PT		PEAT, semi-fibrous, dark brown, wet. (Swamp Deposit)		5 4 TW*		*Thinwall sample.
878.7	12.0	OL		ORGANIC SILT, with shells, light gray, wet. (Swamp Deposit)		4		
874.7	16.0	SP		POORLY GRADED SAND, fine- to coarse-gra with a trace of Gravel, gray, waterbearing, med dense to very loose. (Alluvium)		TW*		*Thinwall sample. *No sample recovery.
869.7	21.0			END OF BORING.		4	1777 THE TOTAL OF	
				Water observed at 17 feet with 17 feet of hollo auger in the ground. Water observed at 15 feet with 19 1/2 feet of hollow-stem auger in the ground. Water observed at 6 feet with a cave-in depth feet immediately after withdrawal of auger. Boring immediately backfilled with bentonite ground.	- - of 6 1/2 _			
-								



Γ	Braur	n Proje	ect B	L-09	9-00745	BORING			ST-10					
	Prelim Interse	inary D ection R	esign tecon	-Star		LOCATIO	DN: Se	e atta	ached sketch.					
ŀ	St. Lou	iis Park, R· D	, Min i Bailey	neso	METHOD: 3 1/4" HSA, Autohammer	DATE:	3/26/09 SCALE: 1" = 4'							
-	Elev. feet	Depth feet	AST	-1/1	Description of Materials] =/=.	BPF	WL	Tests or Notes					
	896.2	0.0	Sym	- 1	(ASTM D2488 or D2487)		J. ,	***	16313 01 140163					
	895.4	0.8	PAV	×××	9 inches of bituminous.	0								
	894.2	2.0	FILL	\bowtie	FILL: Silty Sand, fine- to coarse-grained, with dark brown, moist.									
	- 892.2	4.0	FILL		FILL: Silty Sand, fine- to medium-grained, wit concrete fragments and Clayey Sand layers, obrown and black, moist.	h dark _	8							
iations)	 - 889.2	7.0	FILL		FILL: Poorly Graded Sand, fine- to coarse-grawith a trace of Gravel, brown, moist.	ained, — –	12	WANTER A SPECIAL PROPERTY OF THE WANTER STATES CONTRIBUTION OF THE SPECIAL PROPERTY.						
of abbrevi	- 887.2	9.0	FILL		FILL: Silty Sand, fine- to medium-grained, wit Clay layers, with a trace of Gravel, brown and moist to wet.		11							
r explanation	_		FILL		FILL: Organic Clay, with a trace of Gravel and with Sand layers, black and dark brown, wet.	d fibers, ——	8							
gy sheet fo	884.2	12.0	PT	× ± ±	PEAT, fibrous, dark brown, wet. (Swamp Deposit)		7							
Descriptive Terminology sheet for explanation of abbreviations)				7 77 77 7 77			8							
escript	_			7 77 7 77		_			*Thinwall sample.					
(See D	- 877.2	19.0		77 77 77 77			TW*	Δ	**END OF BORING AT 31 FEET.					
	-		SP		POORLY GRADED SAND, fine- to coarse-grawith a trace of Gravel, gray, waterbearing, loo loose. (Alluvium)		8		Water observed at 19 feet with 19 1/2 feet of hollow-stem auger in the ground.					
7/15/09 11:42						. -			Water observed at 18 feet with 29 1/2 feet of hollow-stem auger in the ground.***					
08.GDT							4*	***************************************	*No sample recovery.					
LOG OF BORING 00745.GPJ BRAUN_08.GDT 7/15/09 11:42						-			***Boring immediately backfilled with bentonite grout.					
NG 00	- 866.2	30.0												
OF BORII	865.2	31.0	SC		CLAYEY SAND, fine- to medium-grained, with of Gravel, gray, wet, very stiff.** (Glacial Till)	n a trace	17							
	BL-09-0074	5	<u></u>		Braun Intertec Corporation		Ц		ST-10 page 1 of 1					



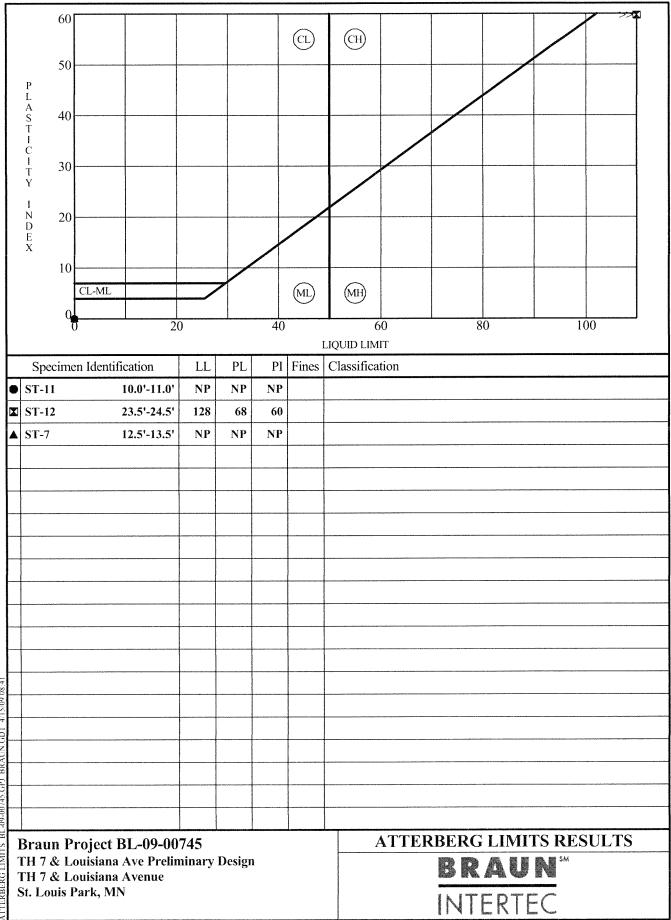
		n Proje							BORING:			S	T-11	
	Prelim Interse		esign lecon	-Stat	te Hig ction	TORY TESTI thway 7 & L	NG ouisiana Ave	enue	LOCATIO	N: Se	e att	ache	d sketch.	
	DRILLE	R: M.	Takada	э		METHOD:	3 1/4" HSA, A	utohammer	DATE:	3/2	6/09		SCALE:	1" = 4'
	Elev. feet 891.7	Depth feet 0.0	AS7 Sym	- 1			escription of M STM D2488 or			BPF	WL	MC %	Tests	or Notes
-	- - 887.7	4.0	FILL		orga black	nic, with a track and dark bro	d, fine- to med ce of Gravel, w own, wet. (Topsoil/Fil d, fine- to med	vith Silty Sand	seams, _	14				
viations)	 - 884.7	7.0			trace	e of Gravel, da	ark brown and	gray, wet.		7				
ation of abbre	-		PT	7 4 4 7 4 7 4 7 4	PEA wet.	T, fibrous to s	semi-fibrous, da (Swamp Dep		lack, - -	7				
(See Descriptive Terminology sheet for explanation of abbreviations)										TW*	<u> </u>	436	*Thinwall s	
	872.7	19.0	OL		ORG	GANIC SILT, v	with shells, ligh (Swamp Dep	t gray, wet. osit)		4	and the second s		feet with 2 hollow-ste ground. Water obs	served at 24 5 1/2 feet of m auger in the
UN_08.GDT 7/1.	 - 864.7	27.0			With	Sand seams	at 25 feet.			4			hollow-ster ground. Water not	9 1/2 feet of m auger in the observed to
LOG OF BORING 00745.GPJ BRAUN_08.GDT 7/15/09 11:42	_	a () V	SP		POC with	ORLY GRADE a trace of Gra	D SAND, fine- avel, green, wa (Alluvium	terbearing, loc	ined, ose 				cave-in de immediate withdrawal	pth of 19 feet ly after of auger.
OG OF BORIN	860.7	31.0			END	OF BORING).*			7			grout.	with bentonite
	3L-09-0074	5			L		Braun Inte	ertec Corporation				-		ST-11 page 1 of



4		n Proje							BORING	:		S	T-12	
						TORY TESTI ghway 7 & L		renue	LOCATION	ON: Se	e att	ache	d sketch.	
ln	iterse	ection R	econ	stru	ction	•			Genralization					
	t. Lou	iis Park, R: J. (. IVIINI Cherma		ta	METHOD:	3 1/4" HSA, A	Autohammer	DATE:	3/2	6/09		SCALE:	1" = 4'
E	lev.	Depth feet	AST			<u> </u>	escription of M			BPF	WL	мс		or Notes
8	95.9	0.0	Sym		0.4/0		STM D2488 c					%		
 - 8	94.4	1.5	PAV		base		uminous over	12 inches of a	aggregate -					
			FILL		FILL coar	: Poorly Grac se-grained, w	ded Sand with	Silt, fine- to Gravel, brown,	moist.	28				<u>.</u>
eviations)	88.9	7.0	FILL		EILI	· Poorly Grac	dad Sand fine	e- to coarse-gra		16				
lanation of abbr	_							wn and brown,		15 M 9				
ogy sheet for expl	81.9	14.0							- - -	X 5*	Δ		*Little sam	ple recovery.
Descriptive Termino			FILL		med	.: Poorly Grad lium-grained, v erbearing.	ded Sand with with a trace o	Silt, fine- to f Gravel, dark l	brown,	9				
8	76.9	19.0	SM	\bowtie	SILT	V SAND fine	- to medium-	grained, dark b)rown	1				
	-		JIVI			erbearing.	(Possible	_		8 🛚				
_8	74.9	21.0	PT		PEA	T, black, wet.				$\uparrow \uparrow$			Į.	
				<u>v</u> <u>v</u> :			(Swamp De	posit)		M 5				
9 11:4;	72.4	23.5	OL	1, 11	ORG	GANIC SILT, v	with shells lia	ht grav wet		TW*		117	*Thinwall s	ample.
7/15/0					Oile	J, II TIO OILI, V	(Swamp De						LL=128, PI DD=39 pcf	=60
8.GDT				閏					_	4			- 55 50.	
AUN O				目					_					
PJ BR									_					
9745.6	66.9	29.0												
ING OC	_		CL		LEA med			ganic, gray, we	et, 	₩ -		-		
LOG OF BORING 00745.GPJ BRAUN_08.GDT 7/15/09 11:42	64.9	31.0	0.5				(Alluviun	n)		7				
	0.003	1	SP				D1	dorton Cornection			<u></u>	<u></u>		ST-12 page 1 of 2
BL-0	9-0074	5					Braun In	tertec Corporation					`	ST-12 page 1 of 2



			9-00745	NC	BORING				2 (cont.)
Prelim Interse	inary Dection R		iction	NG .ouisiana Avenue	LOCATIO	ON: Se	e att	ache	d sketch.	
DRILLE	R: J. 0	Chermak	METHOD:	3 1/4" HSA, Autohammer	DATE:	3/2	6/09		SCALE:	1" = 4
Elev. feet 863.9	Depth feet 32.0	ASTM Symbol	(A:	escription of Materials STM D2488 or D2487)		BPF	WL	MC %	Tests	or Notes
_	-		with Gravel, gray,	D SAND, fine- to coarse-g waterbearing, medium der Alluvium) (continued)						
 859.9	36.0					20				
000.5	50.0		END OF BORING).						
			Water observed a hollow-stem auge	at 12 1/2 feet with 12 1/2 fee r in the ground.	et of					
			Water observed a hollow-stem auge	at 28 feet with 34 1/2 feet of r in the ground.	·					
			Boring immediate	ly backfilled with bentonite	grout.					
		The second secon			_					
	:				-					
					-					
					-		***************************************			
							-			
					-					
_					_	-				
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					MARINIPARAMANA					
_					-					
						11				ST-12 pag



BL-09-00745



Descriptive Terminology of Soil



Standard D 2487 - 00 Classification of Soils for Engineering Purposes (Unified Soil Classification System)

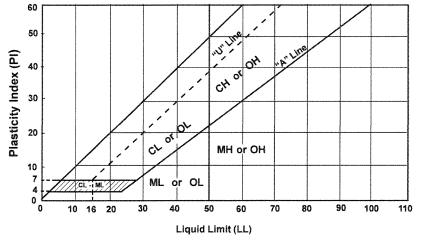
	Critari	ia for Accioni	na Group	Symbols and	Soi	ls Classification
		up Names Usi			Group Symbol	Group Name ^b
<u>"</u> 5	Gravels	C _u ≥ 4 and 1 ≤ C _c ≤ 3 ^c	GW	Well-graded gravel d		
red Soils retained o sieve	More than 50% of coarse fraction	GP	Poorly graded gravel d			
1 035	retained on	GM	Silty gravel ^{dfg}			
grained 50% ret 200 siev	No. 4 sieve	More than 12	% fines e	Fines classify as CL or CH	GC	Clayey gravel dfg
	Sands	Clean Sa	ands	$C_u \ge 6$ and $1 \le C_c \le 3^c$	SW	Well-graded sand ^h
Coarse- more than No.	50% or more of coarse fraction	5% or less	fines ^I	C _u < 6 and/or 1 > C _c > 3 ^c	SP	Poorly graded sand h
Soa ore t	passes	Sands with	Fines	Fines classify as ML or MH	SM	Silty sand ^{fg h}
Ĕ	No. 4 sieve	More than	12%	Fines classify as CL or CH	SC	Clayey sand ^{fgh}
<u>.</u> e	014	Inorganic	PI > 7 ar	id plots on or above "A" line ^j	CL	Lean clay kim
Soils ssed the	Silts and Clays Liquid limit	morganio	PI < 4 or	plots below "A" line!	ML	Silt k i m
	less than 50	Organic	Liquid lim	nit - oven dried < 0.75	OL	Organic clay k l m n
ned 9 pa 0 się			Liquid lin	nit - not dried	OL	Organic silt k I m o
grain more 5, 200	Silts and clays	Inorganic	Pl plots o	n or above "A" line	СН	Fat clay ^{k I m}
Fine-grained % or more pa No. 200 si	Liquid limit	inorganic	Pl plots b	elow "A" line	MH	Elastic silt k l m
Fin 50% o	50 or more	Organic	Liquid lim	nit - oven dried < 0.75	ОН	Organic clay k l m p
20		O. gaino	Liquid lim	nit - not dried	ОН	Organic silt ^{k i m q}
Highly	Organic Soils	Primarily orga	anic matter	, dark in color and organic odor	PT	Peat

- b. If field sample contained cobbles or boulders, or both, add "with cobbles or boulders or both" to group name.
- $C_u = D_{60} / D_{10} C_c = (D_{30})^2$ D₁₀ x D₆₀
- d. If soil contains≥15% sand, add "with sand" to group name
- Gravels with 5 to 12% fines require dual symbols:
 - GW-GM well-graded gravel with silt GW-GC well-graded gravel with clay
 - GP-GM poorly graded gravel with silt poorly graded gravel with clay
- If fines classify as CL-ML, use dual symbol GC-GM or SC-SM. If fines are organic, add "with organic fines" to group name.
- If soil contains ≥ 15% gravel, add "with gravel" to group name
- Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt
 - SW-SC well-graded sand with clay
 - SP-SM
 - poorly graded sand with silt poorly graded sand with clay
- If Atterberg limits plot in hatched area, soil is a CL-ML, silty clay.
- If soil contains 10 to 29% plus No. 200, add "with sand" or "with gravel" whichever is predominant if soil contains ≥ 30% plus No. 200, predominantly sand, add "sandy" to group name.
- If soil contains≥ 30% plus No. 200 predominantly gravel, add "gravelly" to group name
- PI ≥ 4 and plots on or above "A" line. o. Pl <4 or plots below "A" line

Dry density, pcf

- Pl plots on or above "A" line.
- q. Pl plots below "A" line.

DD



Laboratory Tests OC

Organic content, %

WD	Wet density, pcf	S	Percent of saturation, %
MC	Natural moisture content, %	SG	Specific gravity
LL	Ligiuid limit, %	C	Cohesion, psf
PL	Plastic limit, %	Ø	Angle of internal friction
PI	Plasticity index, %	qu	Unconfined compressive strength, psf
P200	% passing 200 sieve	qр	Pocket penetrometer strength, tsf

Particle Size Identification

Boulders	over 12"
Cobbles	3" to 12"
Gravel	
Coarse	3/4" to 3"
Fine	No. 4 to 3/4"
Sand	
Coarse	
Medium	No. 10 to No. 40
Fine	No. 40 to No. 200
Silt	< No. 200, PI < 4 or
	below "A" line
Clay	< No. 200, PI≥4 and
	on or above "A" line

Relative Density of **Cohesionless Soils**

Very loose	0 to 4 BPF
Loose	5 to 10 BPF
Medium dense	11 to 30 BPF
Dense	31 to 50 BPF
Very dense	over 50 BPF

Consistency of Cohesive Soils

Very soft	0 to 1 BPF
Soft	2 to 3 BPF
Rather soft	4 to 5 BPF
Medium	6 to 8 BPF
Rather stiff	9 to 12 BPF
Stiff	13 to 16 BPF
Very stiff	17 to 30 BPF
Hard	over 30 BPF

Drilling Notes

Standard penetration test borings were advanced by 3 1/4" or 6 1/4" ID hollow-stem augers unless noted otherwise, Jetting water was used to clean out auger prior to sampling only where indicated on logs. Standard penetration test borings are designated by the prefix "ST" (Split Tube). All samples were taken with the standard 2" OD split-tube sampler, except where noted

Power auger borings were advanced by 4" or 6" diameter continuousflight, solid-stem augers. Soil classifications and strata depths were inferred from disturbed samples augered to the surface and are, therefore, somewhat approximate. Power auger borings are designated by the

Hand auger borings were advanced manually with a 1 1/2" or 3 1/4" diameter auger and were limited to the depth from which the auger could be manually withdrawn. Hand auger borings are indicated by the prefix

BPF: Numbers indicate blows per foot recorded in standard penetration test, also known as "N" value. The sampler was set 6" into undisturbed soil below the hollow-stern auger. Driving resistances were then counted for second and third 6" increments and added to get BPF. Where they differed significantly, they are reported in the following form: 2/12 for the second and third 6" increments, respectively.

WH: WH indicates the sampler penetrated soil under weight of hammer and rods alone; driving not required.

WR: WR indicates the sampler penetrated soil under weight of rods alone: hammer weight and driving not required

TW indicates thin-walled (undisturbed) tube sample.

Note: All tests were run in general accordance with applicable ASTM standards

Appendix E

Braun Soil Borings, 2004

Elev. feet feet feet feet feet feet feet fee	ant st corne e Street.
GEOTECHNICAL EVALUATION Louis and Avenue Improvements Lake Street to Walker Street St. Louis Park, Minnesota DRILLER: Dave Lovassen METHOD: 3 1/4" HSA Autohammer DATE: 1/16/04 SCALE: 1* Elev. feet feet feet feet feet and Roots, dark brown, wet. FILL: Clayey Sand, fine- to medium-grained, with Gravel and Roots, dark brown, wet. FILL: Clayey Sand, fine- to medium-grained, with a trace of Gravel, brown to dark brown, wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist and Limestone fragments, brown with a trace of Gravel and Limestone fragments, brown with a trace of Gravel and Limestone fragments, brown with a trace of Gravel and Limestone fragments, brown with a trace of Gravel and Li	ant st corne
Lake Street to Walker Street St. Louis Park, Minnesota DRILLER: Dave Lovassen METHOD: 3 1/4" HSA Autohammer DATE: 1/16/04 SCALE: 1 Elev. Depth feet feet feet ASTM (ASTM D2488 or D2487) FILL Clayey Sand, fine- to medium-grained, with Gravel and Roots, dark brown, wet. FILL Clayey Sand, fine- to medium-grained, with a trace of Gravel, brown to dark brown, wet. FILL Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. Season 14 OL ORGANIC CLAY, with shells, black, wet. OL ORGANIC CLAY, with shells, black, wet.	ant st corne
DRILLER: Dave Lovassen METHOD: 3 1/4" HSA Autohammer DATE: 1/16/04 SCALE: 1"	ant st corne
Blev. Depth feet ASTM Description of Materials ASTM Description of Materials ASTM Description of Materials Description of Materials ASTM Description of Materials Description of Description of Materials Descrip	ant st corne
feet feet ASTM Description of Materials BPF WL Tests or Note	ant st corne e Street.
96.9 0.0 Symbol (ASTM D2488 or D2487) FILL: Clayey Sand, fine- to medium-grained, with Gravel and Roots, dark brown, wet. 94.9 2.0 FILL Clayey Sand, fine- to medium-grained, with a trace of Gravel, brown to dark brown, wet. 91.9 5.0 FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. 98.9 8.0 PT PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) 3 Foreign odor detected samples from 10 to 20 82.9 14.0 OL ORGANIC CLAY, with shells, black, wet 3	ant st corne e Street.
and Roots, dark brown, wet. FILL: Clayey Sand, fine- to medium-grained, with a trace of Highway 7 and Lak elevation equals 100.0 FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist (Swamp Deposit) Foreign odor detected samples from 10 to 20 Resp. 14.0 OL ORGANIC CLAY, with shells, black, wet.	st corne e Street.
94.9 2.0 FILL FILL: Clayey Sand, fine- to medium-grained, with a trace of Gravel, brown to dark brown, wet. 91.9 5.0 FILL FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. 88.9 8.0 PT PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) 92.	e Street.
of Gravel, brown to dark brown, wet. 91.9 5.0 FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. 988.9 8.0 PT PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) 3 Foreign odor detected samples from 10 to 20 82.9 14.0 OL ORGANIC CLAY, with shells, black, wet.	
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FILL FILL: Silty Sand, with fibrous Peat, with a trace of Gravel and Limestone fragments, brown with black, moist to wet. PT PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) 2 Poreign odor detected samples from 10 to 20 82.9 14.0 OL ORGANIC CLAY, with shells, black, wet.	
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to wef. Second Secon	
PT 1/2 PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) Foreign odor detected samples from 10 to 20 2 2 82.9 14.0 OL — ORGANIC CLAY, with shells, black, wet. OL — ORGANIC CLAY, with shells, black, wet.	
PT 1/2 PEAT, fibrous, dark brown to black, wet. (Swamp Deposit) Foreign odor detected samples from 10 to 20 2 2 82.9 14.0 OL — ORGANIC CLAY, with shells, black, wet. OL — ORGANIC CLAY, with shells, black, wet.	
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Foreign odor detected samples from 10 to 20 82.9 14.0 OL — ORGANIC CLAY, with shells, black, wet.	
2 82.9 14.0 OL — ORGANIC CLAY, with shells, black, wet.	n all
82.9 14.0 V V V V V V V V V	reet.
82.9 14.0 V V V V V V V V V	
82.9 14.0 0L — ORGANIC CLAY, with shells, black, wet.	
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70 10	
78.9 18.0	•
brown, waterbearing, medium dense. (Alluvium)	
	10 f
- END OF BORING. Tar/oil observed in the sample.	.0-100t
Water observed at 18 feet while drilling.	
An open triangle in the Boring immediately backfilled with grout.	cates
the depth at which grou was observed while dril	ndwater
solid triangle indicates to stable groundwater leve	he _
	i illi the
Groundwater levels fluc	atea.
	tuate.
	ated. tuate.
	ated. tuate.
	ated, tuate.
	ated. tuate.
L-04-02033 Braun Intertec Corporation, Edina ST-1	ated. tuate.

LOG OF BORING

	LOCATIO	N: Se	e atta	ched	sketch.					
					LOCATION: See attached sketch.					
Lake Street to Walker Street St. Louis Park, Minnesota										
utohammer	DATE:	1/10	5/04	T	SCALE:	1" = 4"				
Elev. Depth										
Description of Materials										
r D2487)										
um-grained, wit	h Gravel									
	· 1	· ·								
n-grained with t	fibrous	1 4			••					
e of Gravel and	4	<u> </u>				•				
t to wet.				٠.	· · · :					
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um-grained, with	h Silty	.16				· · · · · · · · · · · · · · · · · · ·				
i, Limestone fra	gments /	1 .				• • •				
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th of 6 feet imm	ediately –		٠.							
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	faterials D2487) um-grained, with regrained, with the of Gravel and t to wet.	faterials D2487) um-grained, with Gravel n-grained, with fibrous to of Gravel and t to wet.	faterials D2487) um-grained, with Gravel n-grained, with fibrous to of Gravel and t to wet. 7 um-grained, with Silty Limestone fragments 16 19	faterials D2487) um-grained, with Gravel n-grained, with fibrous to of Gravel and t to wet. 7 um-grained, with Silty I, Limestone fragments 16	faterials D2487) um-grained, with Gravel n-grained, with fibrous to of Gravel and t to wet. 7	faterials D2487) um-grained, with Gravel n-grained, with fibrous to of Gravel and t to wet. 7				

Braun Project BL-04-02033 GEOTECHNICAL EVALUATION						ST-3									
Louis Lake	siana Ave Street to		rovements Street				LOCATION	LOCATION: See attached sketch.							
DRILL		ive Lovassen		METHOD:	3 1/4" HSA	Autohammer	DATE:	1/16/04			SCALE:		1" = 4'		
Elev. feet 99.1	Depth feet 0.0	ASTM Symbol		. (A:	escription of STM D2488	or D2487)		BPF	WL	MC	oc %	Tes	sts or Notes		
		FILL X	FILL sligh	: Clayey Sand itly organic, wi	l, fine- to me th a trace of	dium-grained, r Gravel, dark bro	on to								
							-	Ŭ · 5		16	4				
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93.6	5.5		END	OF BORING.	·										
			Wate	er not observed	while drillin	g.	_								
_			Borin	ng immediately	backfilled.					٠.			· · · · · .		
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	Bra	un Proj	ect E	BL-0	4-02	033		BORING	:		Ś	T-4		
		OTECHN isiana Av					ľ	LOCATIO	DN: Se	e att	ached	sketch.		
		e Street to												
		ouis Parl				·				٠				
	DRIL	LER: Da	ave Lov	assen		METHOD: 3 1/4" HSA Autohammer		DATE:	1/1	6/04		SCALE:	1" =	= 4 '
	Elev.		A ÓS	DN 4					~~~.			<u>-</u>		
1	feet 99.	· 1	AS7 Sym			Description of Materials (ASTM D2488 or D2487)	٠.		BPF	WL		Tests o	or Notes	
ļ	• • • • • • • • • • • • • • • • • • • •		FILL		FILL	: Clayey Sand, fine- to medium-grained,	with	n a trace						
	97.0	6 1.5	1377 -	\bigotimes		ravel and Roots, dark brown and black, we								
-	• ,		FILL	₩	FILL Grave	: Silty Sand, fine- to medium-grained, wi el and Concrete, brown with dark brown,	ith a moi	trace of	10				*	
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Tatio	•			₩.										
brev	· · · · .			\bowtie			•		8 -			•		
ot ab					With	Peat layers from 8 to 11 feet.		1	1 1				•	· . [
non				XX				1			• •			
ana –									7	∇				
	88.1	11.0	SP-	XXX	POOF	RLY GRADED SAND with SILT, fine- to	<u> </u>			· .	٠.		: .	
2	· · · · ·	1	SM		mediu	im-grained, with a trace of Gravel, gray,	-	+	11	• •	<i>a</i> .			
	. :			***	watert	bearing, loose to medium dense. (Alluvium)	;	<u> </u>	11		٠.			٠ .
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F		15			END C	OF BORING.			1, 11	•			• • •	
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						immediately backfilled with grout.					· .			.[
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INTERTEC

Bı	rau	n Proj	ject	BL-	04-02	033		BORIN	G:		S	T-5	
		ECHN ana Av				ATION lents		LOCAT	ION: S	See atta	ached	sketch.	
La	ke S	treet t	o Wa	lker	Street			.					
St.	Loi	iis Par	k, Mi	innes	ota		A Commence of the Commence of						
DR.	ILLE	R: D	ave Lo	vassen	1	METHOD:	3 1/4" HSA Autohammer	DATE:	1/2	16/04		SCALE:	1" = 4'
Ele fee		Depth feet	Ας.	STM		De	escription of Materials		מממ	33.77			
	8.0	0.0		mbol			STM D2488 or D2487)		BPF	WL		Tests or	Notes
	: '	. :	FILI			: Sandy Lean	Clay, with Gravel and Roo	ots, dark					
- 0,	6.0	2.0			y blow	n, wet.			1				
	0.0	2.0	FILI	- XXX	FILL	: Sandy Lean	Clay, with a trace of Grave	el and	16				
· - ·			:		Lime	estone fragment n, gray and bla	ts, with fibrous Peat layers	s, dark	-{}		·:		
+		٠.		\bowtie		-, 6, ,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	·		-	:		-	
<u> </u>				\bowtie				· · · · · · · · · · · · · · · · · · ·	4				
92	2.0	6.0	· CL	XX	1 T7 A >	NICIAN!	a tunna a C P.1		1				
Zigari L			LCL		to me	N CLAY, with edium.	a trace of Fibers, gray, we	n, rather soft	Ц	.	Ċ		
DOLE							(Alluvium)		₩ 4	又			
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	. .												4.4
									<u>-</u> ₩ 8:				
\$		100	4.									•	
86	-0	12.0	SP-		POOF	RLY GRADED	SAND with SILT, fine-t	to	M 5	T	• • •		
-			SM		mediu	ım-grained, wit	th a trace of Gravel, grav.	-	И				
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		.			the aug	ger.					:		
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·2-0:4-020	در		. •				Braun Intertec Corporation, Ed	iina		· '. '			ST-5 page 1 of 1

Appendix F

STS Soil Borings, 1989

			T	1WC	IER			LOG	OF BOR	ING I	UMBER	1					
G	4			(City of St.	Louis Park	1		B-1								
	"		7			I. 7 Surcharge			HTECT.		NEER						
STS Co	- Isultan	s Ltd.				Lsiana Avenue	İ	В	RW I	nc.							
SITE LO	CATIO	4					······································			Ю	ייאכטיי	FINEDO	CAPPES	SIVE ST	RENGTH		
				5	St. Louis P	ark, Minnesota		1			i i	2	3	4			
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DEPTH	2	YPE	ST	,			-	- 1	\{\{\in\}\}	<u>_</u>	10	20	30	40	5		1
ĪN	SAMPLE NO	SAMPLE TYPE	SAMPLE DISTANCE	RECOVERY					UNIT DRY WT	ļ.							
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	_					Note: 3.5 inche	s aspha	lt				-	1				
	3				over silty	sand fill.											
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	THE S	HATIF	ICAT	ION	LINES REPRESENT	HE APPROXIMATE BOUNDAR	Y LINES BETWI	EEN SC	DIL TYPE	S. IN S	ITU, THE	TRANSI	TION MA	Y BE GI	ADUAL		
WL					WS OR WD	BORING STARTED	4/6/89	T	STS OF				esota				1
WL			ВСЯ	_	ACR	BORING COMPLETED	4/6/89		DRAWN		AN		ET NO.	1	OF	1	1
WL	16 0				hr. AB		REMAN GD	$\overline{}$	APP'D		MBS	-	JOB NO		9401		1
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		ı		IC	WNER	LOG OF BOR	ING N	JMBEF	1				
7	4			L	City of St. Louis Park	B-2		.===					
				P	ROJECT NAME T.H. 7 Surcharge at Old Louisiana Avenue	ARCHITECT-	ENGIN						
STS Con SITE L	OCA	TIO	a. N	1_	1.h. / Suicharge at Old Louisiana Avenue	L			NCONFINED DISSIFT,?	COMPRES	SIVE STRE	NGTH	
011111	-		••		St. Louis Park, Minnesota		1	U 1		3	4		
ELEVATION (FT)	SAMPLE NO.	APLE TYPE	APLE DISTANCE	OVERY	DESCRIPTION OF MATERIAL SURFACE ELEVATION Approx. + 180.5 fc.		ÚNIT DRY WT. LBS./FT	PL UI		CONTE		LIQUID LIMIT *	
\times	SA	SA.	S	# 1	SURFACE ELEVATION Approx. + 180.5 ft.		·\$	11					,
				-	Driller's Note: 3 inches asphalt over silty sar	ndy fill.							
5.0	1	SS			Peat and fine to coarse sand - black - saturated (possible fill)	i - (Pt) -			[₹⊗ 				
10.0	2	ST			Fine fibrous to amorphous peat, few shells - bla - (Pt)	ack -medium	26.3						192%
15.0	3	ST			Clayey silt, trace fine sand, few fine roots - staturated - loose (est.) - (ML-CL)	gray -	95.5		l		3		
25.0	5	SS							18 [®]	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\			
30.0	6	SS		II	Fine to coarse sand and gravel, trace silt - gr saturated - medium dense - (SW-SM)	ay -				29 @			
35.0	7	SS			Note: Clayey silt seam at 20.5 ft.				18/	,			
					(continued on next page)	-							
THESTRAT	IFICATI	ONUN	ES RE	PRE	SENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL TYPES: IN-SITU, THE TRANSITION MAY	BE GRADUAL,	STS JOB NO	940)19-H	SHEE	T NO.	1 of	2

		9]		OWNER		LOGOF	BORING N	UMBER	l		
1	1	Ų.		City of St. Loui							
	_			PROJECT NAME		ARCHITI	B-2 ECT-ENGI	NEER		***************************************	
STS Co				T.H. 7 Surcharge	at Old Louisiana Avenue		BRW, In	c.			
SITE	LOC	ATIO	N	St. Louis Park, Mi	innesota			-O- %	CONFINED COMP.	ESSIVE STRENGT	1
-	T-		П	1						3 4	s
DEPTH (FT) ELEVATION (FT)			삥	SURFACE ELEVATIO				PU UN	ASTIC I	ATER STENT %	LIQUID JMIT %
Ęğ		ᇤ	YY.	1 .	DESCRIPTION OF MATERIAL		<u> </u>	×		•	 △
DEPTH (FT) ELEVATION (EN	ETY	EDI					10	20	30 40	50
ă d	SAMPLE NO.	SAMPLETYPE	WPL				UNIT DRY WT.	8	STANDAR PENETRA	ON BLOW	
\times L	à	ŝ	S	SURFACE ELEVATION	N Approx. + 180.5 ft.		5	10		30 40	50
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	1	L		(continued from p	previous page)						
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60.0	12	ss	忡	Fine to coarse e	sand, some silt, trace to little	gravel				47	ial i
	+	133	##-	- brown - satura	ited - dense - (SM)	STUTCH				1 47	Ĭ
	1						1			/	
	1									1 1/	
65.0	13	SS	ШП							20/6"	\downarrow
	1.58	55	٣								53/6
				Limestone fragment bedrock)	ents - gray - extremely dense -	(apparer	12				1
69.5	14	SS	Ц.								400/1
	_		\prod	End of boring at	: 69.5 ft.					1	
	1			Hollow stem auge:	er to 20 ft. drilling mud 20 ft. to end of b	oring					
	1			MOTTER DIE WIEN	certifing mad 20 fet. to end of b	.gnr 10					
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		THE	STRAT	FICATION LINES REPRESENT	IT THE APPROXIMATE BOUNDARY LINES BETWEE	EN SOIL TYP	ES: IN-SITU. T	HE TRANS	ITION MAY BE	GRADUAL.	
WL				WS OR WD	BORING STARTED		STS OFFICE				
WL	٥.	J I	t. W		80RING COMPLETED		DRAWN BY		Innesota SHEET NO.	OF 0	
WL					4/7/89 RIGFOREMAN			AN			····
	0bsc	ured	d by	mud AB	D-50 GD		APP'O BY	MBS	STS JOB NO	94019-	a .

C	3		T	Ci	er ty of St. I	ouis Park		LOG	OF BOR	NG NUM B-4	BER				
STS Cons	ultant	s Ltd.	1	PRO.	ECTNAME uisiana Ave	. Reconstruc	ction	ARCH	ITECT-E	BRW,	Înc.	***************************************			
Loui			Ave	e./	Lake St.; S	St. Louis Par	ck, MN.			O- 'JN'			ESSIVE ST	PENGTH 5	
DEPTH IN FEET	SAMPLE NO	SAMPLE TYPE	SAMPLE DISTANCE	RECOVERY	SURFACE ELEVA	DESCRIPTION OF MA		·	UNIT DRY WT	IÇ Limi	STAN	CON1		BLOWS/F	2
	1	AS AS			base grav	of asphalt; and a sphalt; and a sphatt; and a sphalt; and a sphalt; and a sphalt; and a sphalt; and	avel - bro								
- 5 -	3 4	SS			Sandy org gravel - dense - (gravel re creosote	anic fill, poblack - dens Pt/SM) fro flected in h smell	eat, trace e to very zen materi igh blow c	al count				12/6 ⊗ ⊗2	" H		
-10-	5	SS			Medium to black t moist - creosot	coarse sand o brown - me (SP) rubbl e smell	, trace si dium dense e in fill;		15.0	8 🛇)*			34	6.4%
	7	ST		П		peat,trace s oist - (Pt)	Creosot		17.7)*			31	1.2%
-15-	8 8A	ST			Organic clays, s - black smell	peat,layered ilty clays & - moist - (P	with orga silty sar t) creoso	anic ad ote	33.0	O* 				19	1.0%
	9 9A	ST	Т	Ш	Clay, tr	ace sand - g		st -		<u> </u>	*	•	©		
-20-	10	SS	Ħ		Medium t and grav dense -	slight creos co coarse san cel - medium wet to satur	id, trace s dense to rated - (S)	M)		11 (⊗ <i>-</i> -	-			25/4
-25-	12	SS			3 inches slight o	sean of pea reosote odor	at at 23.5	ft.	O*	9 &		ed ne	netro	meter	
-30-					Hollow s	ooring at 25. stem augered packfilled an	to full de		1			, pe			
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FEET	SAMPLE NO	SAMPLE TYPE	SAMPLE DISTANCE	RECOVERY	SURFACE ELEVA	ATION 181.18 ft.		UNIT DRY WT LBS FT			TANDARI ENETRA			BLOWS/F	
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<u>-15-</u>	8	SS		٣		coarse sand, little gr	ave1					_	®	39	
	9	SS	П	П		medium dense - (SP)			10	ф-	-				
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	10	SS	+	h	1				1,0	\$	İ				
-20-	10	1	Ш	Ш				ļ	+-	Ψ.					
	1				End of 1	boring at 20.0 ft.		133	To	cvane	she	ar	strer	gth.	
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Appendix G

Braun Soil Borings, 1980

LOG OF BORING



PROJECT: 80-135 SOIL BORINGS
Louisiana Ave. Extension
Between Walker & W. Lake St.
St. Louis Park, Minnesota

BORING: ST-64 LOCATION: Station 110+50, 10' west of centerline.

ı	•			etween Walker & W. Lake St. t. Louis Park, Minnesota	wes	t of	E ce	enterlin	e.	
					DAT	E: -	5/2/	/80	SCAI	E: 1"=4"
	Elev. 179.5±	Depth 0	ASTM D2487 Symbol	Description of Materials (ASTM: D2488)		BPF	WL	Tests	OF	Notes
	177.5		SP-SM with Pt	Fill; SAND, SLIGHTLY SILTY, fir to medium-grained, mixed with some PEAT, black, moist to wet.		3	*			
ology.)	175.0	4.5	SP	Fill; SAND, fine to medium- grained, with a little fine Grayel, brown, wet.		7				·
descriptive terminology.)			Pt	PEAT, amorphous, with a trace of shells, wood and occasional lenses of MUCK, dark brown to black, wet.	of	3/1		MC = 3: OC = 7:		
criptiv						2		MC = 16 $OC = 2$		
	169.5	10		(Swamp Deposit)	-,	2		MC = 1		
tion and	166.5	13	SC-SM with SP	SILTY CLAYEY SAND, fine to medium-grained, with layers of fine-grained SILTY SAND and fine to coarse-grained SAND,*		11		OC = 3	wet,	
evaluation	165.0	14.5	SP	SAND, fine to medium-grained, gray, waterbearing.(Glacial Ou	itwa	sh)		Outwas	. (G1 sh)	aciai
fo		17	ML with SP	CLAYEY SILT, slightly plastic, with a few layers of fine to coarse SAND, gray, wet,**		11		**medi		se. utwash)
rd Plates	Į.		SP	SAND, fine to coarse-grained, gray, waterbearing, loose. slight chemical odor						
Standard	159±	20.5		(Glacial Outwash) Water level down 14' with 19'	of	10]			
and				hollow-stem auger in ground.						
Report	•			Water level down 2' 1/4 hour after completion of boring.						
(See Re	9			Water level down 2' 3-1/2 hour after completion of boring.	rs					
									5 0(49 6

LOG OF BORING



BORING: ST-65 PROJECT: 80-135 SOIL BORINGS Louisiana Ave. Extension LOCATION: Station 111+55 on Between Walker & W. Lake St. centerline. St. Louis Park, Minnesota DATE: 5/2/80 SCALE: 1"=4" Tests Notes ASTM BPF WL Description of Materials D2487 Elev. Depth (ASTM: D2488) 179.5 Symbo: Fill; SILTY SAND, fine to medium-11 grained, with a trace of fine* *Gravel, black, moist. 178.0 1.5 Fill; SAND, fine to coarse-20 grained, with a trace of fine Gravel, brown, wet. 19 173.0 6.5 173.0 6.5 20 170.0 9.5 PEAT, amorphous, dark brown to MC = 287.4%2 brown, wet. 0C = 50.5%(Swamp Deposit) MC = 186.9%MUCK, with a trace of shells and 0C = 33.3%wood, dark olive, moist. (Swamp Deposit) evaluation MC = 85.9%with a thin layer of bog lime. 13 166.5 DD = 47.8 pcfCLAYEY SILT, non to slightly plastic, with a trace of fibers, gray, wet, loose. MC = 30.3%(Alluvium) 163.5 16 SAND, fine to coarse-grained, Plates with some fine to medium Gravel, gray, waterbearing, medium dense. slight chemical odor. (Glacial Outwash) 13 159± 20.5 Water level down 13' with 19' of hollow-stem auger in ground. Water level down 3' 1/4 hour after completion of boring. Water level down 2' 2-3/4 hours after completion of boring. 5001.497

Appendix H

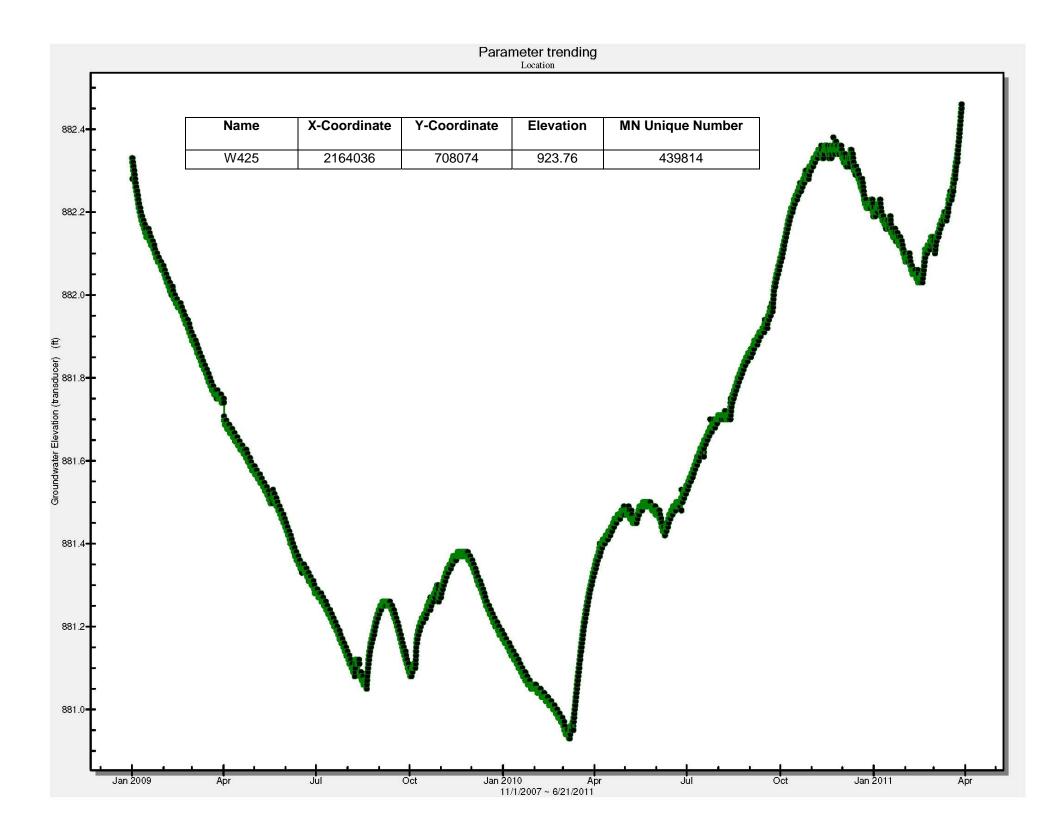
Groundwater Elevation Table

Water Level Data

		2011, Geotech				2011, Phase II				2009, Geotech	
Boring	Elevation	Water Depth (ft)	Water Elev	Boring	Elevation	Water Depth (ft)	Water Elev	Boring	Elevation	Water Depth (ft)	Water Elev
R-1	893.9	9	884.9	GP-01	894	7.2	886.8	B-1	889.1	5	884.1
R-2	892.9	7	885.9	GP-02	894	13	881.0	B-2	891.1	9	882.1
R-3	892.0	4	888.0	GP-03	893	11	882.0	B-3	892.1	12	880.1
R-4	895.3	7.5	887.8	GP-04	892	7.5	884.5	B-4	895.7	11.5	884.2
R-5	897.0	12	885.0	GP-05	893	4	889.0	B-5	896.8	-	-
R-6	897.0	4	893.0	GP-06	891	8	883.0	B-6	892.2	14	878.2
R-7	896.6	12	884.6	GP-07	894	8.5	885.5	B-7	893.4	19	874.4
R-8	888.0	4	884.0	GP-08	896	9.5	886.5	B-8	893.9	12	881.9
R-9	897.7	19	878.7	GP-09	895	9.7	885.3	B-9	890.7	6	884.7
E-1	896.5	17	879.5	GP-10	892	6.4	885.6	B-10	896.2	18	878.2
E-2	896.6	13	883.6	GP-11	892	6.4	885.6	B-11	891.7	11	880.7
E-3	896.6	12	884.6	GP-12	894	15	879.0	B-12	895.9	12.5	883.4
E-4	893.1	7	886.1	GP-13	895	-	-	Avg	St. Dev.	Max	Min
E-5	898.9	8	890.9	GP-14	895	8	887.0	881.1	3.2	884.7	874.4
C-1	895.3	7	888.3	GP-15	897	9	888.0				
C-2	895.4	8.5	886.9	GP-16	888	15.5	872.5				
C-3	895.7	10	885.7	GP-17	888	8	880.0				
C-4	897.1	12	885.1	GP-18	888	3	885.0				
C-5	897.2	12	885.2	GP-19	897	6	891.0				
C-6	897.6	15	882.6	GP-20	896	6	890.0				
C-7	897.6	15	882.6	GP-21	896	7.5	888.5				
C-8	898.3	15	883.3	GP-22	894	7.5	886.5				
C-9/9A	897.7	15	882.7	GP-23	896	11	885.0				
C-10	897.6	16	881.6	GP-24	898	12	886.0				
C-11	898.3	14	884.3	GP-25	897	7.6	889.4				
C-12	901.2	17	884.2	GP-26	905	23	882.0				
P-1	888.0	7	881.0	GP-27	907	-	-				
B-1	915.0	-	-	GP-28	906	21.9	884.1				
B-2	905.9	19	886.9	GP-29	893	19	874.0				
B-3	900.2	14	886.2	GP-30	890	12	878.0				
B-4	896.6	12	884.6	GP-31	894	-	-				
B-5	897.5	14	883.5	GP-32	893	7.6	885.4				
B-6	890.7	4	886.7	GP-33	893	7.5	885.5				
B-7	892.8	10.5	882.3	Avg	St. Dev.	Max	Min				
B-8	901.1	17	884.1	884.4	4.3	891.0	872.5				
B-9	904.8	-	-								
B-10	904.1	18	886.1								
B-11	911.7	-	-								
B-12	907.2	-	-								
B-13	906.8	-	-								
B-14	907.9	-	-								
Avg	St. Dev.	Max	Min								
884.9	2.8	893.0	878.7								

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Water Level Data from Summit Observation Well, W425



Appendix J

Literature Paper by Jim Collin

Geosynthetic-Reinforced Column-Support Embankment Design Guidelines

James G. Collin¹, J. Han², and J. Huang³

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Keywords: Load transfer platform, geosynthetic reinforcement, ground improvement.

Abstract

The problems associated with constructing highway embankments over soft compressible soil (i.e., large settlements, embankment instability and the long period of time required for consolidation of the foundation soil) has lead to the development and/or extensive use of many of the ground improvement techniques used today. Wick drains, surcharge loading, and geosynthetic reinforcement, have all been used to solve the settlement and embankment stability issues associated with construction on marginal soils. However, when time constraints are critical to the success of the project, owners have resorted to another innovative approach: geosynthetic reinforcement column supported embankments.

Column supported embankments (CSE) consist of vertical columns that are designed to transfer the load of the embankment through the soft compressible soil layer to a firm foundation. The load from the embankment must be effectively transferred to the columns to prevent punching of the columns through the embankment fill creating differential settlement at the surface of the embankment. If the columns are placed close enough together, soil arching will occur and the load will be transferred to the columns. In order to minimize the number of columns required to support the embankment and increase the efficiency of the design, a load transfer platform (LTP) reinforced with geosynthetic reinforcement is being used on a regular basis. The load transfer platform consists of one or more layers of geosynthetic reinforcement placed between the top of the columns and the bottom of the embankment.

This paper will present the guidelines for the design of column supported embankments developed by the authors under contract with the Federal Highway Administration. These guidelines were developed based on a review of current design methodologies and a parametric study of design variables using numerical modeling (FLAC).

1.0 DESCRIPTION

Column supported embankments consist of vertical columns that are designed to transfer the

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load of the embankment through the soft compressible soil layer to a firm foundation. The selection of the type of column used for the CSE will depend on the design loads, constructability of the column, cost, etc., and is not the focus of this paper (see Collin, 2004). The load from the embankment must be effectively transferred to the columns to prevent punching of the columns through the embankment fill causing differential settlement at the surface of the embankment. If the columns are placed close enough together, soil arching will occur and the load will be transferred to the columns. Figure 1 shows a conventional CSE. The columns are spaced relatively close together, and some battered columns are required at the sides of the embankment to prevent lateral spreading. In order to minimize the number of columns required to support the embankment and increase the efficiency of the design, a geosynthetically reinforced load transfer platform (LTP) may be used. The load transfer platform consists of one or more layers of geosynthetic reinforcement placed between the top of the columns and the bottom of the embankment. Figure 2 shows schematically a CSE with geosynthetic reinforcement.

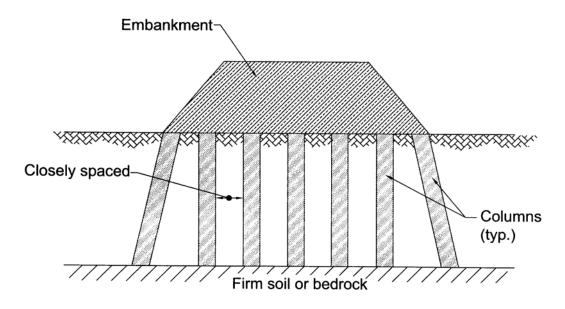


Figure 1. Conventional Column Supported Embankment

2.0 DESIGN CONCEPTS

The design of column supported embankments must consider both limit state, and serviceability state failure criteria. The limit state failure modes are shown in Figure 3. The columns must be designed to carry the vertical load from the embankment without failing (Figure 3a). The columns are typically assumed to carry the full load from the embankment. The lateral extent of the columns under the embankment must be determined (Figure 3b). The load transfer platform must be designed to transfer the vertical load from the embankment to the columns (Figure 3c). The potential for lateral sliding of the embankment on top of the columns must be addressed (Figure 3d). Finally, global stability of the system must be evaluated (Figure 3e).

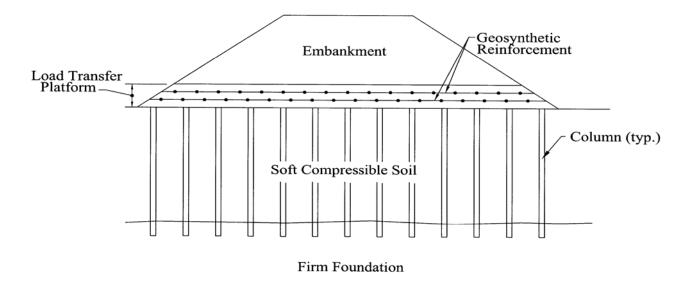


Figure 2. Column supported embankment with a geosynthetic reinforced load transfer platform

In addition to limit state analysis, serviceability state design must be considered. The strain in the geosynthetic reinforcement used to create the load transfer platform should be kept below some maximum threshold to preclude unacceptable deformation reflection (*i.e.*, differential settlement) at the top of the embankment. Settlement of the columns must also be analyzed to assure that unacceptable settlement of the overall system does not occur, as shown in Figure 4.

The general design steps for a CSE are provided below:

- 1. Estimate preliminary column spacing (use feasibility assessment guidelines).
- 2. Determine required column load.
- 3. Select preliminary column type based on required column load and site geotechnical requirements.
- 4. Determine capacity of column to satisfy limit and serviceability state design requirements.
- 5. Determine extent of columns required across the embankment width.
- 6. Select LTP design approach (*i.e.*, catenary or beam).
- 7. Determine reinforcement requirements based on estimated column spacing (step 1). Revise column spacing as required.
- 8. Determine reinforcement requirements for lateral spreading.
- 9. Determine overall reinforcement requirements based on LTP and lateral spreading.
- 10. Check global stability.
- 11. Prepare construction drawings and specifications.

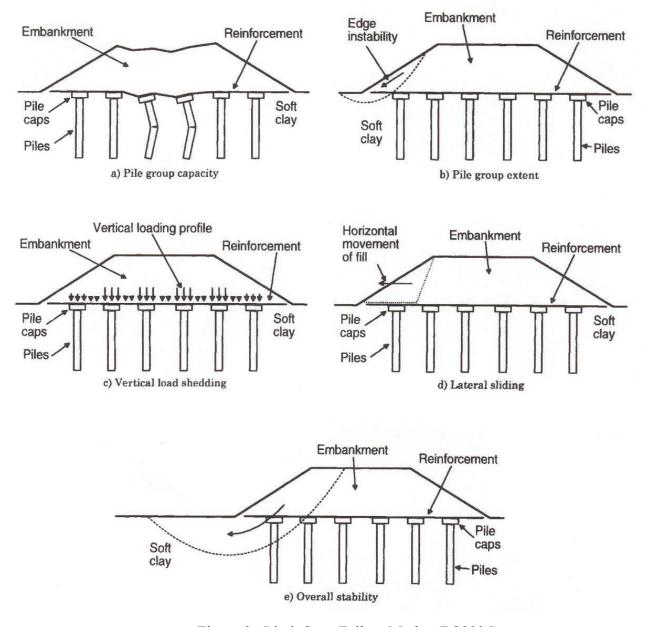
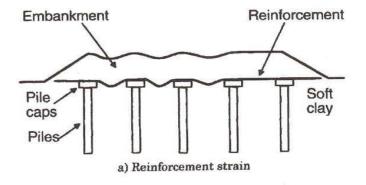


Figure 3. Limit State Failure Modes (BS8006)

The majority of the design steps follow conventional geotechnical engineering practice and is covered extensively in British Standard BS 8006 and the paper "Column Supported Embankment Design Considerations" (Collin, 2004) and will only be briefly covered within this paper. The much more controversial aspect of the design, the design of the load transfer platform (LTP) will be the focus of this paper.



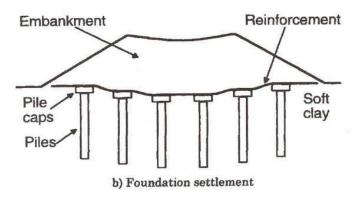


Figure 4. Serviceability State (BS8006)

3.0 COLUMN DESIGN

The selection of column type is most often based on constructability, load capacity, and cost. The load that a column is required to carry is typically based on the tributary area for each column. The embankment and any surcharge load is typically assumed to be carried in their entirety by the columns.

For purposes of determining the design vertical load in the column, it is convenient to associate the tributary area of soil surrounding each column, as illustrated in Figure 5. Although the tributary area forms a regular hexagon about the column, it can be closely approximated as an equivalent circle having the same total area. For square column pattern, the effective diameter (diameter D_e) is equal to 1.13 times the center-to-center column spacing. For triangular column pattern, the effective diameter is equal to 1.05 times the center-to-center column spacing (typical center-to-center column spacing ranges from 1.5- 3.0 m (5-10 ft.)).

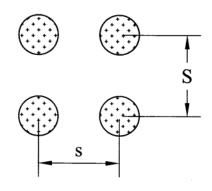
The required design vertical load (Q_r) in the column is determined according to the following equation:

$$Q_r = \pi (D_e/2)^2 (\gamma H + q)$$
 (1)

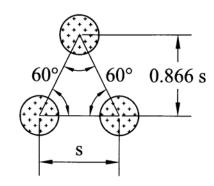
where: $D_e = \text{effective tributary area of column}$

H = height of embankment

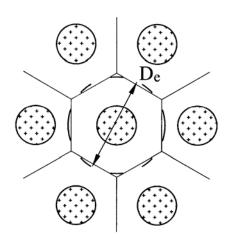
q = live and dead load surcharge (typically 12 kN/m² (250 psf)) γ = unit weight of the embankment soil



a) Square Spacing



b) Triangular Spacing



 $D_e = 1.05 \text{ s}$ for Triangular Spacing

 $D_e = 1.13 \text{ s}$ for Square Spacing

c) Effective Diameter

Figure 5. Column Layout

4.0 EDGE STABILITY- LATERAL EXTENT OF COLUMNS

The lateral extent of the column system across the width of the embankment should extend a sufficient distance beyond the edge of the embankment to ensure that any instability or differential settlement that occurs outside the column supported area will not affect the embankment crest (Figure 3b). There are several approaches that may be used to check the edge stability. The computer software developed for FHWA for the design of both reinforced and non-reinforced slopes and embankments, ReSSA, is an excellent tool for checking edge stability.

The British Standard (BS8006) requires that the columns extend to within a minimum distance (L_p) of the toe of the embankment. Figure 6 defines the terms for edge stability. L_p is determined from the following equation:

$$L_{p} = H (n-\tan\theta_{p})$$
 (2)

where:

n = side slope of the embankment

 θ_p = is the angle (from vertical) between the outer edge of the outer-most column and the crest of the embankment $[\theta_p = (45-\phi_{emb}/2)]$.

 φ_{emb} = effective friction angle of embankment fill

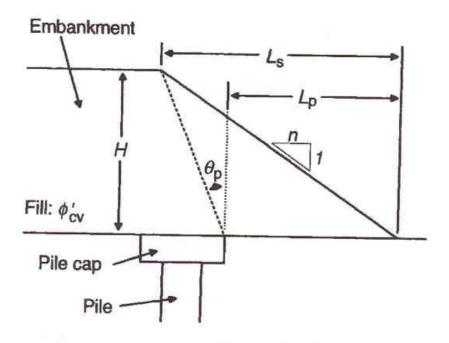


Figure 6. Edge Stability (BS 8006)

The British method is an excellent check of the more rigorous stability analysis using limit

equilibrium techniques (*i.e.*, ReSSA). For preliminary designs and/or feasibility analysis, the simplified British approach is sufficient.

5.0 LATERAL SPREADING

The potential for lateral spreading of the embankment must be analyzed (Figure 7). The geosynthetic reinforcement must be designed to prevent lateral spreading of the embankment. This is a critical aspect of the design, as many of the columns that are appropriate for column supported embankments are not capable of providing adequate lateral resistance to prevent spreading of the embankment without failing.

The geosynthetic reinforcement must be designed to resist the horizontal force due to the lateral spreading of the embankment. The required tensile force to prevent lateral spreading (T_{ls}) is determined from the following equation:

$$T_{ls} = K_a (\gamma H + q)H/2$$
 (3)

where:

 K_a = coefficient of active earth pressure $(\tan^2 (45-\phi_{emb}/2))$

The minimum length of reinforcement (L_e) necessary to develop the required strength of the reinforcement without the side slope of the embankment sliding across the reinforcement is determined using the equation below:

$$L_e = T_{ls} / [0.5 \gamma H(c_{iemb} tan \varphi_{emb})]$$
 (4)

where:

c_{iemb} = coefficient of interaction for sliding between the geosynthetic reinforcement and embankment fill

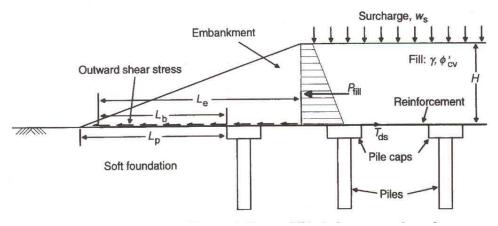


Figure 7. Lateral Spreading (BS 8006)

6.0 LOAD TRANSFER PLATFORM DESIGN

The design of the load transfer platform (Collin Method, Collin, 2004) is based on the use of multiple layers of reinforcement to create a stiff reinforced soil mass (Figure 8). The Collin Method is a refinement of a method sometimes referred to as the Guido Method and assumes that the reinforced soil mass acts as a beam to transfer the load from the embankment above the platform to the columns below. The primary assumptions for the beam theory are:

- A minimum of three layers of reinforcement is used to create the platform.
- Spacing between layers of reinforcement is 200-450 mm (8-18 in.).
- Platform thickness is greater than or equal to one half the clear span between columns.
- Soil arch is fully developed within the depth of the platform.

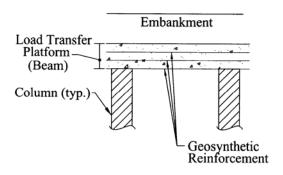


Figure 8. Load transfer mechanism – beam method

6.1 Tension Membrane

In addition to soil arching, the load transfer platform design includes tension membrane theory. The vertical load from the soil within the arch and any surcharge load, if the thickness of the embankment is not great enough to develop the full arch, is carried by the reinforcement. There are several theories available to estimate the tension in the reinforcement (Fluet and Giroud). Figure 9 shows the symbols that will be used in presenting the LTP design. They are defined below:

d = diameter of the column H = height of embankment

 P_c ' = vertical stress on the column

q = surcharge load

s = center-to-center column spacing

 T_{RP} = tension in the extensible reinforcement W_T = vertical load carried by the reinforcement

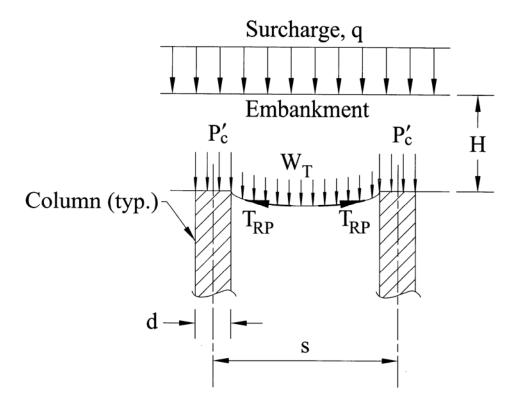


Figure 9. Definition of terms

6.2 Beam Method

The beam (Collin) method is based on the following assumptions:

- The thickness (h) of the load transfer platform is equal to or greater than one half the clear span between columns (s-d).
- A minimum of three layers of extensible (geosynthetic) reinforcement is used to create the load transfer platform.
- Minimum distance between layers of reinforcement is 150 mm (6 in.).
- Select fill is used in the load transfer platform.
- The primary function of the reinforcement is to provide lateral confinement of the select fill to facilitate soil arching within the height (thickness) of the load transfer platform.
- The secondary function of the reinforcement is to support the wedge of soil below the arch.
- The vertical load from the embankment above the load transfer platform is transferred to the columns below the platform.
- The initial strain in the reinforcement is limited to 5%.

The vertical load carried by each layer of reinforcement is a function of the column spacing pattern (*i.e.*, square or triangular) and the vertical spacing of the reinforcement. If the subgrade soil is strong enough to support the first lift of fill, the first layer of reinforcement is located 0.15-

0.25 m (6-10 in.) above subgrade. Each layer of reinforcement is designed to carry the load from the platform fill that is within the soil wedge below the arch. The fill load attributed to each layer of reinforcement is the material located between that layer of reinforcement and the next layer above (Figure 10).

The uniform vertical load on any layer (n) of reinforcement (W_{Tn}) may be determined from the equation below for an angle of arching of 45 degrees:

 W_{Tn} = (area at reinforcement layer n + area at reinforcement layer (n+1))/2) (layer thickness) (load transfer platform fill density)/(area at reinforcement layer n)

$$W_{Tn} = [A_n + A_{n+1}] h_n \gamma / 2 A_n$$
 (5)

where: A = Area at reinforcement layer n or n+1

= $[(s-d) - 2(\Sigma Reinforcement Vertical Spacing/tan45)]^2$ for square column spacing

= $[(s-d) - 2(\Sigma Reinforcement Vertical Spacing/tan45)]^2 sin60/2$ for triangular column spacing

The tensile load in the reinforcement is determined based on tension membrane theory and is a function of the amount of strain in the reinforcement. The tension in the reinforcement is determined from the following equation:

$$T_{rpn} = W_{Tn} \Omega D/2$$
 (6)

where: D = design span for tensioned membrane

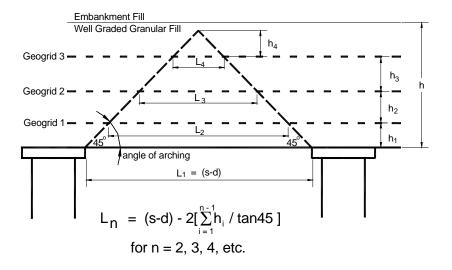
= $1.41*[(s-d) - 2(\Sigma Vertical Spacing/tan45)]$ for square column spacing

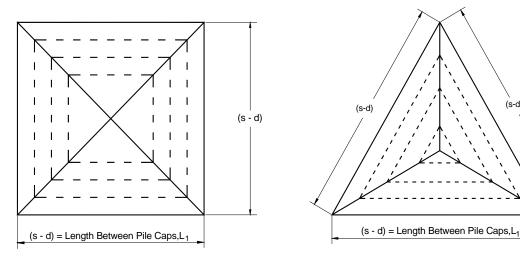
= $0.867*[(s-d) - 2(\Sigma Vertical Spacing/tan45)]$ for triangular column spacing

 Ω = dimensionless factor from tensioned membrane theory

Table 1. Values of Ω .

Ω	Reinforcement Strain (ε)%
2.07	1
1.47	2
1.23	3
1.08	4
0.97	5





Square Column Spacing

Triangular Column Spacing

Figure 10. Load transfer platform design Collin method

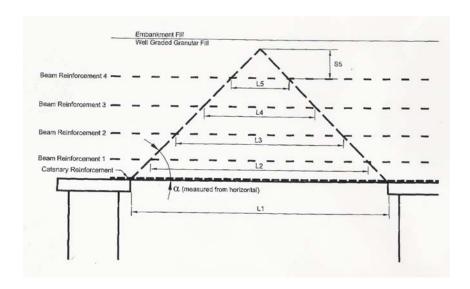


Figure 11. Modified beam method reinforcement

6.3 Modified Beam Method

Based on research recently completed (Collin, et. al., 2005) using numerical modeling the above procedure has been modified. The modification involves the addition of one layer of reinforcement at subgrade. This layer of reinforcement is designed as a catenary to carry the load from the soil below the arch (Figure 11).

The uniform vertical load on the catenary layer of reinforcement (W_{TC}) may be determined from the equation below:

 W_{TCn} = (volume pyramid below the arch) (load transfer platform fill density)/(area at reinforcement catenary layer)

$$W_{Tn} = h_n \gamma / 3$$
 Square or Triangular column spacing (7)

The tensile load in the reinforcement is determined based on tension membrane theory and is a function of the amount of strain in the reinforcement. The tension in the reinforcement is determined from the following equation:

$$T_{rpC} = W_{TC} \Omega D/2$$
 (8)

where: D = design span for tensioned membrane

= $1.41*[(s-d) - 2(\Sigma \text{Vertical Spacing/tan45})]$ for square column spacing

= $0.867*[(s-d) - 2(\Sigma Vertical Spacing/tan45)]$ for triangular column spacing

 Ω = dimensionless factor from tensioned membrane theory

The reinforcement to create the beam above the catenary layer of reinforcement is designed according to equations 5 and 6.

7.0 CONCLUSIONS

The used of CSE is expanding both in the US and abroad. Numerous design guidelines have been developed for the design. Currently there are at least 5 to 10 methods to design the load transfer platform. The method presented here is one that has been developed by the authors and used with great success. However, the recommendations provided in this paper cover only the basic steps in the design of the LTP. The detailing of the platform (i.e., edge detail), selection of geosynthetic reinforcement, creep characteristics of the geosynthetic, overlaps, etc. are beyond the scope of this paper but must be considered in the design.

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